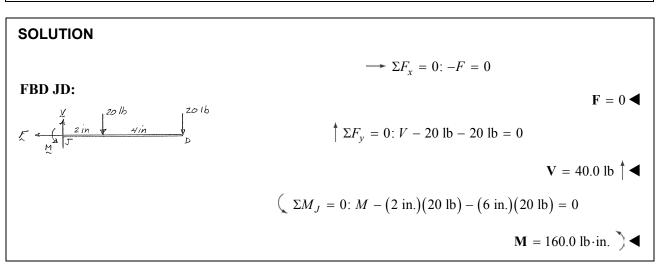
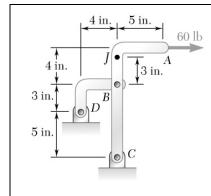


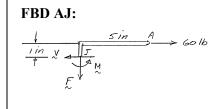
Determine the internal forces (axial force, shearing force, and bending moment) at point J of the structure indicated: Frame and loading of Prob. 6.77.

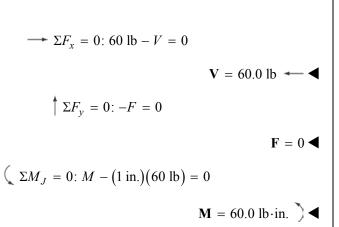


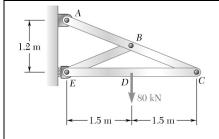


Determine the internal forces (axial force, shearing force, and bending moment) at point J of the structure indicated: Frame and loading of Prob. 6.76.

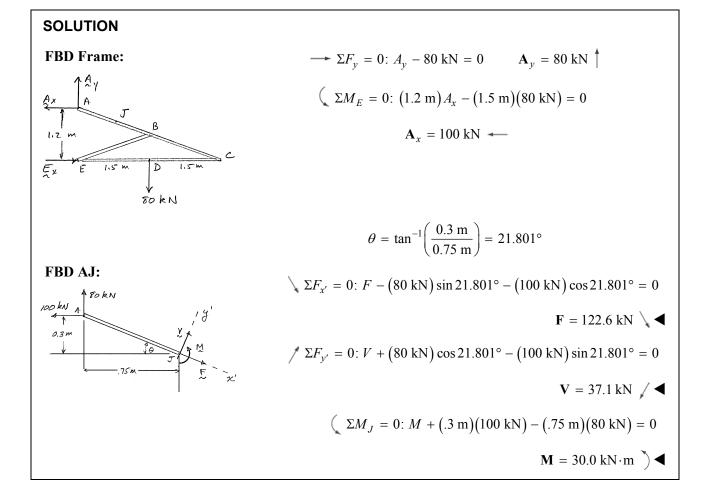
# SOLUTION

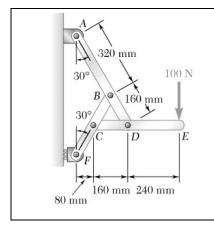




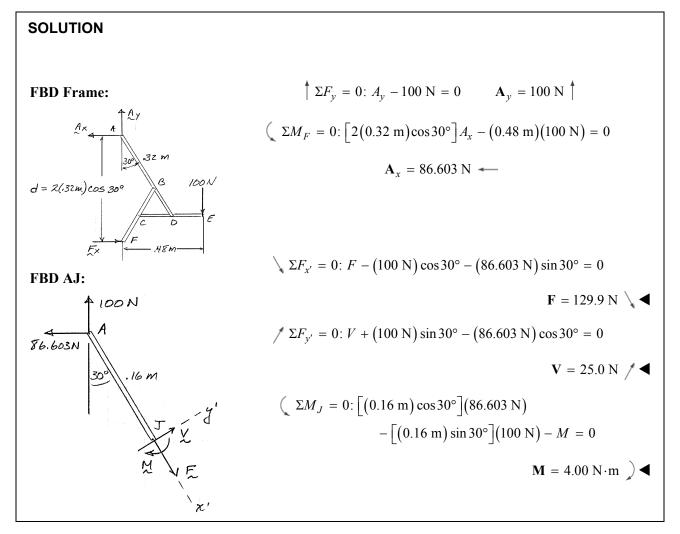


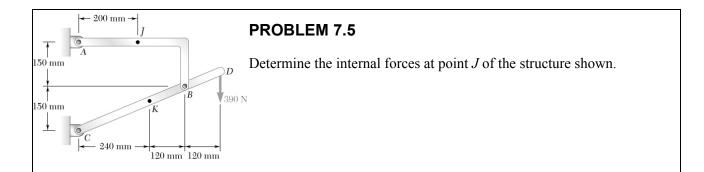
For the frame and loading of Prob. 6.80, determine the internal forces at a point J located halfway between points A and B.

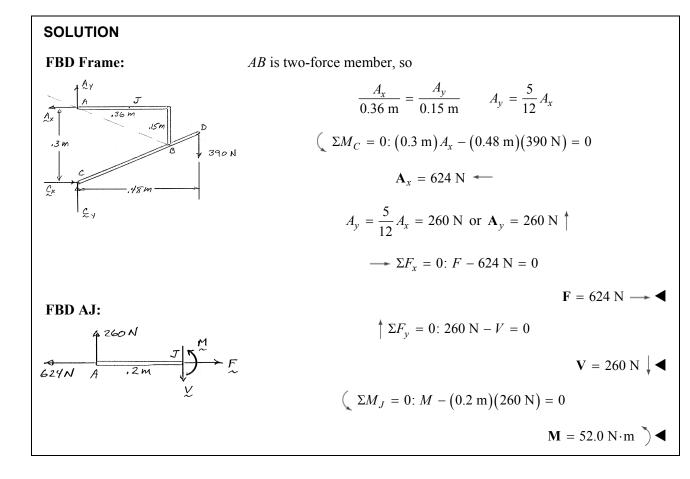


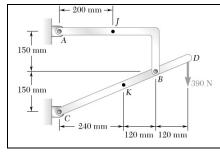


For the frame and loading of Prob. 6.101, determine the internal forces at a point J located halfway between points A and B.

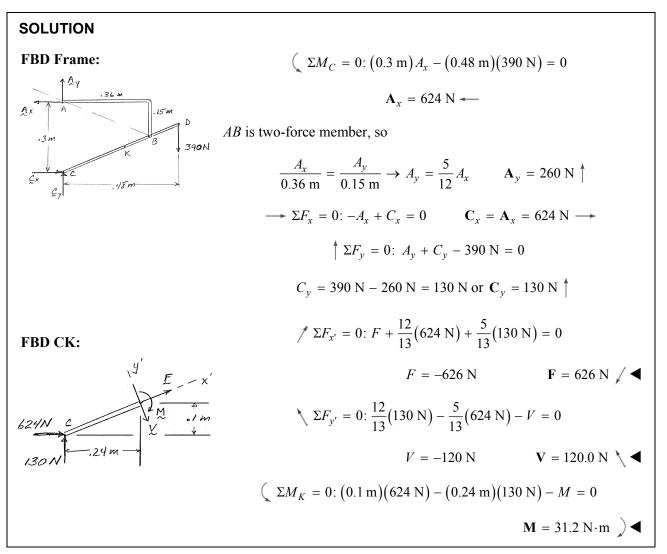


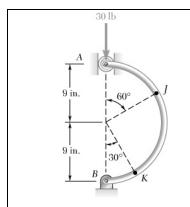






Determine the internal forces at point *K* of the structure shown.

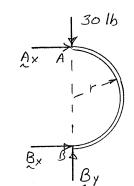




A semicircular rod is loaded as shown. Determine the internal forces at point J.

SOLUTION



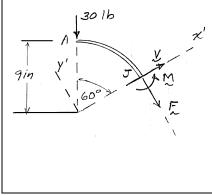


$$\left( \sum M_B = 0 : A_x(2r) = 0 \right)$$
$$\mathbf{A}_x = 0$$

 $\int \Sigma F_{x'} = 0: V - (30 \text{ lb}) \cos 60^\circ = 0$ 

**V** = 15.00 lb / ◀

FBD AJ:

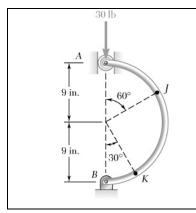


 $\sum \Sigma F_{y'} = 0: F + (30 \text{ lb}) \sin 60^\circ = 0$ F = -25.98 lb

 $\mathbf{F} = 26.0 \text{ lb} \setminus \blacktriangleleft$ 

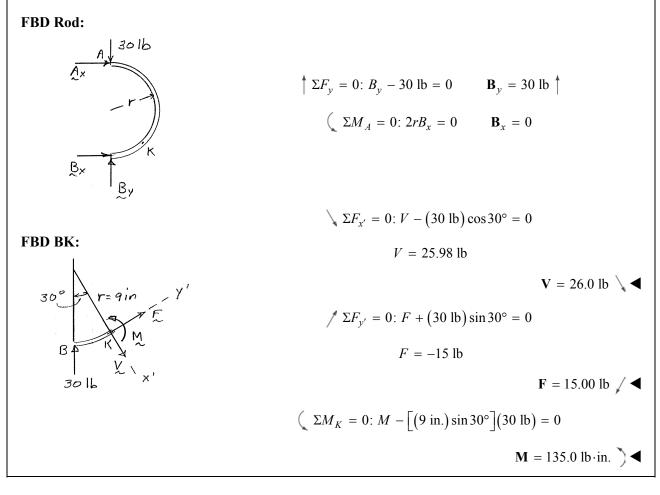
$$(\Sigma M_J = 0: M - [(9 \text{ in.}) \sin 60^\circ](30 \text{ lb}) = 0$$
  
 $M = -233.8 \text{ lb} \cdot \text{in.}$ 

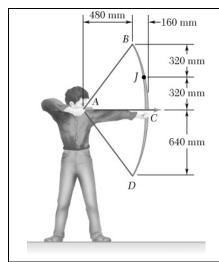
 $\mathbf{M} = 234 \text{ lb} \cdot \text{in.}$ 



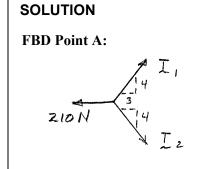
A semicircular rod is loaded as shown. Determine the internal forces at point *K*.

#### SOLUTION





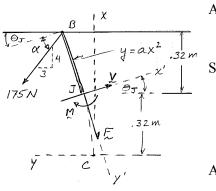
An archer aiming at a target is pulling with a 210-N force on the bowstring. Assuming that the shape of the bow can be approximated by a parabola, determine the internal forces at point *J*.



By symmetry 
$$T_1 = T_2$$
  
 $\longrightarrow \Sigma F_x = 0: 2\left(\frac{3}{5}T_1\right) - 210 \text{ N} = 0$   $T_1 = T_2 = 175 \text{ N}$ 

Curve CJB is parabolic:  $y = ax^2$ 

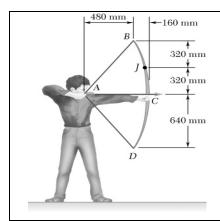
FBD BJ:



At B: 
$$x = 0.64 \text{ m}, \quad y = 0.16 \text{ m} \quad a = \frac{0.16 \text{ m}}{(0.64 \text{ m})^2} = \frac{1}{2.56 \text{ m}}$$
  
So, at J:  $y_J = \frac{1}{2.56 \text{ m}} (0.32 \text{ m})^2 = 0.04 \text{ m}$   
Slope of parabola =  $\tan \theta = \frac{dy}{dx} = 2ax$   
At J:  $\theta_J = \tan^{-1} \left[ \frac{2}{2.56 \text{ m}} (0.32 \text{ m}) \right] = 14.036^\circ$   
So  $\alpha = \tan^{-1} \frac{4}{3} - 14.036^\circ = 39.094^\circ$   
 $\swarrow \Sigma F_{x'} = 0: V - (175 \text{ N})\cos(39.094^\circ) = 0$   
 $V = 135.8 \text{ N} \checkmark \blacktriangleleft$   
 $\Sigma F_{y'} = 0: F + (175 \text{ N})\sin(39.094^\circ) = 0$   
 $F = -110.35 \text{ N}$   
 $F = 110.4 \text{ N} \checkmark \blacktriangleleft$ 

# **PROBLEM 7.9 CONTINUED**

$$\left(\Sigma M_{J} = 0: M + (0.32 \text{ m}) \left[\frac{3}{5}(175 \text{ N})\right] + \left[(0.16 - 0.04) \text{m}\right] \left[\frac{4}{5}(175 \text{ N})\right] = 0$$
  
 $\mathbf{M} = 50.4 \text{ N} \cdot \text{m}$ 



For the bow of Prob. 7.9, determine the magnitude and location of the maximum (a) axial force, (b) shearing force, (c) bending moment.

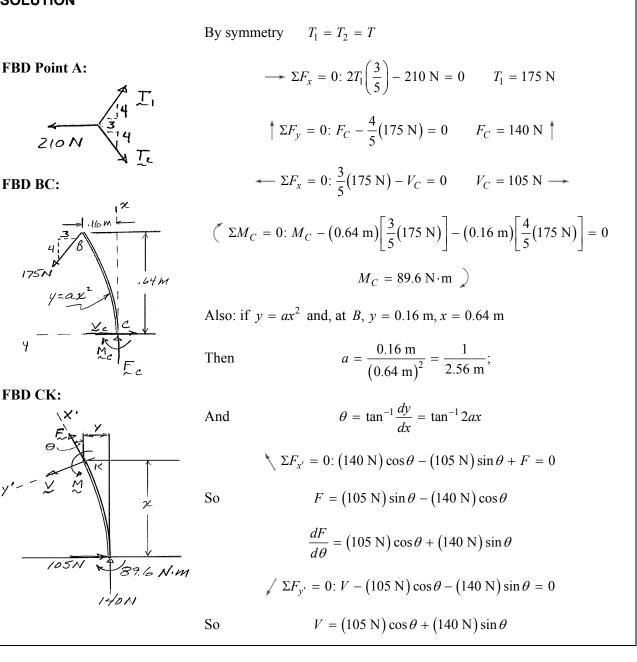
SOLUTION

**FBD BC:** 

175

Y

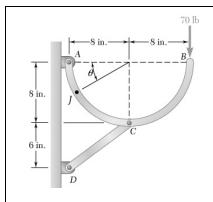
**FBD CK:** 



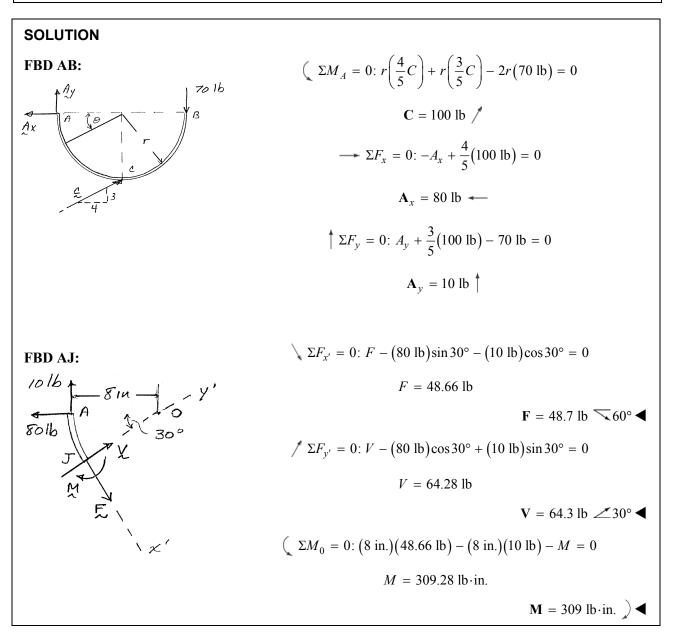
# **PROBLEM 7.10 CONTINUED**

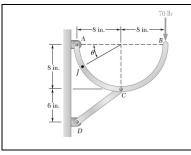
And 
$$\frac{dV}{d\theta} = -(105 \text{ N})\sin\theta + (140 \text{ N})\cos\theta$$
$$\left(\Sigma M_{K} = 0: M + x(105 \text{ N}) + y(140 \text{ N}) - 89.6 \text{ N} \cdot \text{m} = 0$$
$$M = -(105 \text{ N})x - \frac{(140 \text{ N})x^{2}}{(2.56 \text{ m})} + 89.6 \text{ N} \cdot \text{m}$$
$$\frac{dM}{dx} = -(105 \text{ N}) - (109.4 \text{ N/m})x + 89.6 \text{ N} \cdot \text{m}$$
Since none of the functions, *F*, *V*, or *M* has a vanishing derivative in the valid range of  $0 \le x \le 0.64 \text{ m} (0 \le \theta \le 26.6^{\circ})$ , the maxima are at the limits  $(x = 0, \text{ or } x = 0.64 \text{ m})$ .

Therefore,	<i>(a)</i>	$\mathbf{F}_{\max} = 140.0 \text{ N} \uparrow \text{at } C \blacktriangleleft$
	<i>(b)</i>	$\mathbf{V}_{\max} = 156.5 \text{ N} / \text{at } B \blacktriangleleft$
	(c)	$\mathbf{M}_{\text{max}} = 89.6 \text{ N} \cdot \text{m}$ at $C \blacktriangleleft$

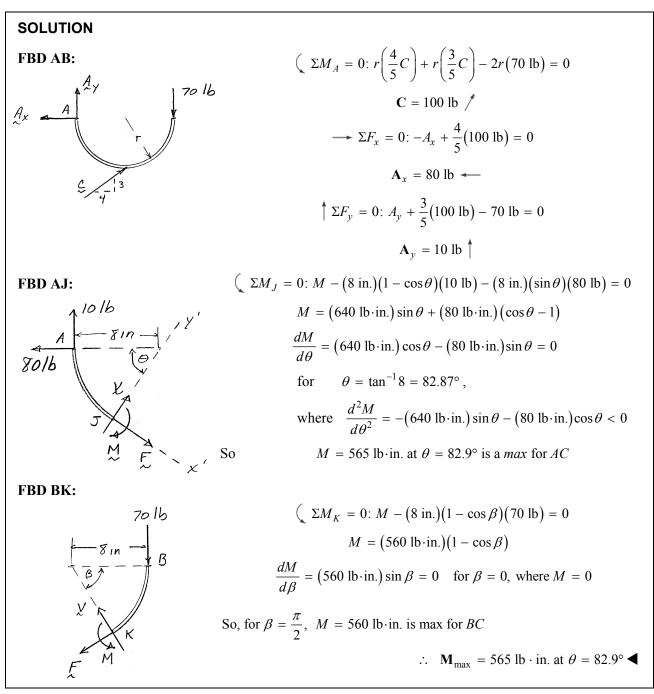


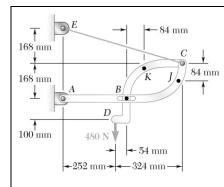
A semicircular rod is loaded as shown. Determine the internal forces at point J knowing that  $\theta = 30^{\circ}$ .



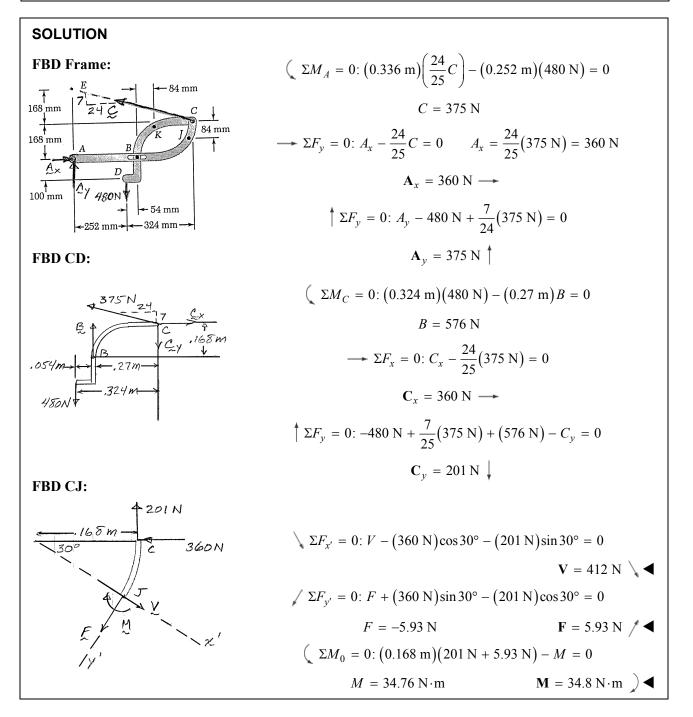


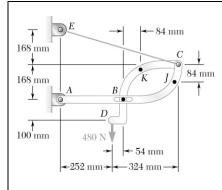
A semicircular rod is loaded as shown. Determine the magnitude and location of the maximum bending moment in the rod.





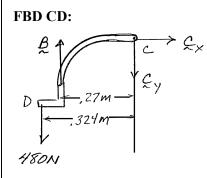
Two members, each consisting of straight and 168-mm-radius quartercircle portions, are connected as shown and support a 480-N load at D. Determine the internal forces at point J.



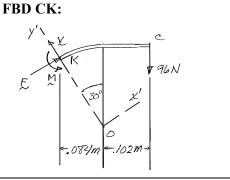


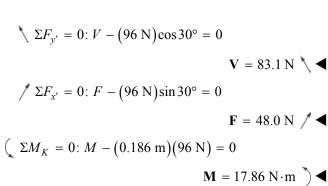
Two members, each consisting of straight and 168-mm-radius quartercircle portions, are connected as shown and support a 480-N load at D. Determine the internal forces at point K.

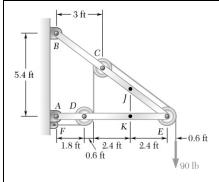
#### SOLUTION



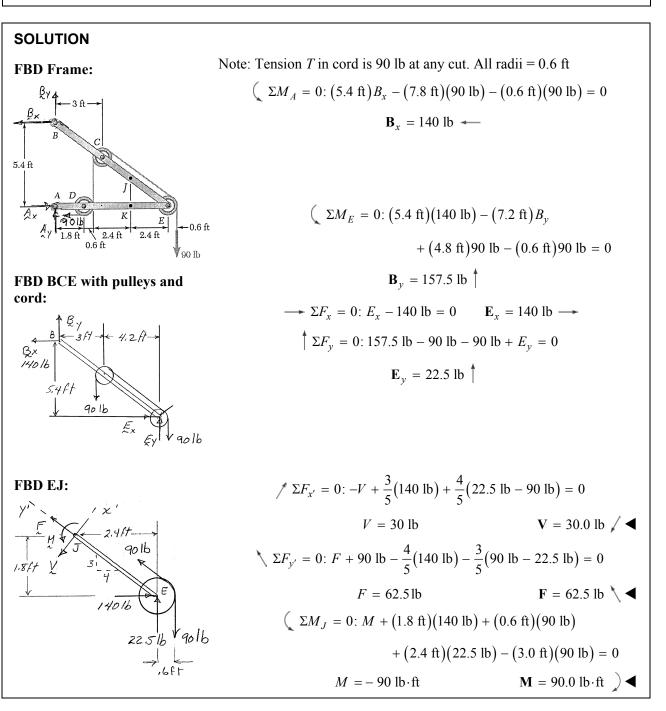
 $\sum F_x = 0: \quad \mathbf{C}_x = 0$   $( \Sigma M_B = 0: (0.054 \text{ m})(480 \text{ N}) - (0.27 \text{ m})C_y = 0$   $\mathbf{C}_y = 96 \text{ N} \downarrow$   $\uparrow \Sigma F_y = 0: B - C_y = 0 \qquad \mathbf{B} = 96 \text{ N} \uparrow$   $\sum F_{y'} = 0: V - (96 \text{ N})\cos 30^\circ = 0$ 

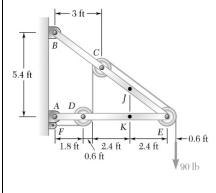




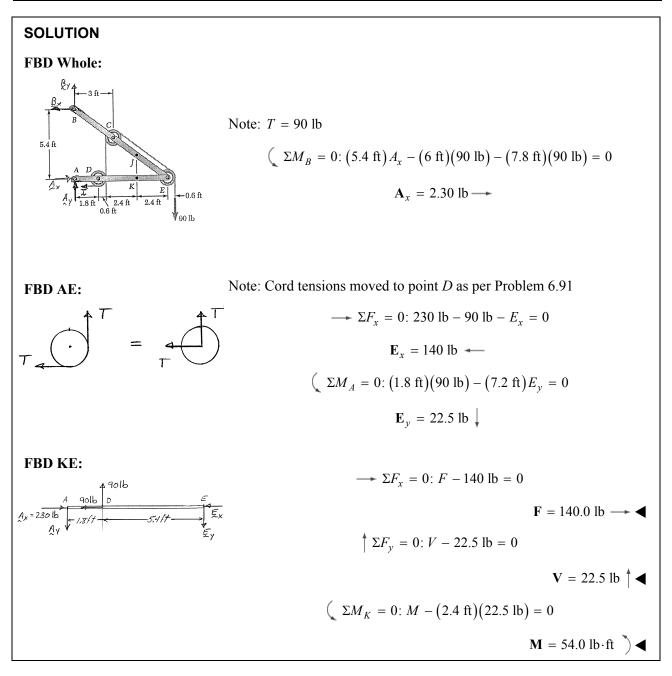


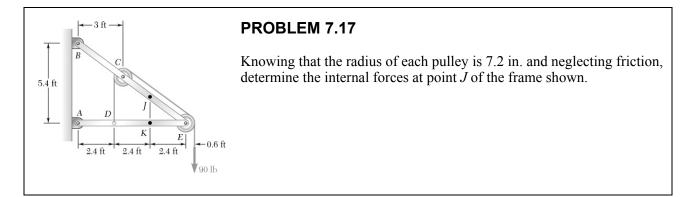
Knowing that the radius of each pulley is 7.2 in. and neglecting friction, determine the internal forces at point J of the frame shown.

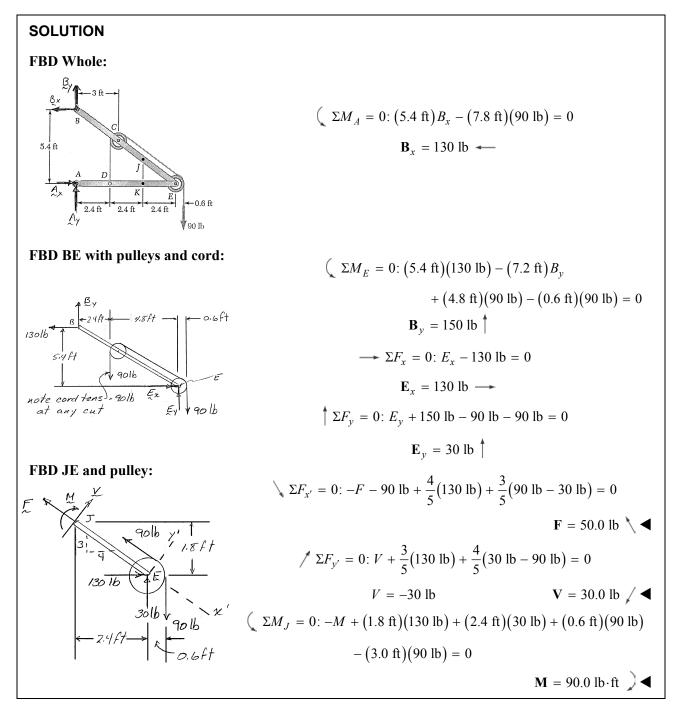


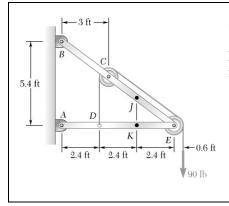


Knowing that the radius of each pulley is 7.2 in. and neglecting friction, determine the internal forces at point K of the frame shown.

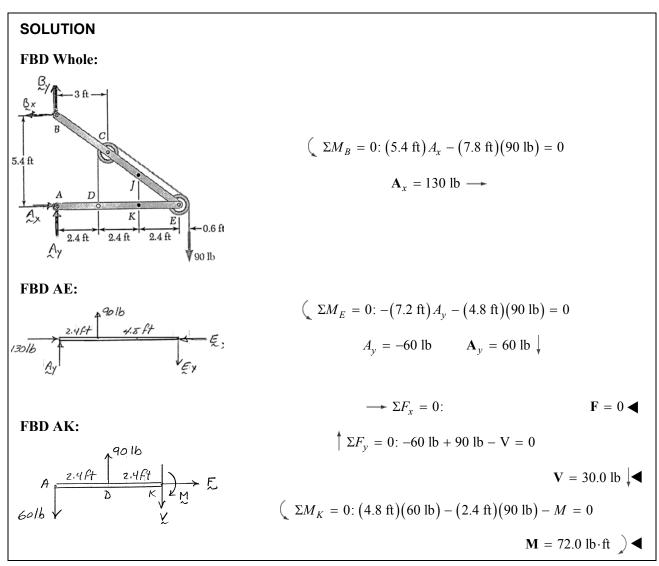


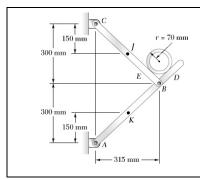




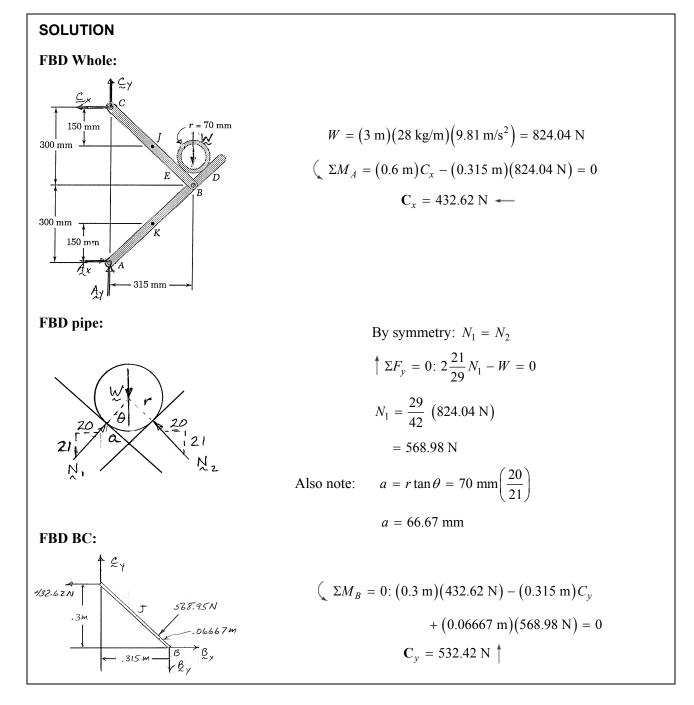


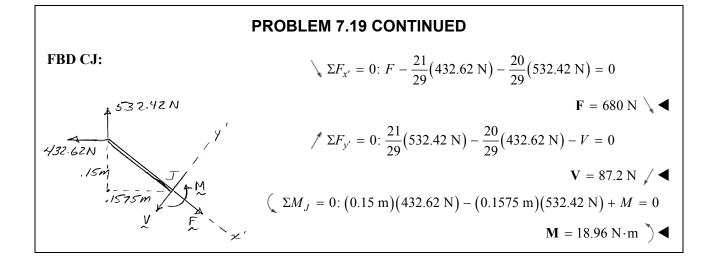
Knowing that the radius of each pulley is 7.2 in. and neglecting friction, determine the internal forces at point *K* of the frame shown.

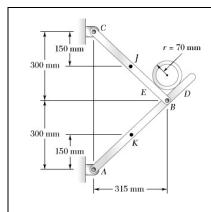




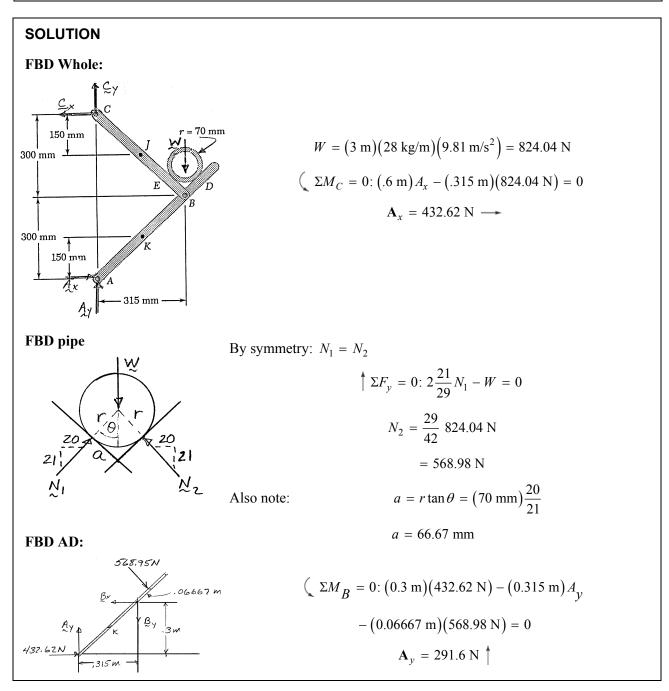
A 140-mm-diameter pipe is supported every 3 m by a small frame consisting of two members as shown. Knowing that the combined mass per unit length of the pipe and its contents is 28 kg/m and neglecting the effect of friction, determine the internal forces at point *J*.

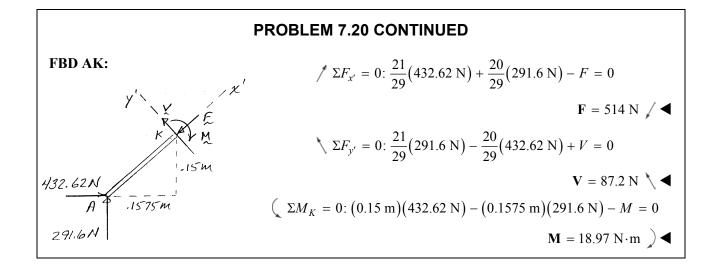


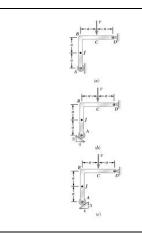




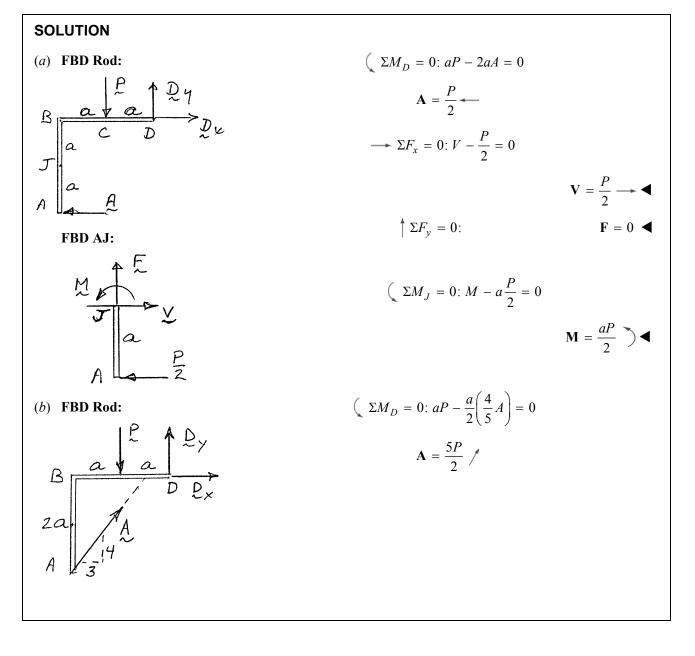
A 140-mm-diameter pipe is supported every 3 m by a small frame consisting of two members as shown. Knowing that the combined mass per unit length of the pipe and its contents is 28 kg/m and neglecting the effect of friction, determine the internal forces at point K.

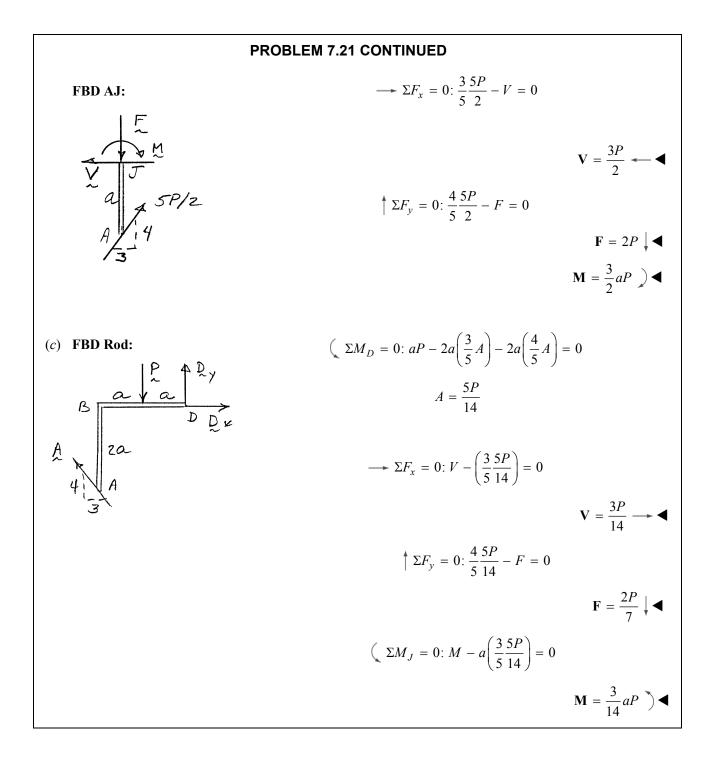


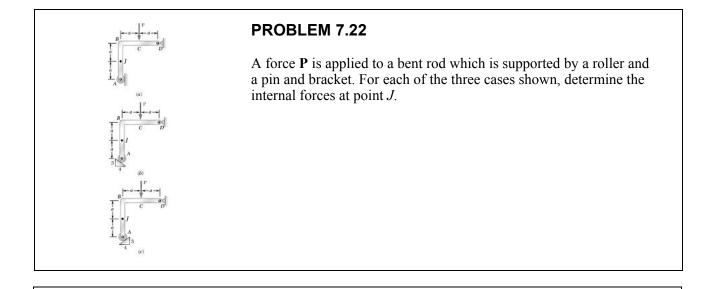


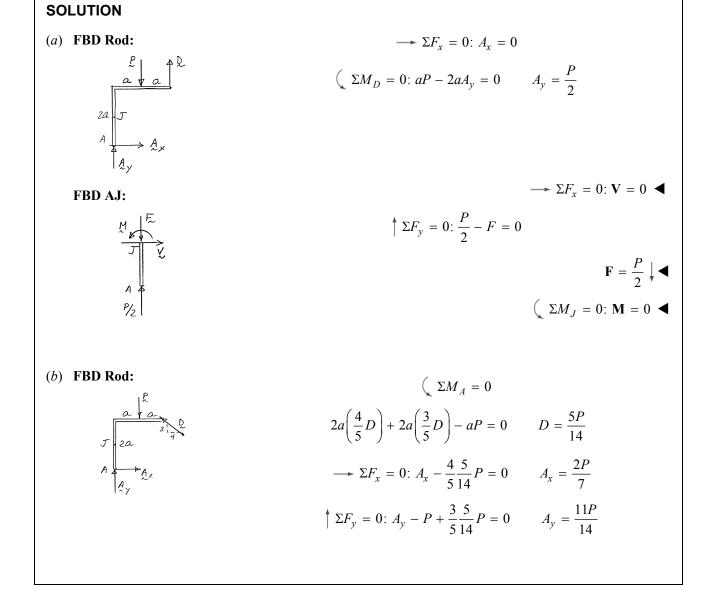


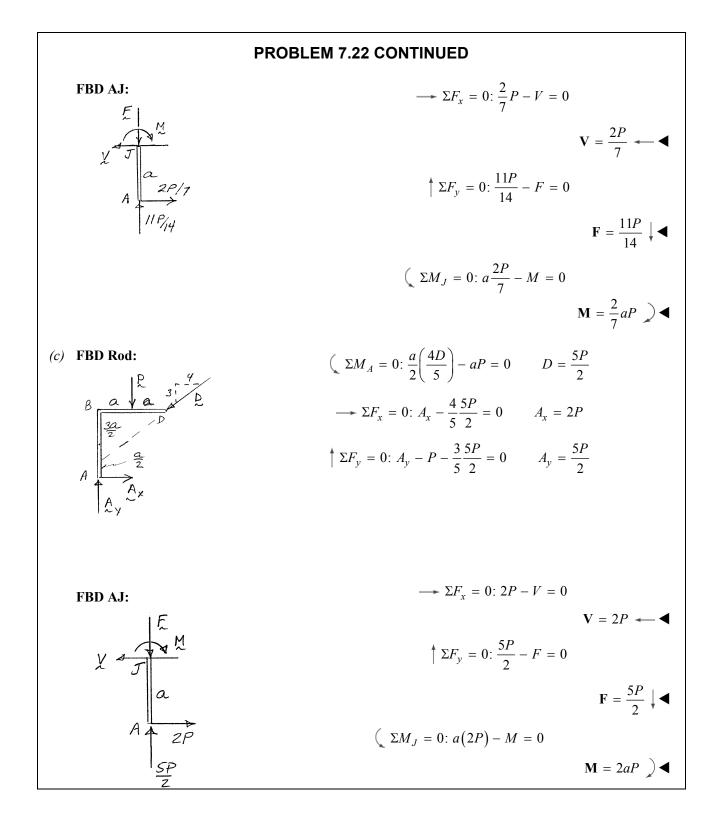
A force **P** is applied to a bent rod which is supported by a roller and a pin and bracket. For each of the three cases shown, determine the internal forces at point J.

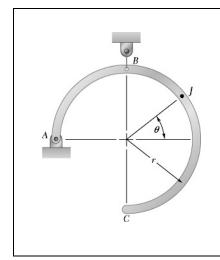


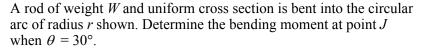




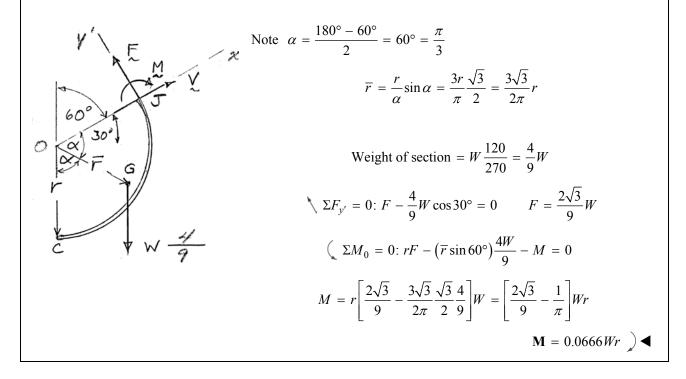


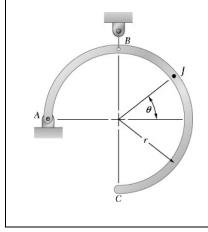




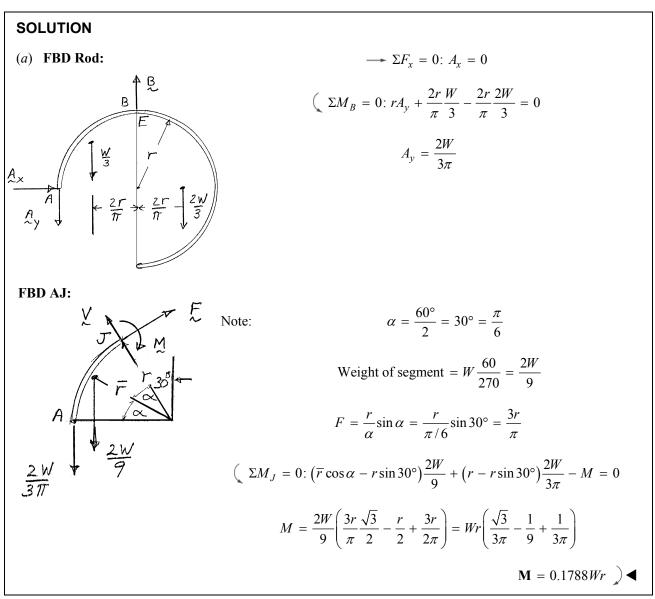


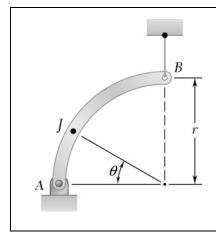
#### SOLUTION





A rod of weight W and uniform cross section is bent into the circular arc of radius r shown. Determine the bending moment at point J when  $\theta = 120^{\circ}$ .





A quarter-circular rod of weight W and uniform cross section is supported as shown. Determine the bending moment at point J when  $\theta = 30^{\circ}$ .

 $\nabla E$ 

A. A

# SOLUTION



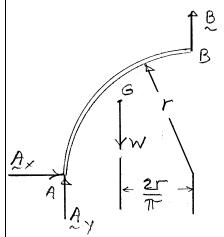
FBD AJ:

₩<u>₩</u>

1

f

150



150

0

$$\rightarrow \Sigma F_x = 0: \mathbf{A}_x = 0$$

$$\left( \Sigma M_B = 0: \frac{2r}{\pi} W - rA_y = 0 \qquad \mathbf{A}_y = \frac{2W}{\pi} \right)$$

$$\alpha = 15^\circ, \text{ weight of segment} = W \frac{30^\circ}{90^\circ} = \frac{W}{3}$$

$$\overline{r} = \frac{r}{\alpha} \sin \alpha = \frac{r}{\pi/12} \sin 15^\circ = 0.9886r$$

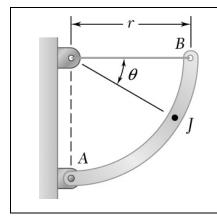
$$f \Sigma F_{y'} = 0: \frac{2W}{\pi} \cos 30^\circ - \frac{W}{3} \cos 30^\circ - F = 0$$

$$\mathbf{F} = \frac{W\sqrt{3}}{2} \left(\frac{2}{\pi} - \frac{1}{3}\right) \mathbf{A}$$

$$\left(\Sigma M_0 = M + r \left(F - \frac{2W}{\pi}\right) + \overline{r} \cos 15^\circ \frac{W}{3} = 0$$

$$\mathbf{M} = 0.0557 Wr$$

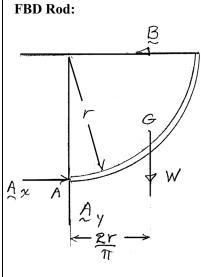
◀



Β

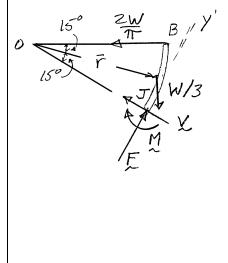
A quarter-circular rod of weight W and uniform cross section is supported as shown. Determine the bending moment at point J when  $\theta = 30^{\circ}$ .

# SOLUTION



 $\sum M_A = 0: rB - \frac{2r}{\pi}W = 0$  $\mathbf{B} = \frac{2W}{\pi} \longleftarrow$ 

FBD BJ:



$$\overline{r} = \frac{r}{\pi/12} \sin 15^\circ = 0.98862r$$
  
Weight of segment =  $W \frac{30^\circ}{90^\circ} = \frac{W}{3}$ 

 $\alpha = 15^\circ = \frac{\pi}{12}$ 

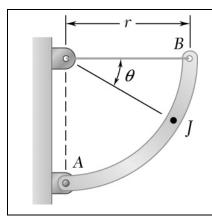
$$\int \Sigma F_{y'} = 0: F - \frac{W}{3}\cos 30^\circ - \frac{2W}{\pi}\sin 30^\circ = 0$$

$$\mathbf{F} = \left(\frac{\sqrt{3}}{6} + \frac{1}{\pi}\right) W / \mathbf{I}$$

$$\left(\Sigma M_0 = 0: rF - \left(\overline{r}\cos 15^\circ\right)\frac{w}{3} - M = 0\right)$$

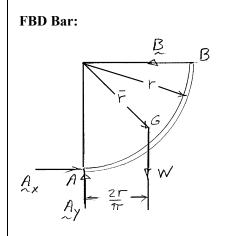
$$M = rW\left(\frac{\sqrt{3}}{6} + \frac{1}{\pi}\right) - \left(0.98862\frac{\cos 15^\circ}{3}\right)Wr$$

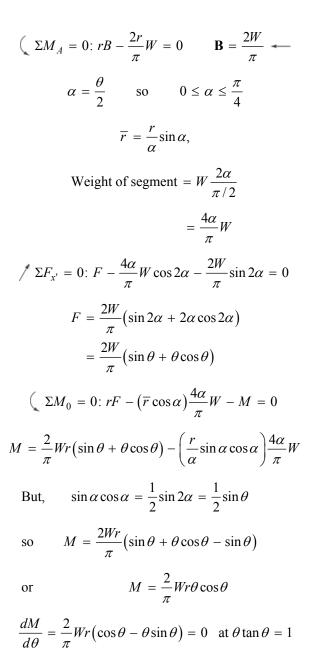
 $\mathbf{M} = 0.289 W r$ 



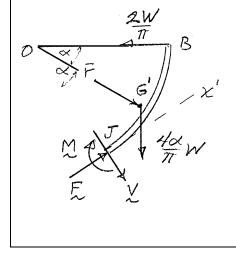
For the rod of Prob.7.26, determine the magnitude and location of the maximum bending moment.

#### SOLUTION

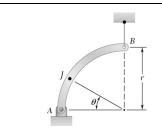




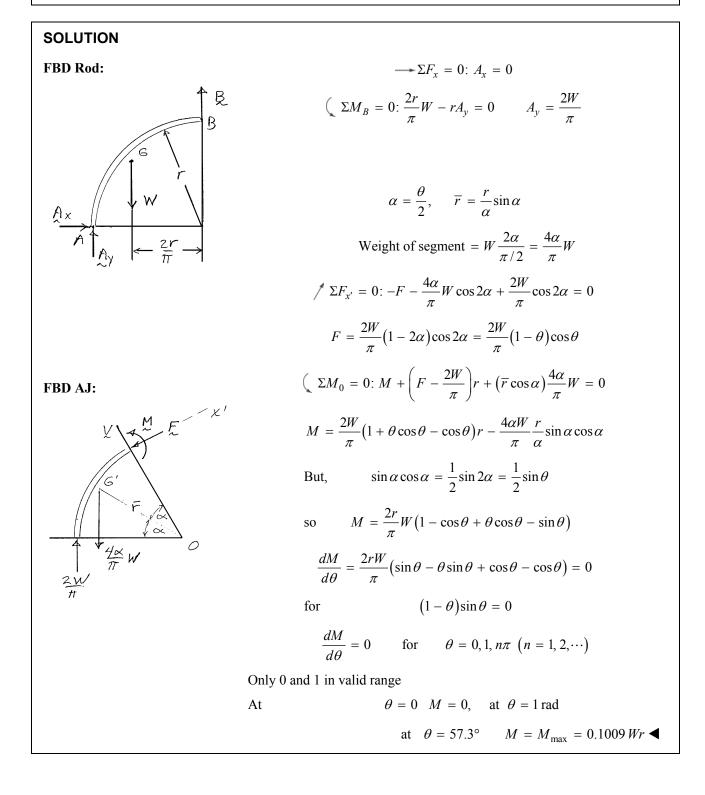
FBD BJ:

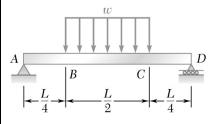


# **PROBLEM 7.27 CONTINUED** Solving numerically $\theta = 0.8603$ rad and $\mathbf{M} = 0.357 Wr$ (4)at $\theta = 49.3^{\circ}$ (Since M = 0 at both limits, this is the maximum)

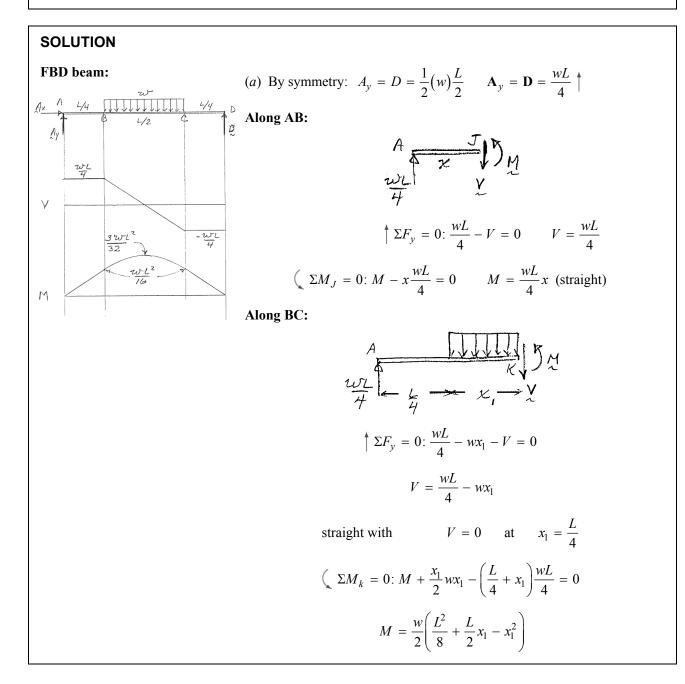


For the rod of Prob.7.25, determine the magnitude and location of the maximum bending moment.

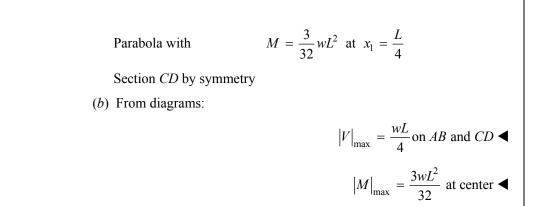


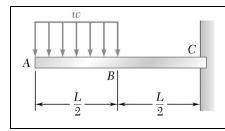


For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



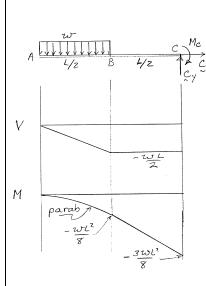
#### **PROBLEM 7.29 CONTINUED**





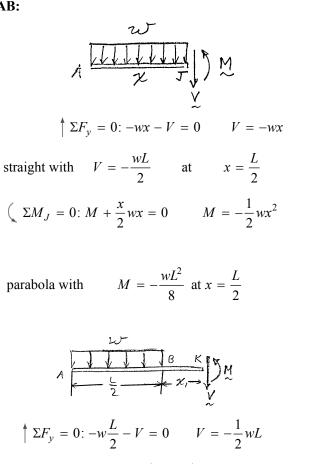
For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

#### SOLUTION



(a) Along AB:

Along BC:



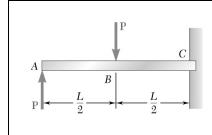
$$\sum F_{v} = 0: -w\frac{L}{2} - V$$

$$\sum M_k = 0: M + \left(x_1 + \frac{L}{4}\right)w\frac{L}{2} = 0$$
$$M = -\frac{wL}{2}\left(\frac{L}{4} + x_1\right)$$

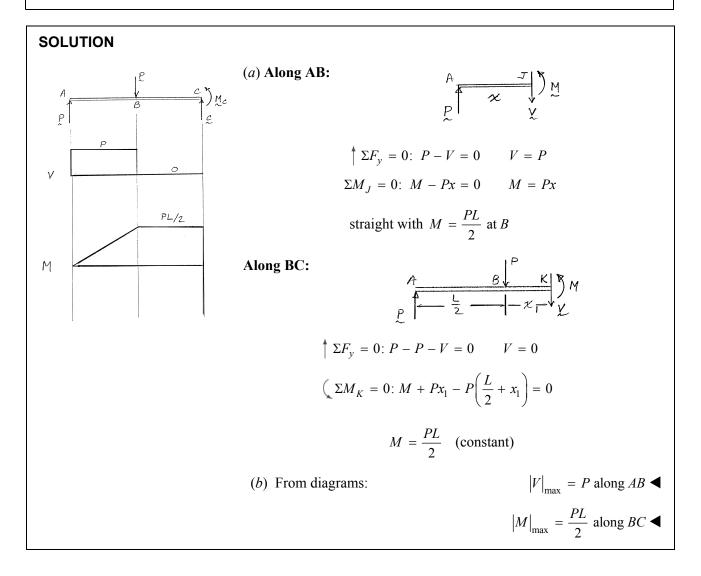
straight with  $M = -\frac{3}{8}wL^2$  at  $x_1 = \frac{L}{2}$ 

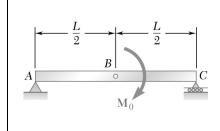
(b) From diagrams:

$$|V|_{\text{max}} = \frac{wL}{2} \text{ on } BC \blacktriangleleft$$
$$|M|_{\text{max}} = \frac{3wL^2}{8} \text{ at } C \blacktriangleleft$$



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

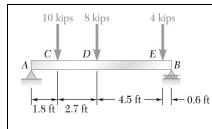




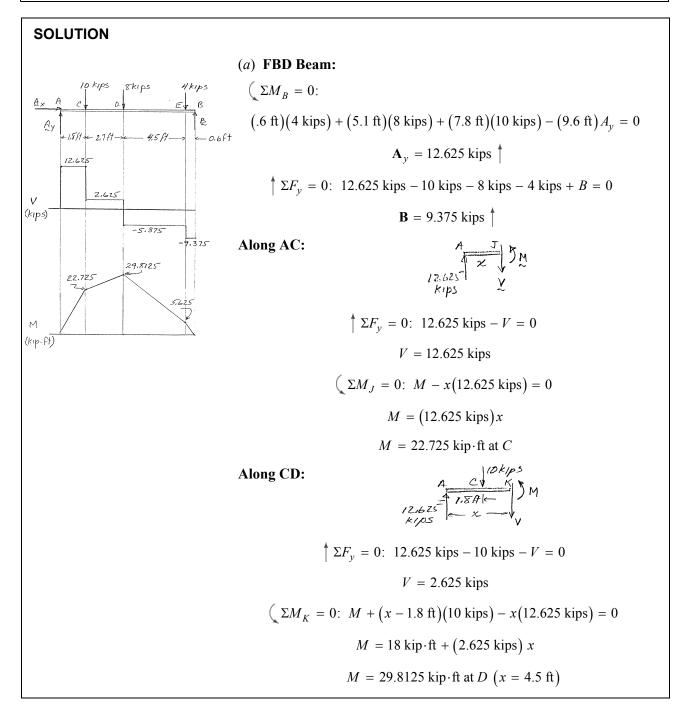
For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

### 

 $(\Sigma M_{C} = 0: LA_{v} - M_{0} = 0$ (*a*) **FBD Beam:**  $\mathbf{A}_{y} = \frac{M_{0}}{L} \downarrow$  $\uparrow \Sigma F_y = 0: -A_y + C = 0 \qquad \mathbf{C} = \frac{M_0}{I} \uparrow$ A T M Along AB:  $\sum F_y = 0: -\frac{M_0}{I} - V = 0$   $V = -\frac{M_0}{I}$  $(\Sigma M_J = 0: x \frac{M_0}{I} + M = 0 \qquad M = -\frac{M_0}{I} x$ straight with  $M = -\frac{M_0}{2}$  at B  $\begin{array}{c}
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\left( T  $)
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\left( T$  )**Along BC:**  $\uparrow \Sigma F_y = 0: -\frac{M_0}{I} - V = 0 \qquad V = -\frac{M_0}{I}$  $\sum M_{K} = 0: M + x \frac{M_{0}}{L} - M_{0} = 0 \qquad M = M_{0} \left(1 - \frac{x}{L}\right)$ straight with  $M = \frac{M_0}{2}$  at B = 0 at C $|V|_{\text{max}} = P$  everywhere (b) From diagrams:  $|M|_{\text{max}} = \frac{M_0}{2}$  at  $B \blacktriangleleft$ 



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.33 CONTINUED**

Along DE:

Along EB:

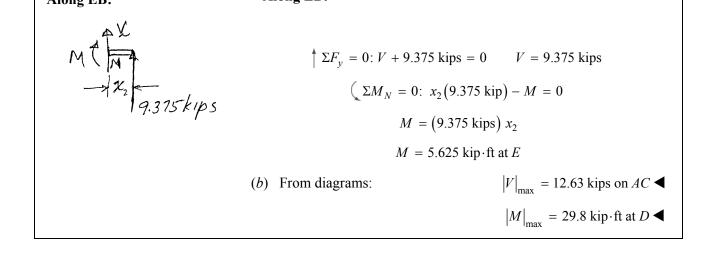
12.625 KIPS

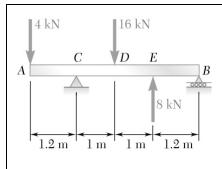
lokips 8k

C

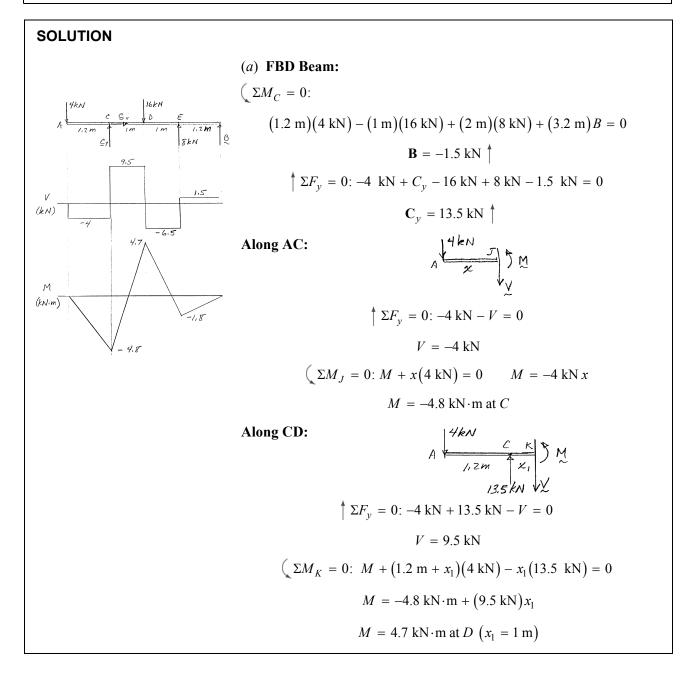
#### Along DE:

$$\sum_{k=0}^{K} \sum_{k=0}^{K} \sum_{k$$





For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.34 CONTINUED**

Along DE:

$$\uparrow \Sigma F_y = 0: V + 8 \text{ kN} - 1.5 \text{ kN} = 0$$
$$V = -6.5 \text{ kN}$$
$$(\Sigma M_L = 0: M - x_3(8 \text{ kN}) + (x_3 + 1.2 \text{ m})(1.5 \text{ kN}) = 0$$
$$M = -1.8 \text{ kN} \cdot \text{m} + (6.5 \text{ kN})x_3$$
$$M = 4.7 \text{ kN} \cdot \text{m} \text{ at } D (x_3 = 1 \text{ m})$$

Along EB:

$$\int_{M} \bigvee_{N} = 0: V - 1.5 \text{ kN} = 0$$

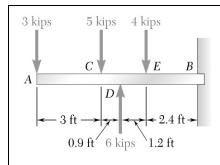
$$V = 1.5 \text{ kN}$$

$$(\sum M_{N} = 0: x_{2}(1.5 \text{ kN}) + M = 0$$

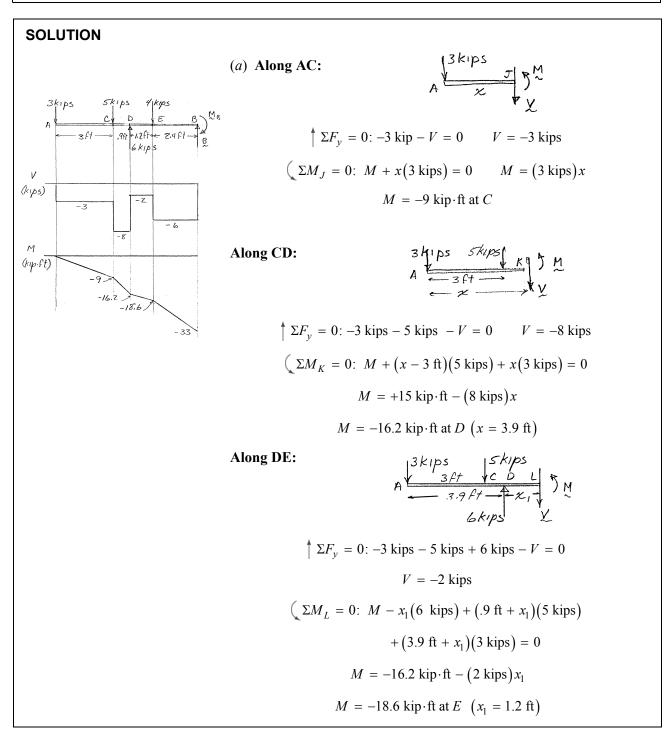
$$M = -(1.5 \text{ kN})x_{2} \qquad M = -1.8 \text{ kN} \cdot \text{m at } E$$

$$(b) \text{ From diagrams:} \qquad |V|_{\text{max}} = 9.50 \text{ kN} \cdot on \ CD \blacktriangleleft$$

$$|M|_{\text{max}} = 4.80 \text{ kN} \cdot \text{m at } C \blacktriangleleft$$



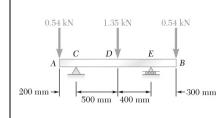
For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



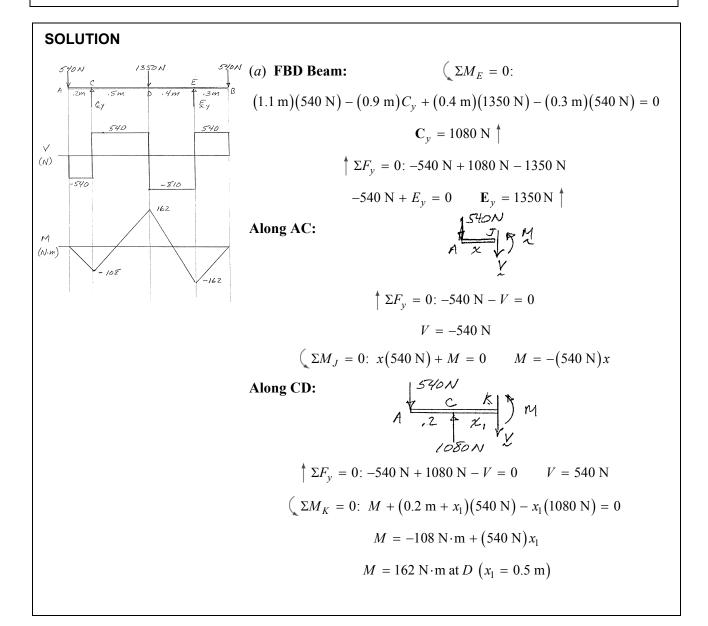
#### **PROBLEM 7.35 CONTINUED**

Along EB:

$$A = \frac{\int_{3}^{3} \frac{k}{k} \int_{3}^{3} \frac{k}{k} \int_{2}^{3} \frac{k}{k} \int_{2$$



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.36 CONTINUED**

Along DE:

Along DE:  

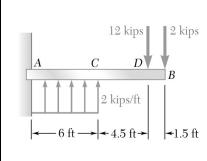
$$M = -162 \text{ N} \cdot \text{m} + (810 \text{ N})x_3$$

$$M = 162 \text{ N} \cdot \text{m} + (x_3 = 0.4)$$
Along EB:

540N1

M(Lx2 SHON

 $\Sigma F_y = 0: V - 540 \text{ N} = 0$  V = 540 N $(\Sigma M_L = 0: M + x_2 (540 \text{ N}) = 0 \qquad M = -540 \text{ N} x_2$  $M = -162 \text{ N} \cdot \text{m} \text{ at } E \quad (x_2 = 0.3 \text{ m})$  $|V|_{\text{max}} = 810 \text{ N on } DE \blacktriangleleft$ (b) From diagrams  $|M|_{\text{max}} = 162.0 \text{ N} \cdot \text{m at } D \text{ and } E \blacktriangleleft$ 



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

# SOLUTION $\begin{array}{c} 12 kips & 2kips \\ 2kips & 2kips \\ 12 kips & 2kips \\ 13 kips & 15 kip \\ 2kips & 2kips \\ 14 & 15 kip \\ 2kips & 15 ki$

 $\Sigma F_v = 0: A_v + (6 \text{ ft})(2 \text{ kips/ft}) - 12 \text{ kips} - 2 \text{ kips} = 0$  $A_v = 2 \text{ kips}^{\dagger}$  $(\Sigma M_A = 0: M_A + (3 \text{ ft})(6 \text{ ft})(2 \text{ kips/ft})$ -(10.5 ft)(12 kips) - (12 ft)(2 kips) = 0 $\mathbf{M}_A = 114 \text{ kip} \cdot \text{ft}$ 114 kip from A x J M 2 kips 2 kips / Ft V y Along AC:  $\sum F_y = 0: 2 \text{ kips} + x(2 \text{ kips/ft}) - V = 0$ V = 2 kips + (2 kips/ft) xV = 14 kips at C (x = 6 ft)  $(\Sigma M_I = 0: 114 \text{ kip} \cdot \text{ft} - x(2 \text{ kips}))$  $-\frac{x}{2}x(2 \text{ kips/ft}) + M = 0$  $M = (1 \operatorname{kip/ft})x^2 + (2 \operatorname{kips})x - 114 \operatorname{kip} \cdot \operatorname{ft}$  $M = -66 \operatorname{kip} \cdot \operatorname{ft} \operatorname{at} C (x = 6 \operatorname{ft})$ M (K ZI V 1.5ft V Along CD:  $\Sigma F_{v} = 0: V - 12 \text{ kips} - 2 \text{ kips} = 0$  V = 14 kips $(\Sigma M_k = 0: -M - x_1(12 \text{ kips}) - (1.5 \text{ ft} + x_1)(2 \text{ kips}) = 0$ 

#### **PROBLEM 7.37 CONTINUED**

$$M = -3 \operatorname{kip} \cdot \operatorname{ft} - (14 \operatorname{kips}) x_{1}$$

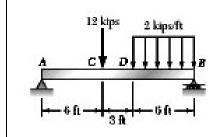
$$M = -66 \operatorname{kip} \cdot \operatorname{ft} \operatorname{at} C \quad (x_{1} = 4.5 \operatorname{ft})$$
Along DB:
$$M = -2 \operatorname{kips} = 0 \qquad V = +2 \operatorname{kips}$$

$$(\Sigma M_{L} = 0: -M - 2 \operatorname{kip} x_{3} = 0$$

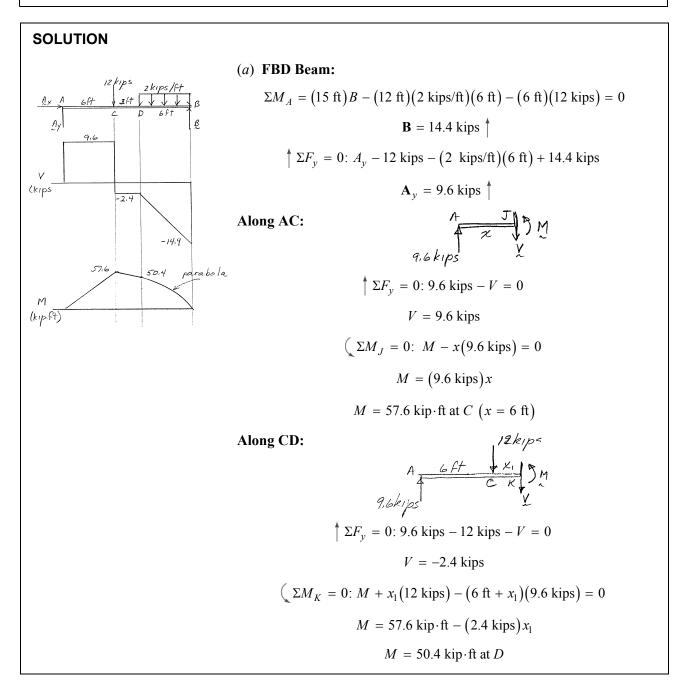
$$M = -(2 \operatorname{kips}) x_{3}$$

$$M = -3 \operatorname{kip} \cdot \operatorname{ft} \operatorname{at} D \quad (x = 1.5 \operatorname{ft})$$
(b) From diagrams:
$$|V|_{\max} = 14.00 \operatorname{kips} \operatorname{on} CD \blacktriangleleft$$

$$|M|_{\max} = 114.0 \operatorname{kip} \cdot \operatorname{ft} \operatorname{at} A \blacktriangleleft$$



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.38 CONTINUED**

Along DB:

$$\sum_{k=1}^{N} \frac{2^{k} \mu s^{k} t^{*}}{(1 + k^{*})^{k} s^{*}}$$

$$\sum_{k=1}^{N} F_{y} = 0: \ V - x_{3}(2 \text{ kips/ft}) + 14.4 \text{ kips} = 0$$

$$V = -14.4 \text{ kips} + (2 \text{ kips/ft})x_{3}$$

$$V = -2.4 \text{ kips at } D$$

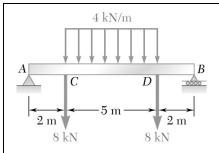
$$\left(\sum_{k=1}^{N} D_{k} + \frac{x_{3}}{2}(2 \text{ kips/ft})(x_{3}) - x_{3}(14.4 \text{ kips}) = 0$$

$$M = (14.4 \text{ kips})x_{3} - (1 \text{ kip/ft})x_{3}^{2}$$

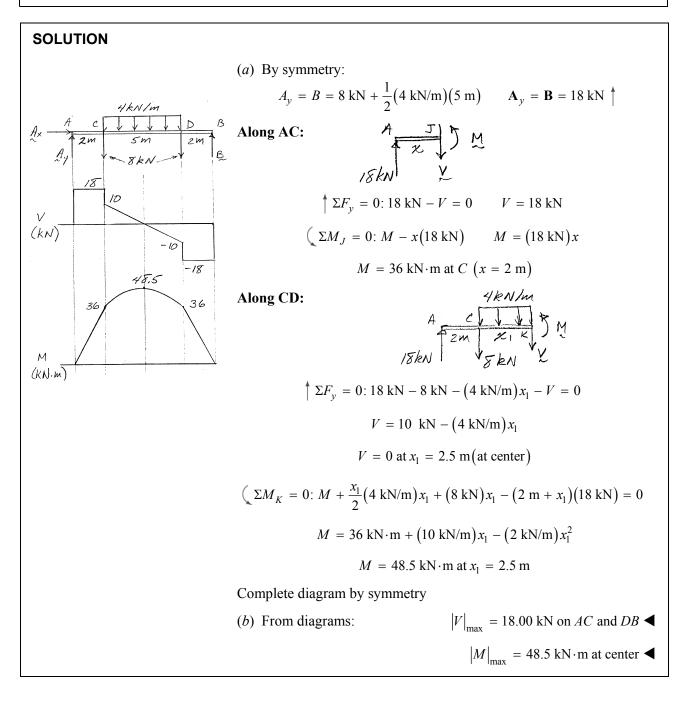
$$M = 50.4 \text{ kip} \cdot \text{ft} \text{ at } D (x_{3} = 6 \text{ ft})$$

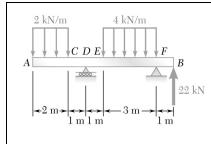
$$(b) \text{ From diagrams:} \qquad |V|_{\text{max}} = 14.40 \text{ kips at } B \blacktriangleleft$$

$$|M|_{\text{max}} = 57.6 \text{ kip} \cdot \text{ft} \text{ at } C \blacktriangleleft$$

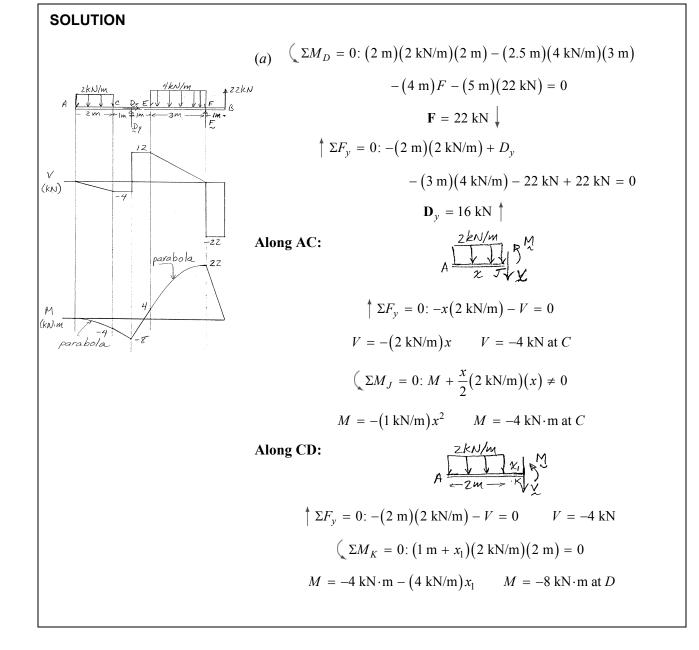


For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.





For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.40 CONTINUED**

Along DE:

$$A = 2m = K_{Y}$$

$$\uparrow \Sigma F_y = 0: -(2 \text{ kN/m})(2 \text{ m}) + 16 \text{ kN} - V = 0 \qquad V = 12 \text{ kN}$$
$$(\Sigma M_L = 0: M - x_2(16 \text{ kN}) + (x_2 + 2 \text{ m})(2 \text{ kN/m})(2 \text{ m}) = 0$$
$$M = -8 \text{ kN} \cdot \text{m} + (12 \text{ kN})x_2 \qquad M = 4 \text{ kN} \cdot \text{m} \text{ at } E$$

Along EF:

$$M = \frac{\frac{4kN}{m}}{22kN}$$

$$\sum F_y = 0: V - x_4 (4 \text{ kN/m}) - 22 \text{ kN} + 22 \text{ kN} = 0$$

$$V = (4 \text{ kN/m})x_4 \qquad V = 12 \text{ kN at } E$$

$$\sum M_0 = 0: M + \frac{x_4}{2} (4 \text{ kN/m})x_4 - (1 \text{ m})(22 \text{ kN}) = 0$$

$$M = 22 \text{ kN} \cdot \text{m} - (2 \text{ kN/m})x_4^2 \qquad M = 4 \text{ kN} \cdot \text{m at } E$$

Along FB:

$$V = 22 \text{ kN}$$

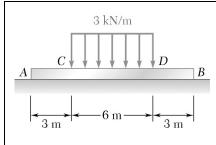
$$M = 22 \text{ kN} = 0 \qquad V = 22 \text{ kN}$$

$$(\Sigma M_N = 0: M - x_3(22 \text{ kN}) = 0$$

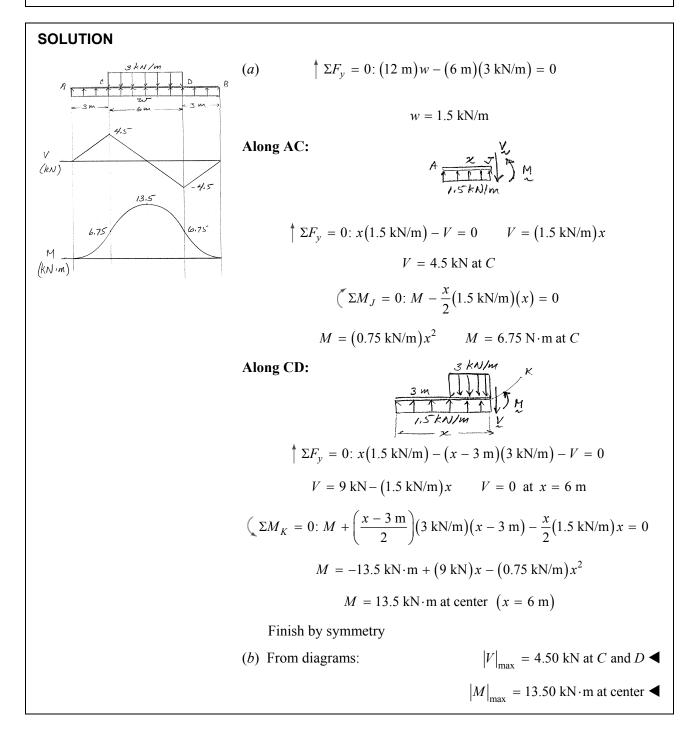
$$M = (22 \text{ kN})x_3$$

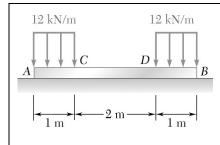
$$M = 22 \text{ kN} \cdot \text{m at } F$$
(b) From diagrams:
$$|V|_{\text{max}} = 22.0 \text{ kN on } FB \blacktriangleleft$$

$$|M|_{\text{max}} = 22.0 \text{ kN} \cdot \text{m at } F$$

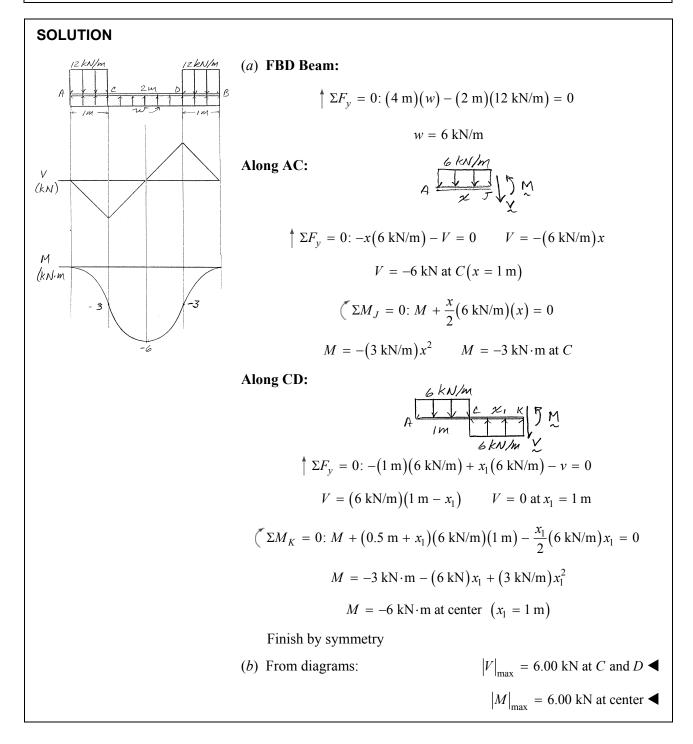


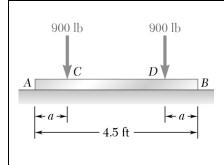
Assuming the upward reaction of the ground on beam AB to be uniformly distributed, (a) draw the shear and bending-moment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



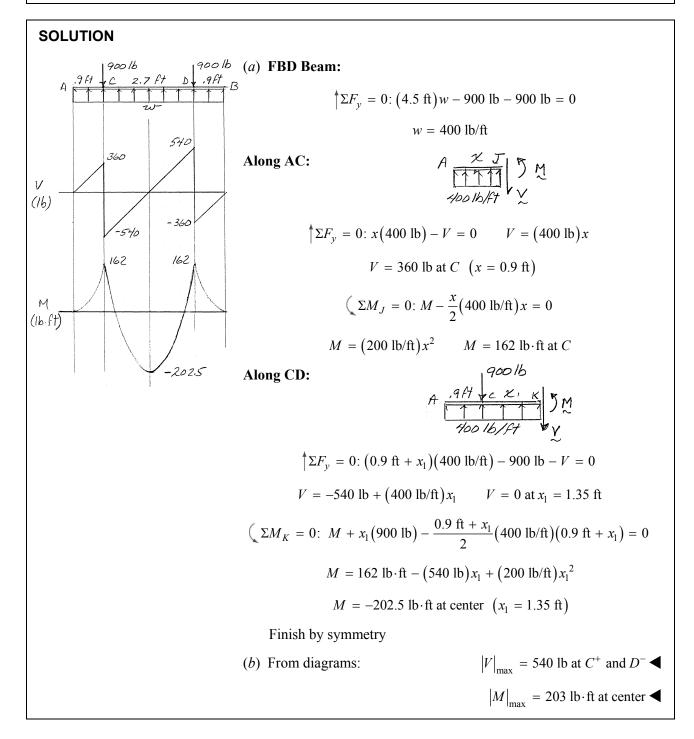


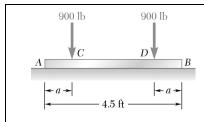
Assuming the upward reaction of the ground on beam AB to be uniformly distributed, (a) draw the shear and bending-moment diagrams, (b) determine the maximum absolute values of the shear and bending moment.



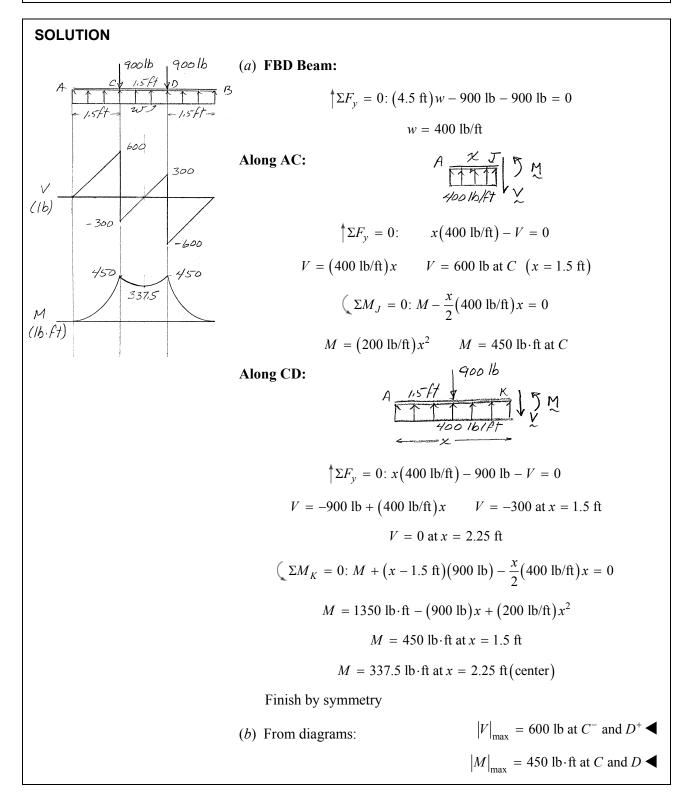


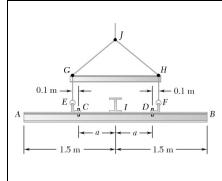
Assuming the upward reaction of the ground on beam *AB* to be uniformly distributed and knowing that a = 0.9 ft, (*a*) draw the shear and bending-moment diagrams, (*b*) determine the maximum absolute values of the shear and bending moment.





Solve Prob. 7.43 assuming that a = 1.5 ft.





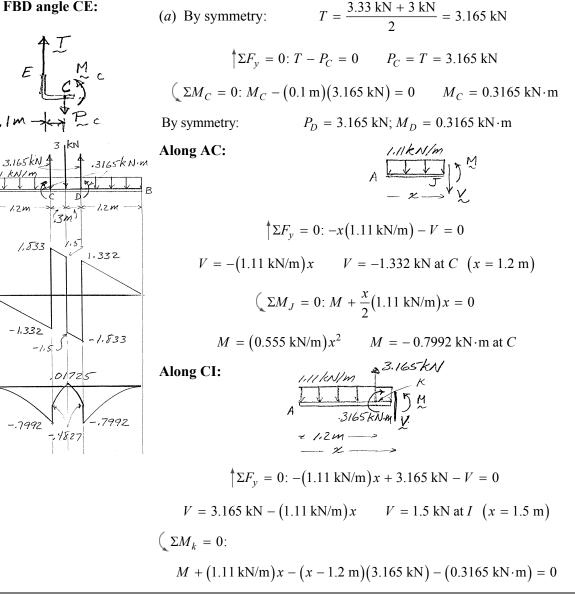
Two short angle sections CE and DF are bolted to the uniform beam AB of weight 3.33 kN, and the assembly is temporarily supported by the vertical cables EG and FH as shown. A second beam resting on beam AB at I exerts a downward force of 3 kN on AB. Knowing that a = 0.3 m and neglecting the weight of the ngle sections, (a) draw the shear and bending-moment diagrams for beam AB, (b) determine the maximum absolute values of the shear and bending moment in the beam.

## SOLUTION FBD angle CE:

V

M (KN·M)

(KN)



#### **PROBLEM 7.45 CONTINUED**

 $M = 3.4815 \text{ kN} \cdot \text{m} + (3.165 \text{ kN})x - (0.555 \text{ kN/m})x^2$ 

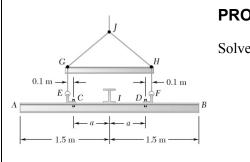
 $M = -0.4827 \text{ kN} \cdot \text{m at } C$   $M = 0.01725 \text{ kN} \cdot \text{m at } I$ 

Note: At *I*, the downward 3 kN force will reduce the shear *V* by 3 kN, from +1.5 kN to -1.5 kN, with no change in *M*. From *I* to *B*, the diagram can be completed by symmetry.

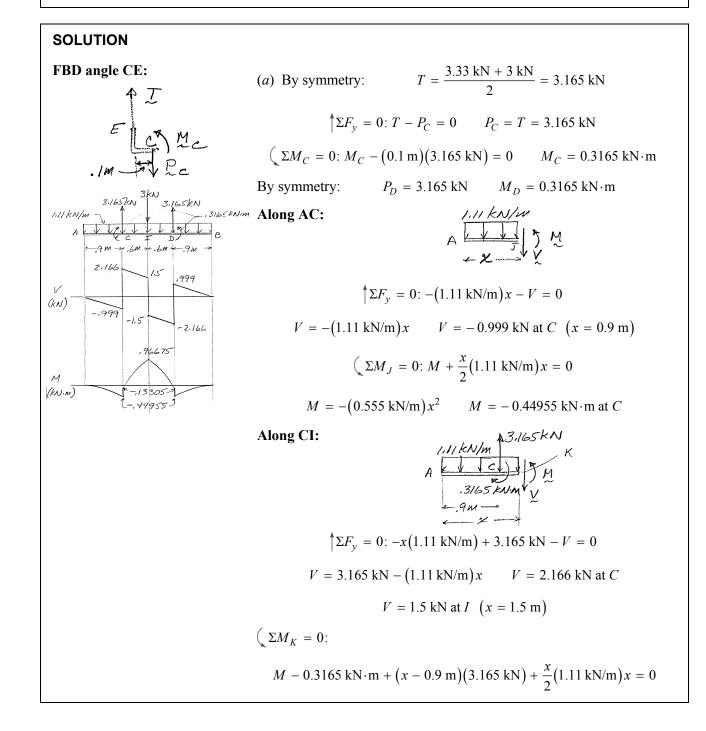
(*b*) From diagrams:

 $|V|_{\text{max}} = 1.833 \text{ kN} \text{ at } C \text{ and } D \blacktriangleleft$ 

 $|M|_{\text{max}} = 799 \text{ N} \cdot \text{m at } C \text{ and } D \blacktriangleleft$ 

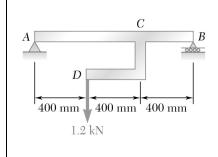


Solve Prob. 7.45 when a = 0.6 m.

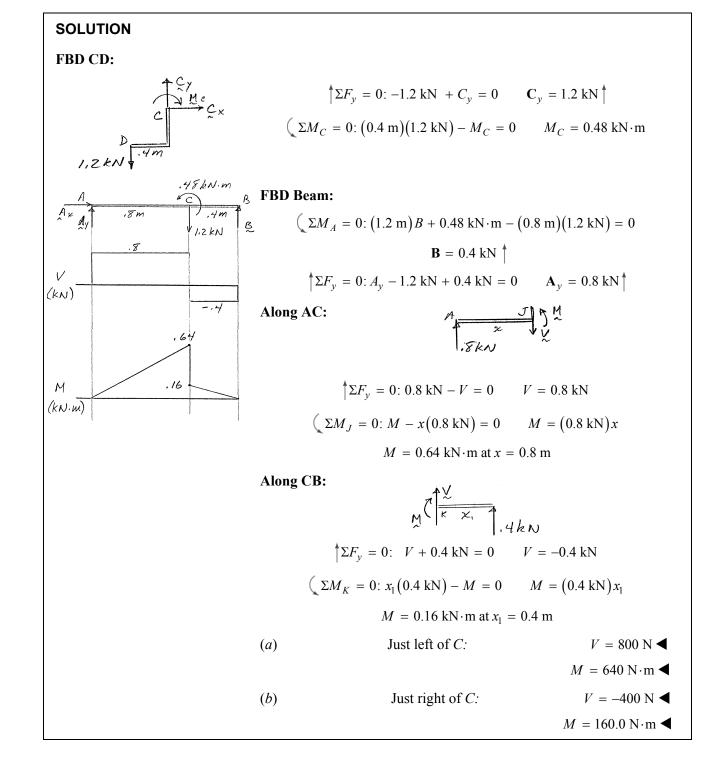


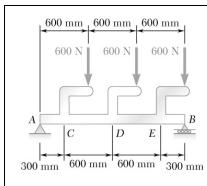
#### **PROBLEM 7.46 CONTINUED**

 $M = -2.532 \text{ kN} \cdot \text{m} + (3.165 \text{ kN})x - (0.555 \text{ kN/m})x^2$  $M = -0.13305 \text{ kN} \cdot \text{m} \text{ at } C \qquad M = 0.96675 \text{ kN} \cdot \text{m} \text{ at } I$ Note: At *I*, the downward 3 kN force will reduce the shear *V* by 3 kN, from +1.5 kN to -1.5 kN, with no change in *M*. From *I* to *B*, the diagram can be completed by symmetry. (b) From diagrams:  $|V|_{\text{max}} = 2.17 \text{ kN at } C \text{ and } D \blacktriangleleft$  $|M|_{\text{max}} = 967 \text{ N} \cdot \text{m at } I \blacktriangleleft$ 

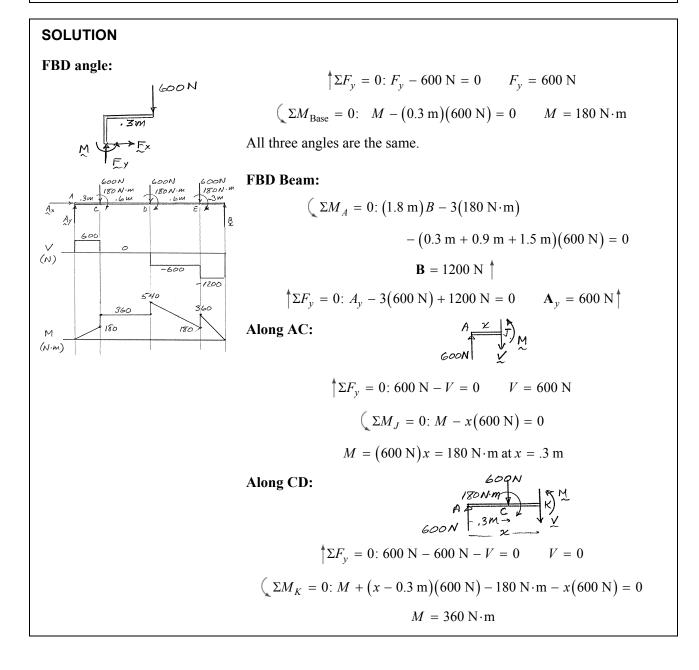


Draw the shear and bending-moment diagrams for the beam AB, and determine the shear and bending moment (*a*) just to the left of *C*, (*b*) just to the right of *C*.





Draw the shear and bending-moment diagrams for the beam AB, and determine the maximum absolute values of the shear and bending moment.



#### **PROBLEM 7.48 CONTINUED**

Along DE:

$$\Sigma F_{y} = 0: V - 600 \text{ N} + 1200 \text{ N} = 0 \qquad V = -600 \text{ N}$$

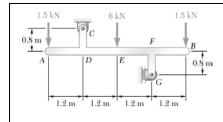
$$(\Sigma M_{N} = 0: -M - 180 \text{ N} \cdot \text{m} - x_{2}(600 \text{ N}) + (x_{2} + 0.3 \text{ m})(1200 \text{ N}) = 0$$

$$M = 180 \text{ N} \cdot \text{m} + (600 \text{ N})x_{2} = 540 \text{ N} \cdot \text{m} \text{ at } \text{D}, x_{2} = 0.6 \text{ m}$$

$$M = 180 \text{ N} \cdot \text{m} \text{ at } \text{E} (x_{2} = 0)$$

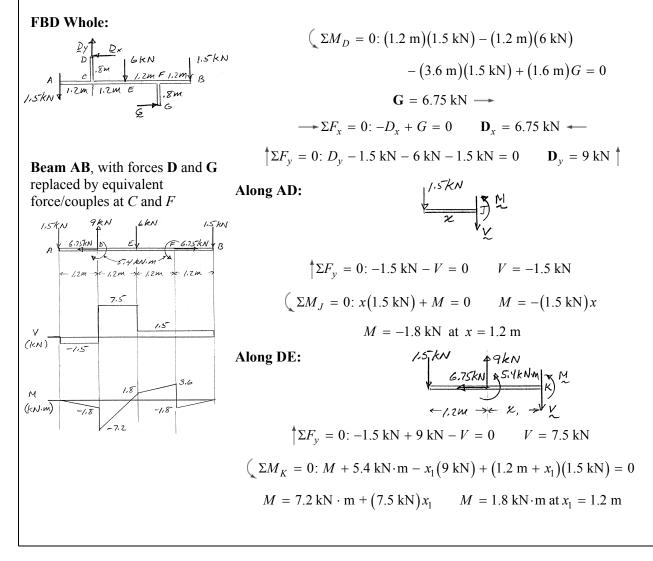
Along EB:

$$\begin{split} & \left| \Sigma F_y = 0; V + 1200 \text{ N} = 0 \quad V = -1200 \text{ N} \right| \\ & \left( \Sigma M_L = 0; x_1 (1200 \text{ N}) - M = 0 \quad M = (1200 \text{ N}) x_1 \right) \\ & M = 360 \text{ N} \cdot \text{m at } x_1 = 0.3 \text{ m} \\ & \text{From diagrams:} \qquad \left| V \right|_{\text{max}} = 1200 \text{ N on } EB \\ & \left| M \right|_{\text{max}} = 540 \text{ N} \cdot \text{m at } D^+ \end{split}$$

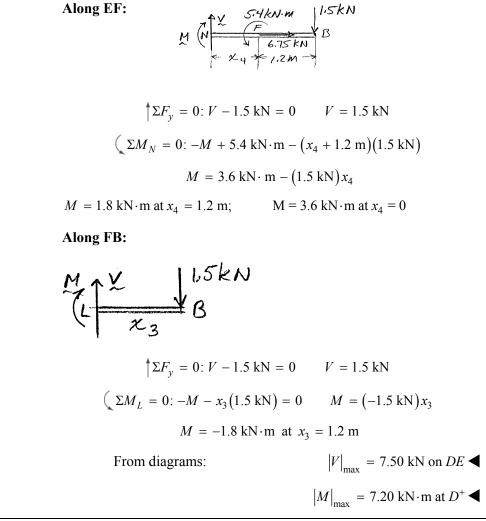


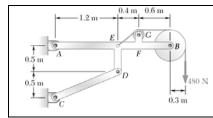
Draw the shear and bending-moment diagrams for the beam AB, and determine the maximum absolute values of the shear and bending moment.

#### SOLUTION



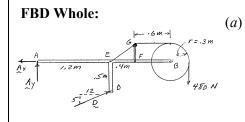
#### **PROBLEM 7.49 CONTINUED**





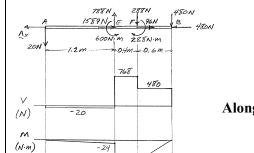
Neglecting the size of the pulley at G, (a) draw the shear and bending-moment diagrams for the beam AB, (b) determine the maximum absolute values of the shear and bending moment.

#### SOLUTION



**Beam AB** with pulley forces and Along AE force at D replaced by equivalent force-couples at B, F, E

-288 316.8



-624

$$\begin{aligned} & \left( \Sigma M_A = 0: (0.5 \text{ m}) \frac{12}{13} D + (1.2 \text{ m}) \frac{5}{13} D - (2.5 \text{ m}) (480 \text{ N}) = 0 \\ D = 1300 \text{ N} \\ & \uparrow \Sigma F_y = 0: A_y + \frac{5}{13} (1300 \text{ N}) - 480 \text{ N} = 0 \\ A_y = -20 \text{ N} \qquad \mathbf{A}_y = 20 \text{ N} \right) \end{aligned}$$
Along AE:  

$$\begin{aligned} & \int \Sigma F_y = 0: -20 \text{ N} - V = 0 \qquad V = -20 \text{ N} \\ & \left( \Sigma M_J = 0: M + x (20 \text{ N}) \qquad M = -(20 \text{ N}) x \\ M = -24 \text{ N} \cdot \text{m at } x = 1.2 \text{ m} \end{aligned}$$
Along EF:  

$$\begin{aligned} & \bigvee_{M = -24 \text{ N} \cdot \text{m at } x = 1.2 \text{ m} \\ & \bigwedge_{M = -24 \text{ N} \cdot \text{m at } x = 1.2 \text{ m} \end{aligned}$$

$$\begin{aligned} & \int \Sigma F_y = 0: V - 288 \text{ N} - 480 \text{ N} = 0 \qquad V = 768 \text{ N} \\ & \left( \Sigma M_L = 0: -M - x_2 (288 \text{ N}) - (28.8 \text{ N} \cdot \text{m}) - (x_2 + 0.6 \text{ m}) (480 \text{ N}) = 0 \\ & M = -316.8 \text{ N} \cdot \text{m} - (768 \text{ N}) x_2 \end{aligned}$$

 $M = -316.8 \text{ N} \cdot \text{m}$  at  $x_2 = 0$ ;  $M = -624 \text{ N} \cdot \text{m}$  at  $x_2 = 0.4 \text{ m}$ 

Along FB:

M K Z 480N

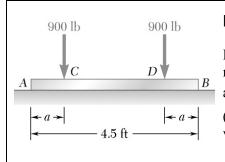
$$\uparrow \Sigma F_y = 0: V - 480 \text{ N} = 0 \qquad V = 480 \text{ N}$$
$$(\Sigma M_K = 0: -M - x_1 (480 \text{ N}) = 0 \qquad M = -(480 \text{ N}) x_1$$
$$M = -288 \text{ N} \cdot \text{m at } x_1 = 0.6 \text{ m}$$

#### **PROBLEM 7.50 CONTINUED**

(*b*) From diagrams:

 $|V|_{\text{max}} = 768 \text{ N along } EF \blacktriangleleft$ 

$$|M|_{\text{max}} = 624 \text{ N} \cdot \text{m at } E^+$$



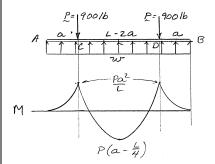
For the beam of Prob. 7.43, determine (a) the distance a for which the maximum absolute value of the bending moment in the beam is as small as possible, (b) the corresponding value of  $|M|_{\text{max}}$ .

(*Hint:* Draw the bending-moment diagram and then equate the absolute values of the largest positive and negative bending moments obtained.)

 $\sum F_v = 0: Lw - 2P = 0$ 

#### SOLUTION



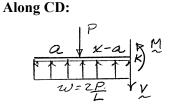


 $w = 2\frac{P}{L}$   $(\sum M_J = 0: M - \frac{x}{2}\left(\frac{2P}{L}x\right) = 0 \qquad M = \frac{P}{L}x^2$   $M = \frac{P}{L}a^2 \text{ at } x = a$   $(\sum M_K = 0: M + (x - a)P - \frac{x}{2}\left(\frac{2P}{L}x\right) = 0$   $M = P(a - x) + \frac{P}{L}x^2 = \frac{Pa^2}{L} \qquad \text{at } x = a$   $M = P\left(a - \frac{L}{4}\right) \text{ at } x = \frac{L}{2}$ 



Along AC:

AF



This is M min by symmetry–see moment diagram completed by symmetry.

For minimum  $|M|_{\text{max}}$ , set  $M_{\text{max}} = -M_{\text{min}}$ :

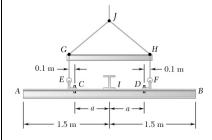
$$P\frac{a^2}{L} = -P\left(a - \frac{L}{4}\right)$$
$$a^2 + La - \frac{L^2}{4} = 0$$

or

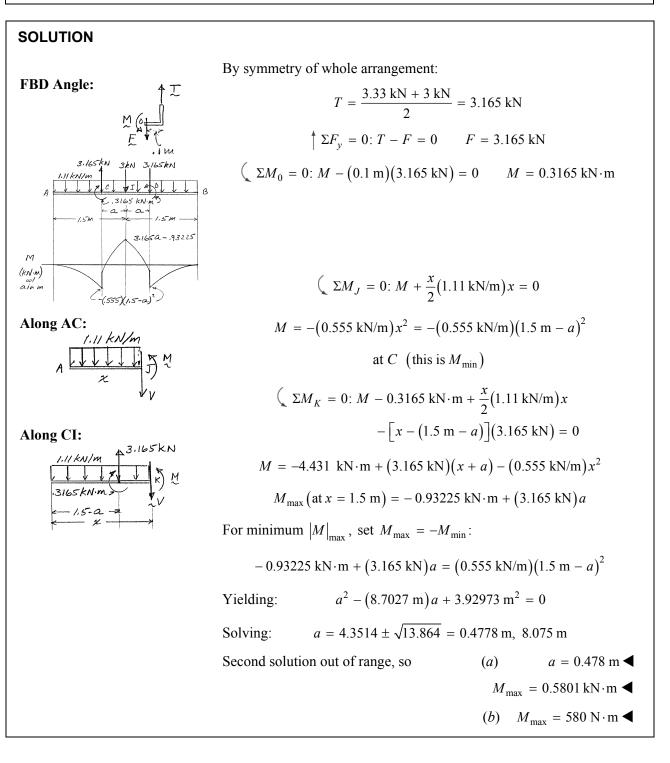
$$a = \frac{-1 \pm \sqrt{2}}{2}L$$

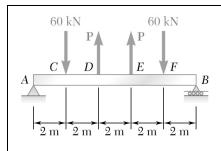
Solving:

Positive answer (a)  $a = 0.20711L = 0.932 \text{ ft} \blacktriangleleft$ (b)  $|M|_{\text{max}} = 0.04289PL = 173.7 \text{ lb} \cdot \text{ft} \blacktriangleleft$ 



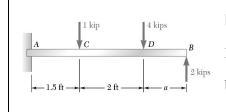
For the assembly of Prob. 7.45, determine (a) the distance a for which the maximum absolute value of the bending moment in beam AB is as small as possible, (b) the corresponding value of  $|M|_{\text{max}}$ . (See hint for Prob. 7.51.)





For the beam shown, determine (a) the magnitude P of the two upward forces for which the maximum value of the bending moment is as small as possible, (b) the corresponding value of  $|M|_{\text{max}}$ . (See hint for Prob. 7.51.)

# SOLUTION By symmetry: $A_v = B = 60 \text{ kN} - P$ N P R GOKN 2m 2m 2m 2m B D E F B Along AC: A T JM $(\Sigma M_J = 0: M - x(60 \text{ kN} - P) = 0 \qquad M = (60 \text{ kN} - P)x$ 120-2P 120-2P $M = 120 \text{ kN} \cdot \text{m} - (2 \text{ m})P$ at x = 2 mΜ (KN·m Along CD: ZM K M Pin KN) 120-4P $(\Sigma M_K = 0: M + (x - 2 m)(60 kN) - x(60 kN - P) = 0$ $M = 120 \text{ kN} \cdot \text{m} - Px$ $M = 120 \text{ kN} \cdot \text{m} - (4 \text{ m})P$ at x = 4 mAlong DE: Zm Zm LM zm Zm LM $(\Sigma M_L = 0: M - (x - 4 m)P + (x - 2 m)(60 kN)$ -x(60 kN - P) = 0 $M = 120 \text{ kN} \cdot \text{m} - (4 \text{ m})P \quad \text{(const)}$ Complete diagram by symmetry For minimum $|M|_{\text{max}}$ , set $M_{\text{max}} = -M_{\text{min}}$ $120 \text{ kN} \cdot \text{m} - (2 \text{ m})P = -[120 \text{ kN} \cdot \text{m} - (4 \text{ m})P]$ P = 40.0 kN*(a)* (b) $|M|_{\text{max}} = 40.0 \text{ kN} \cdot \text{m} \blacktriangleleft$ $M_{\min} = 120 \text{ kN} \cdot \text{m} - (4 \text{ m})P$

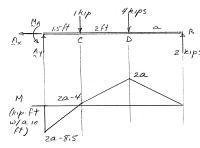


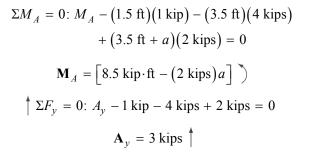
1

For the beam and loading shown, determine (*a*) the distance *a* for which the maximum absolute value of the bending moment in the beam is as small as possible, (*b*) the corresponding value of  $|M|_{\text{max}}$ . (See hint for Prob. 7.51.)

# SOLUTION

## **FBD Beam:**





Along AC:

Along DB:

4 kips

$$\left( \sum M_J = 0 : M - x(3 \text{ kips}) + 8.5 \text{ kip} \cdot \text{ft} - (2 \text{ kips})a = 0 \right)$$

$$M = (3 \text{ kips})x + (2 \text{ kips})a - 8.5 \text{ kip} \cdot \text{ft}$$

$$M = (2 \text{ kips})a - 4 \text{ kip} \cdot \text{ft} \text{ at } C(x = 1.5 \text{ ft})$$

$$M = (2 \text{ kips})a - 8.5 \text{ kip} \cdot \text{ft} \text{ at } A(M_{\min})$$

$$\left(\Sigma M_K = 0: -M + x_1(2 \text{ kips}) = 0 \qquad M = (2 \text{ kips})x_1$$
$$M = (2 \text{ kips})a \text{ at } D$$

$$\sum M_{L} = 0: (x_{2} + a)(2 \text{ kips}) - x_{2}(4 \text{ kips}) - M = 0$$

$$M = (2 \text{ kips})a - (2 \text{ kips})x_{2}$$

$$M = (2 \text{ kips})a - 4 \text{ kip} \cdot \text{ft at } C \text{ (see above)}$$
For minimum  $|M|_{\text{max}}$ , set  $M_{\text{max}}(\text{at } D) = -M_{\text{min}}(\text{at } A)$ 

$$(2 \text{ kips})a = -[(2 \text{ kips})a - 8.5 \text{ kip} \cdot \text{ft}]$$

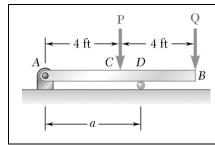
$$4a = 8.5 \text{ ft} \quad a = 2.125 \text{ ft}$$

$$(a) \quad a = 2.13 \text{ ft} \blacktriangleleft$$
So
$$M_{\text{max}} = (2 \text{ kips})a = 4.25 \text{ kip} \cdot \text{ft}$$

(b)  $|M|_{\text{max}} = 4.25 \text{ kip} \cdot \text{ft} \blacktriangleleft$ 

Along CD:

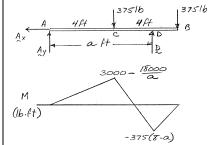
M



Knowing that P = Q = 375 lb, determine (a) the distance a for which the maximum absolute value of the bending moment in beam AB is as small as possible, (b) the corresponding value of  $|M|_{\text{max}}$ . (See hint for Prob. 7.51.)

# SOLUTION

FBD Beam:

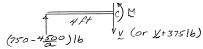


$$\sum M_{A} = 0: (a \text{ ft})D - (4 \text{ ft})(375 \text{ lb}) - (8 \text{ ft})(375 \text{ lb}) = 0$$
$$\mathbf{D} = \frac{4500}{a} \text{ lb} \uparrow$$
$$\uparrow \Sigma F_{y} = 0: A_{y} - 2(375 \text{ lb}) + \frac{4500}{a} \text{ lb} = 0$$
$$\mathbf{A}_{y} = \left(750 - \frac{4500}{a}\right) \text{lb} \uparrow$$

It is apparent that M = 0 at A and B, and that all segments of the M diagram are straight, so the max and min values of M must occur at C and D

Segment AC:

**Segment DB:** 



$$\sum M_{C} = 0: M - (4 \text{ ft}) \left( 750 - \frac{4500}{a} \right) \text{lb} = 0$$
$$M = \left( 3000 - \frac{18000}{a} \right) \text{lb} \cdot \text{ft}$$
$$\sum M_{D} = 0: -\left[ (8 - a) \text{ft} \right] (375 \text{ lb}) - M = 0$$
$$M = -375(8 - a) \text{lb} \cdot \text{ft}$$

For minimum  $|M|_{\text{max}}$ , set  $M_{\text{max}} = -M_{\text{min}}$ 

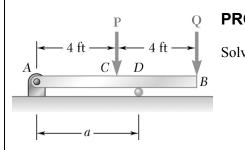
So

$$3000 - \frac{18000}{a} = 375(8 - a)$$
$$a^{2} = 48 \qquad a = 6.9282 \text{ ft}$$
(a)

a = 6.93 ft

$$M_{\rm max} = 375(8-a) = 401.92 \, \rm lb \cdot ft$$

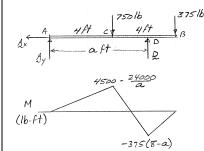
(b) 
$$|M|_{\text{max}} = 402 \text{ lb} \cdot \text{ft} \blacktriangleleft$$



Solve Prob. 7.55 assuming that P = 750 lb and Q = 375 lb.

# SOLUTION

**FBD Beam:** 



<u>4 *Ft*</u> *c*) M *y* (*cr y* + 750 *l*b)

 $\sum M_D = 0: -(a \text{ ft})A_y + [(a-4)\text{ft}](750 \text{ lb})$  $-\left\lceil \left(8-a\right) \mathrm{ft} \right\rceil \left(375 \ \mathrm{lb}\right) = 0$  $\mathbf{A}_{y} = \left(1125 - \frac{6000}{a}\right) \mathbf{lb} \uparrow$ 

It is apparent that M = 0 at A and B, and that all segments of the *M*-diagram are straight, so  $M_{\text{max}}$  and  $M_{\text{min}}$  occur at *C* and *D*.

$$\left(\sum M_{C} = 0: M - (4 \text{ ft}) \left(1125 - \frac{6000}{a}\right) \text{lb} = 0\right)$$

$$M = \left(4500 - \frac{24000}{a}\right) \text{lb} \cdot \text{ft}$$

$$\left(\sum M_{D} = 0: -M - \left[(8 - a) \text{ft}\right](375 \text{ lb}) = 0\right)$$

$$M = -375(8 - a) \text{lb} \cdot \text{ft}$$
For minimum  $M_{\text{max}}$ , set  $M_{\text{max}} = -M_{\text{min}}$ 

$$4500 - \frac{24000}{a} = 375(8 - a)$$

$$a^{2} + 4a - 64 = 0 \qquad a = -2 \pm \sqrt{68} \text{ (need +)}$$

$$a = 6.2462 \text{ ft} \qquad (a) \qquad a = 6.25 \text{ ft} \blacktriangleleft$$

*(a)* 

Segment DB:

**Segment AC:** 

(1125- 6000

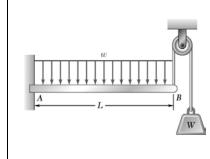
 $\chi(or \chi + D)$ 375 lb M (D

a = 6.2462 ft

Then

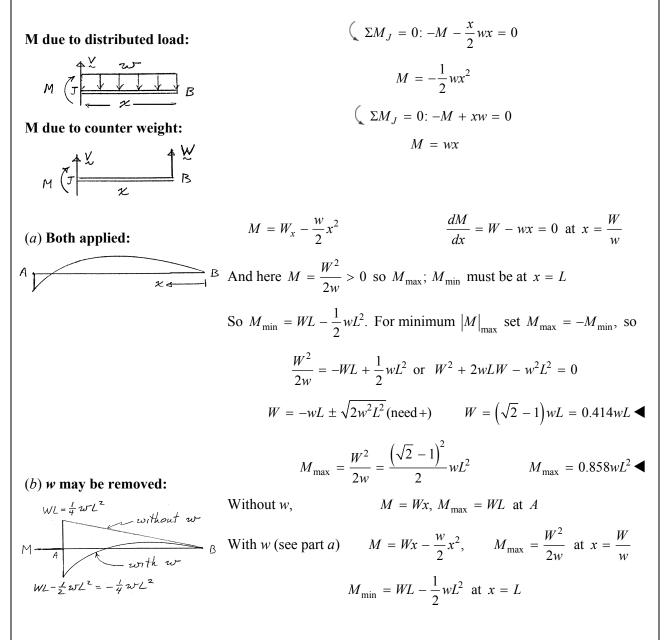
$$M_{\rm max} = 375(8-a) = 657.7 \, \rm lb \cdot ft$$

 $|M|_{\text{max}} = 658 \text{ lb} \cdot \text{ft} \blacktriangleleft$ *(b)* 



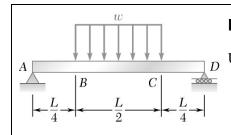
In order to reduce the bending moment in the cantilever beam *AB*, a cable and counterweight are permanently attached at end *B*. Determine the magnitude of the counterweight for which the maximum absolute value of the bending moment in the beam is as small as possible and the corresponding value of  $|M|_{max}$ . Consider (*a*) the case when the distributed load is permanently applied to the beam, (*b*) the more general case when the distributed load may either be applied or removed.

#### SOLUTION



# **PROBLEM 7.57 CONTINUED**

For minimum  $M_{\text{max}}$ , set  $M_{\text{max}} (\text{no } w) = -M_{\text{min}} (\text{with } w)$   $WL = -WL + \frac{1}{2}wL^2 \rightarrow W = \frac{1}{4}wL \rightarrow \qquad M_{\text{max}} = \frac{1}{4}wL^2 \blacktriangleleft$ With  $W = \frac{1}{4}wL \blacktriangleleft$ 



Using the method of Sec. 7.6, solve Prob. 7.29.

## SOLUTION

(*a*) and (*b*)

WL/4

w12 16

V

M

¢

32222

symmetry: 
$$A_y = D = \frac{1}{2} \left( w \frac{L}{2} \right) = \frac{wL}{4}$$
 or  $A_y = \mathbf{D} = \frac{wL}{4}$ 

Shear Diag:

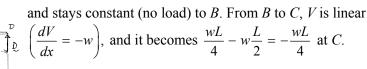
By

L\_\_\_\_\_

- w2/4

202

V jumps to  $A_y = \frac{wL}{4}$  at A,



(Note: V = 0 at center of beam. From C to D, V is again constant.) Moment Diag: M starts at zero at A

and increases linearly  $\left(\frac{dM}{dV} = \frac{wL}{4}\right)$  to *B*.

$$M_B = 0 + \frac{L}{4} \left( \frac{wL}{4} \right) = \frac{wL^2}{16}.$$

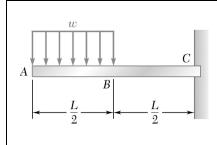
From *B* to *C M* is parabolic

 $\left(\frac{dM}{dx} = V, \text{ which decreases to zero at center and } -\frac{wL}{4} \text{ at } C\right),$ M is maximum at center.  $M_{\text{max}} = \frac{wL^2}{16} + \frac{1}{2} \left(\frac{L}{4}\right) \left(\frac{wL}{4}\right)$ Then, M is linear with  $\frac{dM}{dy} = -\frac{wL}{4}$  to D

$$M_{D} = 0$$

$$|V|_{\max} = \frac{wL}{4} \blacktriangleleft$$
$$|M|_{\max} = \frac{3wL^2}{32} \blacktriangleleft$$

Notes: Symmetry could have been invoked to draw second half. Smooth transitions in *M* at *B* and *C*, as no discontinuities in *V*.



Using the method of Sec. 7.6, solve Prob. 7.30.

# SOLUTION

(a) and (b)

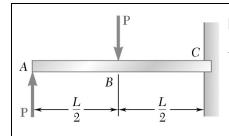
A

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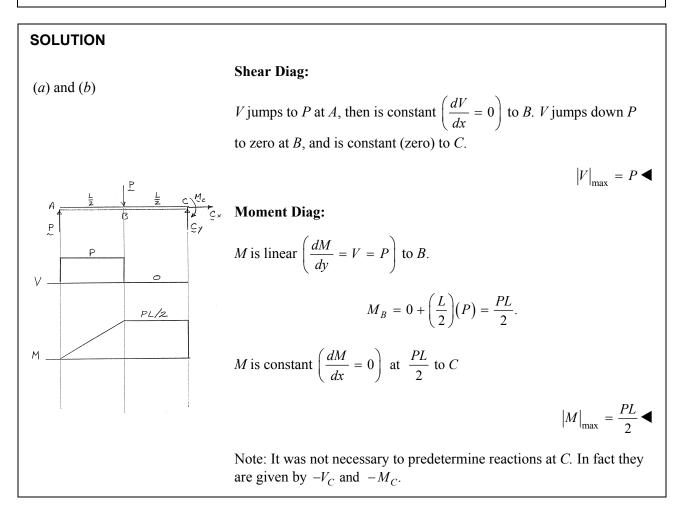
M

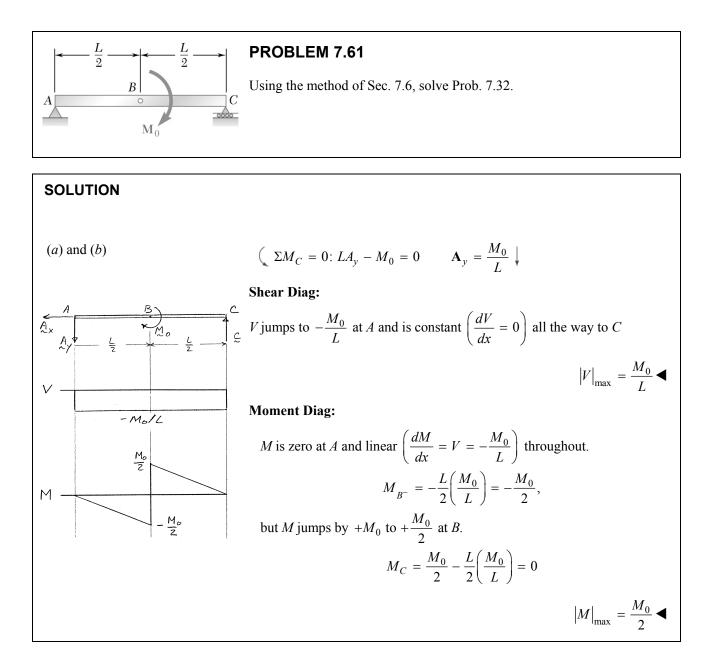
Shear Diag: V = 0 at A and is linear  $\left(\frac{dV}{dx} = -w\right)$  to  $-w\left(\frac{L}{2}\right) = -\frac{wL}{2}$  at *B*. *V* is constant  $\left(\frac{dV}{dx} = 0\right)$  from *B* to *C*.  $|V|_{\text{max}} = \frac{wL}{2} \blacktriangleleft$ e, **Moment Diag:** M = 0 at A and is parabolic  $\left(\frac{dM}{dx}\right)$  decreasing with V to B. - wL/2  $M_B = \frac{1}{2} \left( \frac{L}{2} \right) \left( -\frac{wL}{2} \right) = -\frac{wL^2}{8}$  $-\frac{\omega L^2}{8}$ -<u>3wi</u> From *B* to *C*, *M* is linear  $\left(\frac{dM}{dx} = -\frac{wL}{2}\right)$  $M_{C} = -\frac{wL^{2}}{8} - \left(\frac{L}{2}\right)\left(\frac{wL}{2}\right) = -\frac{3wL^{2}}{8}$  $\left|M\right|_{\max} = \frac{3wL^2}{8}$ Notes: Smooth transition in *M* at *B*, as no discontinuity in *V*. It was not necessary to predetermine reactions at C.

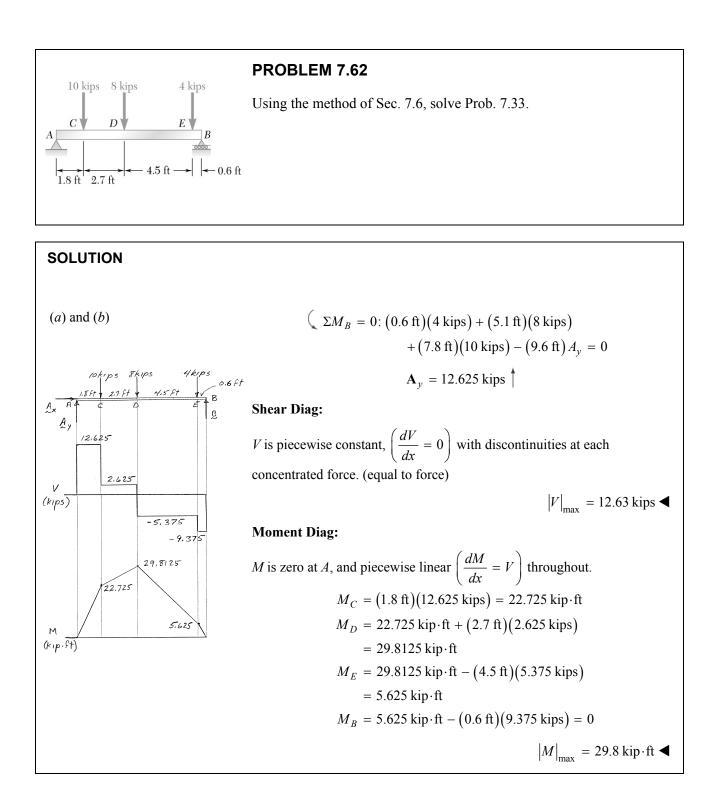
In fact they are given by  $-V_C$  and  $-M_C$ .

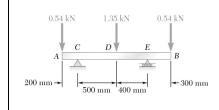


Using the method of Sec. 7.6, solve Prob. 7.31.







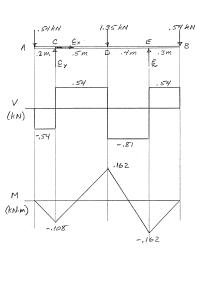


Using the method of Sec. 7.6, solve Prob. 7.36.

# SOLUTION

(*a*) and (*b*)

#### FBD Beam:



# $\sum M_E = 0: (1.1 \text{ m})(0.54 \text{ kN}) - (0.9 \text{ m})C_y$ + (0.4 m)(1.35 kN) - (0.3 m)(0.54 kN) = 0 $C_y = 1.08 \text{ kN}$ $\sum F_y = 0: -0.54 \text{ kN} + 1.08 \text{ kN} - 1.35 \text{ kN} + E - 0.54 \text{ kN} = 0$ $\mathbf{E} = 1.35 \text{ kN}$

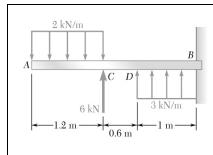
#### Shear Diag:

*V* is piecewise constant,  $\left(\frac{dV}{dx} = 0 \text{ everywhere}\right)$  with discontinuities at each concentrated force. (equal to the force)

$$|V|_{\text{max}} = 810 \text{ N} \blacktriangleleft$$

#### **Moment Diag:**

*M* is piecewise linear starting with  $M_A = 0$   $M_C = 0 - 0.2 \text{ m}(0.54 \text{ kN}) = 0.108 \text{ kN} \cdot \text{m}$   $M_D = 0.108 \text{ kN} \cdot \text{m} + (0.5 \text{ m})(0.54 \text{ kN}) = 0.162 \text{ kN} \cdot \text{m}$   $M_E = 0.162 \text{ kN} \cdot \text{m} - (0.4 \text{ m})(0.81 \text{ kN}) = -0.162 \text{ kN} \cdot \text{m}$   $M_B = 0.162 \text{ kN} \cdot \text{m} + (0.3 \text{ m})(0.54 \text{ kN}) = 0$  $|M|_{\text{max}} = 0.162 \text{ kN} \cdot \text{m} = 162.0 \text{ N} \cdot \text{m} \blacktriangleleft$ 

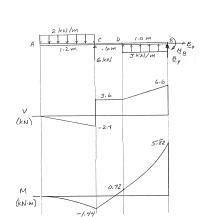






For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

#### Shear Diag:



 $V = 0 \text{ at } A \text{ and linear} \left(\frac{dV}{dx} = -2 \text{ kN/m}\right) \text{ to } C$   $V_C = -1.2 \text{ m}(2 \text{ kN/m}) = -2.4 \text{ kN}.$ At C, V jumps 6 kN to 3.6 kN, and is constant to D. From there, V is
linear  $\left(\frac{dV}{dx} = +3 \text{ kN/m}\right)$  to B  $V_B = 3.6 \text{ kN} + (1 \text{ m})(3 \text{ kN/m}) = 6.6 \text{ kN}$   $|V|_{\text{max}} = 6.60 \text{ kN} \blacktriangleleft$ 

Moment Diag:  

$$M_{A} = 0.$$
From A to C, M is parabolic,  $\left(\frac{dM}{dx} \text{ decreasing with } V\right).$ 

$$M_{C} = -\frac{1}{2}(1.2 \text{ m})(2.4 \text{ kN}) = -1.44 \text{ kN} \cdot \text{m}$$
From C to D, M is linear  $\left(\frac{dM}{dx} = 3.6 \text{ kN}\right)$ 

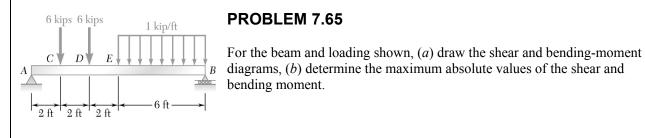
$$M_{D} = -1.44 \text{ kN} \cdot \text{m} + (0.6 \text{ m})(3.6 \text{ kN})$$

$$= 0.72 \text{ kN} \cdot \text{m}.$$
From D to B, M is parabolic  $\left(\frac{dM}{dx} \text{ increasing with } V\right)$ 

$$M_{B} = 0.72 \text{ kN} \cdot \text{m} + \frac{1}{2}(1 \text{ m})(3.6 + 6.6) \text{ kN}$$

$$= 5.82 \text{ kN} \cdot \text{m}$$

Notes: Smooth transition in *M* at *D*. It was unnecessary to predetermine reactions at *B*, but they are given by  $-V_B$  and  $-M_B$ 



6 kips 6 kips

4.5

-1.5

27

H

30

(*a*) and (*b*)

A×

V (kips)

M (kipift)

Ay

# $\sum M_B = 0: (3 \text{ ft})(1 \text{ kip/ft})(6 \text{ ft}) + (8 \text{ ft})(6 \text{ kips}) + (10 \text{ ft})(6 \text{ kips}) - (12 \text{ ft})A_y = 0$ $A_y = 10.5 \text{ kips}^{\dagger}$

#### Shear Diag:

ß

so

-7.5

*V* is piecewise constant from *A* to *E*, with discontinuities at *A*, *C*, and *E* equal to the forces.  $V_E = -1.5$  kips. From *E* to *B*, *V* is linear

$$\left(\frac{dV}{dx} = -1 \,\mathrm{kip/ft}\right),\,$$

 $V_B = -1.5 \text{ kips} - (6 \text{ ft})(1 \text{ kip/ft}) = -7.5 \text{ kips}$ 

$$|V|_{\text{max}} = 10.50 \text{ kips}$$

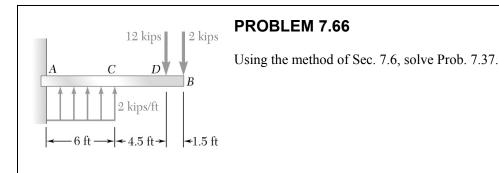
**Moment Diag:**  $M_A = 0$ , then *M* is piecewise linear to *E* 

$$M_{C} = 0 + 2 \operatorname{ft}(10.5 \operatorname{kips}) = 21 \operatorname{kip} \cdot \operatorname{ft}$$

$$M_{D} = 21 \operatorname{kip} \cdot \operatorname{ft} + (2 \operatorname{ft})(4.5 \operatorname{kips}) = 30 \operatorname{kip} \cdot \operatorname{ft}$$

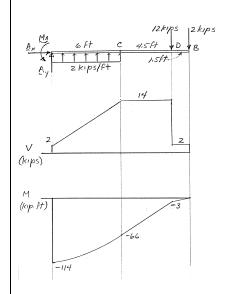
$$M_{E} = 30 \operatorname{kip} \cdot \operatorname{ft} - (2 \operatorname{ft})(1.5 \operatorname{kips}) = 27 \operatorname{kip} \cdot \operatorname{ft}$$
From E to B, M is parabolic  $\left(\frac{dM}{dx} \operatorname{decreasing with} V\right)$ , and
$$M_{B} = 27 \operatorname{kip} \cdot \operatorname{ft} - \frac{1}{2}(6 \operatorname{ft})(1.5 \operatorname{kips} + 7.5 \operatorname{kips}) = 0$$

$$|M|_{\max} = 30.0 \operatorname{kip} \cdot \operatorname{ft} \blacktriangleleft$$



(*a*) and (*b*)

#### FBD Beam:



 $\uparrow \Sigma F_y = 0: A_y + (6 \text{ ft})(2 \text{ kips/ft}) - 12 \text{ kips} - 2 \text{ kips} = 0$  $A_y = 2 \text{ kips} \uparrow$  $(\Sigma M_A = 0: M_A + (3 \text{ ft})(2 \text{ kips/ft})(6 \text{ ft}) - (10.5 \text{ ft})(12 \text{ kips}) - (12 \text{ ft})(2 \text{ kips}) = 0$ 

 $\mathbf{M}_A = 114 \text{ kip} \cdot \text{ft}$ 

#### **Shear Diag:**

$$V_A = A_y = 2$$
 kips. Then V is linear  $\left(\frac{dV}{dx} = 2$  kips/ft $\right)$  to C, where  
 $V_C = 2$  kips + (6 ft)(2 kips/ft) = 14 kips.

V is constant at 14 kips to D, then jumps down 12 kips to 2 kips and is constant to B

 $|V|_{\text{max}} = 14.00 \text{ kips} \blacktriangleleft$ 

**Moment Diag:** 

 $M_A = -114 \text{ kip} \cdot \text{ft.}$ 

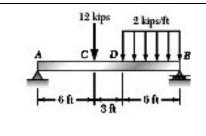
From A to C, M is parabolic  $\left(\frac{dM}{dx}\right)$  increasing with V and

$$M_C = -114 \operatorname{kip} \cdot \operatorname{ft} + \frac{1}{2} (2 \operatorname{kips} + 14 \operatorname{kips}) (6 \operatorname{ft})$$
$$M_C = -66 \operatorname{kip} \cdot \operatorname{ft}.$$

Then *M* is piecewise linear.

$$M_D = -66 \operatorname{kip} \cdot \operatorname{ft} + (14 \operatorname{kips})(4.5 \operatorname{ft}) = -3 \operatorname{kip} \cdot \operatorname{ft}$$
$$M_B = -3 \operatorname{kip} \cdot \operatorname{ft} + (2 \operatorname{kips})(1.5 \operatorname{ft}) = 0$$

 $|M|_{\text{max}} = 114.0 \text{ kip} \cdot \text{ft} \blacktriangleleft$ 



Using the method of Sec. 7.6, solve Prob. 7.38.

# SOLUTION

(*a*) and (*b*)

# FBD Beam:

$$\left(\Sigma M_B = 0: (3 \text{ ft}) \left(2 \frac{\text{kips}}{\text{ft}}\right) (6 \text{ ft}) + (9 \text{ ft}) (12 \text{ kips}) - (15 \text{ ft}) A_y = 0$$
$$\mathbf{A}_y = 9.6 \text{ kips} \uparrow$$

# Shear Diag:

*V* jumps to  $A_y = 9.6$  kips at *A*, is constant to *C*, jumps down 12 kips to -2.4 kips at *C*, is constant to *D*, and then is linear

$$\left(\frac{dV}{dx} = -2 \text{ kips/ft}\right) \text{to } B$$

$$V_B = -2.4 \text{ kips} - (2 \text{ kips/ft})(6 \text{ ft})$$

$$= -14.4 \text{ kips}$$

$$|V|_{\text{max}} = 14.40 \text{ kips} \blacktriangleleft$$

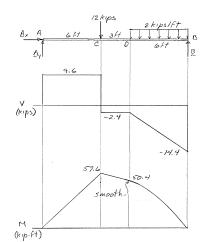
# **Moment Diag:**

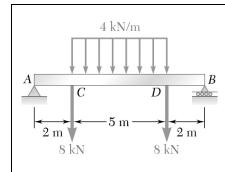
M is linear from A to C

$$\left(\frac{dM}{dx} = 9.6 \text{ kips/ft}\right)$$

$$M_C = 9.6 \operatorname{kips}(6 \operatorname{ft}) = 57.6 \operatorname{kip} \cdot \operatorname{ft},$$

$$M \text{ is linear from } C \text{ to } D \qquad \left(\frac{dM}{dx} = -2.4 \text{ kips/ft}\right)$$
$$M_D = 57.6 \text{ kip} \cdot \text{ft} - 2.4 \text{ kips}(3 \text{ ft})$$
$$M_D = 50.4 \text{ kip} \cdot \text{ft}.$$
$$M \text{ is parabolic } \left(\frac{dM}{dx} \text{ decreasing with } V\right) \text{ to } B.$$
$$M_B = 50.4 \text{ kip} \cdot \text{ft} - \frac{1}{2}(2.4 \text{ kips} + 14.4 \text{ kips})(6 \text{ ft}) = 0$$
$$= 0$$
$$|M|_{\text{max}} = 57.6 \text{ kip} \cdot \text{ft} \blacktriangleleft$$

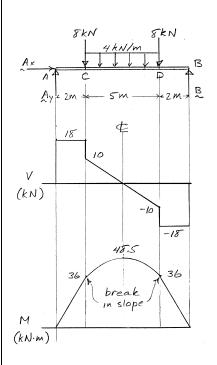




Using the method of Sec. 7.6, solve Prob. 7.39.

# SOLUTION

#### (*a*) and (*b*)



#### FBD Beam:

By symmetry:

$$A_y = B = \frac{1}{2} (5 \text{ m}) (4 \text{ kN/m}) + 8 \text{ kN}$$
  
or  $\mathbf{A}_y = \mathbf{B} = 18 \text{ kN}^{\dagger}$ 

#### **Shear Diag:**

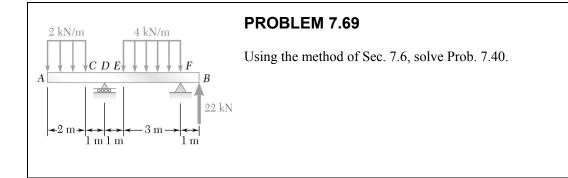
*V* jumps to 18 kN at *A*, and is constant to *C*, then drops 8 kN to 10 kN. After *C*, *V* is linear  $\left(\frac{dV}{dx} = -4 \text{ kN/m}\right)$ , reaching -10 kN at  $D\left[V_D = 10 \text{ kN} - (4 \text{ kN/m})(5 \text{ m})\right]$  passing through zero at the beam center. At *D*, *V* drops 8 kN to -18 kN and is then constant to *B*  $|V|_{\text{max}} = 18.00 \text{ kN} \blacktriangleleft$ 

#### **Moment Diag:**

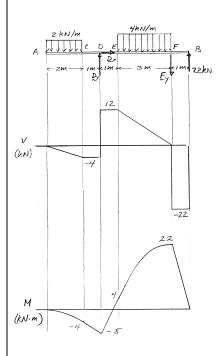
$$M_A = 0$$
. Then *M* is linear  $\left(\frac{dM}{dx} = 18 \text{ kN/m}\right)$  to *C*  
 $M_C = (18 \text{ kN})(2 \text{ m}) = 36 \text{ kN} \cdot \text{m}$ , *M* is parabolic to *D*  
 $\left(\frac{dM}{dx}\right)$  decreases with *V* to zero at center  $\int$ 

$$M_{\text{center}} = 36 \text{ kN} \cdot \text{m} + \frac{1}{2} (10 \text{ kN}) (2.5 \text{ m}) = 48.5 \text{ kN} \cdot \text{m} = M_{\text{max}}$$
$$|M|_{\text{max}} = 48.5 \text{ kN} \cdot \text{m} \blacktriangleleft$$

Complete by invoking symmetry.



(*a*) and (*b*)



FBD Beam:  $\sum \Sigma M_F = 0: (1 \text{ m})(22 \text{ kN}) + (1.5 \text{ m})(4 \text{ kN/m})(3 \text{ m})$   $-(4 \text{ m})D_y + (6 \text{ m})(2 \text{ kN/m})(2 \text{ m}) = 0$   $D_y = 16 \text{ kN}$   $\uparrow \Sigma F_y = 0: 16 \text{ kN} + 22 \text{ kN} - F_y - (2 \text{ kN/m})(2 \text{ m})$  -(4 kN/m)(3 m) = 0 $F_y = 22 \text{ kN}$ 

Shear Diag:

$$V_A = 0$$
, then V is linear  $\left(\frac{dV}{dx} = -2 \text{ kN/m}\right)$  to C;  
 $V_C = -2 \text{ kN/m}(4 \text{ m}) = -4 \text{ kN}$ 

V is constant to D, jumps 16 kN to 12 kN and is constant to E.

Then V is linear 
$$\left(\frac{dV}{dx} = -4 \text{ kN/m}\right)$$
 to F.  
 $V_F = 12 \text{ kN} - (4 \text{ kN/m})(3 \text{ m}) = 0.$ 

V jumps to -22 kN at F, is constant to B, and returns to zero.

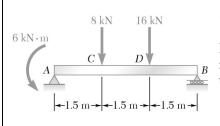
$$|V|_{\text{max}} = 22.0 \text{ kN} \blacktriangleleft$$

#### **Moment Diag:**

$$M_A = 0$$
, *M* is parabolic  $\left(\frac{dM}{dx} \text{ decreases with } V\right)$  to *C*.  
 $M_C = -\frac{1}{2}(4 \text{ kN})(2 \text{ m}) = -4 \text{ kN} \cdot \text{m}.$ 

# **PROBLEM 7.69 CONTINUED**

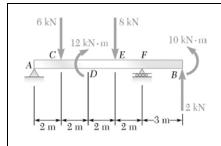
Then *M* is linear 
$$\left(\frac{dM}{dx} = -4 \text{ kN}\right)$$
 to *D*.  
 $M_D = -4 \text{ kN} \cdot \text{m} - (4 \text{ kN})(1 \text{ m}) = -8 \text{ kN} \cdot \text{m}$   
From *D* to *E*, *M* is linear  $\left(\frac{dM}{dx} = 12 \text{ kN}\right)$ , and  
 $M_E = -8 \text{ kN} \cdot \text{m} + (12 \text{ kN})(1\text{m})$   
 $M_E = 4 \text{ kN} \cdot \text{m}$   
M is parabolic  $\left(\frac{dM}{dx}$  decreasing with *V*  $\right)$  to F.  
 $M_F = 4 \text{ kN} \cdot \text{m} + \frac{1}{2}(12 \text{ kN})(3 \text{ m}) = 22 \text{ kN} \cdot \text{m}$ .  
Finally, *M* is linear  $\left(\frac{dM}{dx} = -22 \text{ kN}\right)$ , back to zero at *B*.  
 $|M|_{\text{max}} = 22.0 \text{ kN} \cdot \text{m} \blacktriangleleft$ 



# **PROBLEM 7.70**

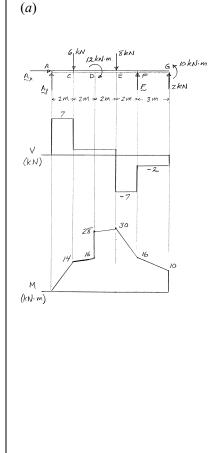
For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

#### (a) and (b)**FBD Beam:** $(\Sigma M_B = 0: (1.5 \text{ m})(16 \text{ kN})$ + (3 m)(8 kN) + $6 \text{ kN} \cdot \text{m} - (4.5 \text{ m})A_y = 0$ $\mathbf{A}_y = 12 \text{ kN}^{\dagger}$ 16 KN 8KN 6 KN.M ß **Shear Diag:** V is piecewise constant with discontinuities equal to the concentrated 17 forces at A, C, D, B 4 $|V|_{\text{max}} = 12.00 \text{ kN} \blacktriangleleft$ V (kN)**Moment Diag:** -12 After a jump of $-6 \text{ kN} \cdot \text{m}$ at A, M is piecewise linear $\left(\frac{dM}{dx} = V\right)$ 18 12 Μ $M_C = -6 \text{ kN} \cdot \text{m} + (12 \text{ kN})(1.5 \text{ m}) = 12 \text{ kN} \cdot \text{m}$ (KNim) So -6 $M_D = 12 \text{ kN} \cdot \text{m} + (4 \text{ kN})(1.5 \text{ m}) = 18 \text{ kN} \cdot \text{m}$ $M_B = 18 \text{ kN} \cdot \text{m} - (12 \text{ kN})(1.5 \text{ m}) = 0$ $|M|_{\rm max} = 18.00 \, \rm kN \cdot m \blacktriangleleft$



For the beam and loading shown, (a) draw the shear and bendingmoment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

# SOLUTION



#### **FBD Beam:**

(

$$\Sigma M_{A} = 0: (8 \text{ m})F + (11 \text{ m})(2 \text{ kN}) + 10 \text{ kN} \cdot \text{m} - (6 \text{ m})(8 \text{ kN})$$
$$- 12 \text{ kN} \cdot \text{m} - (2 \text{ m})(6 \text{ kN}) = 0 \quad \mathbf{F} = 5 \text{ kN} \uparrow$$
$$\uparrow \Sigma F_{y} = 0: A_{y} - 6 \text{ kN} - 8 \text{ kN} + 5 \text{ kN} + 2 \text{ kN} = 0$$
$$\mathbf{A}_{y} = 7 \text{ kN} \uparrow$$

## Shear Diag:

V is piecewise constant with discontinuities equal to the concentrated forces at A, C, E, F, G

#### **Moment Diag:**

*M* is piecewise linear with a discontinuity equal to the couple at *D*.

$$M_{C} = (7 \text{ kN})(2 \text{ m}) = 14 \text{ kN} \cdot \text{m}$$

$$M_{D^{-}} = 14 \text{ kN} \cdot \text{m} + (1 \text{ kN})(2 \text{ m}) = 16 \text{ kN} \cdot \text{m}$$

$$M_{D^{+}} = 16 \text{ kN} \cdot \text{m} + 12 \text{ kN} \cdot \text{m} = 28 \text{ kN} \cdot \text{m}$$

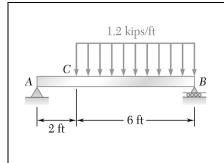
$$M_{E} = 28 \text{ kN} \cdot \text{m} + (1 \text{ kN})(2 \text{ m}) = 30 \text{ kN} \cdot \text{m}$$

$$M_{F} = 30 \text{ kN} \cdot \text{m} - (7 \text{ kN})(2 \text{ m}) = 16 \text{ kN} \cdot \text{m}$$

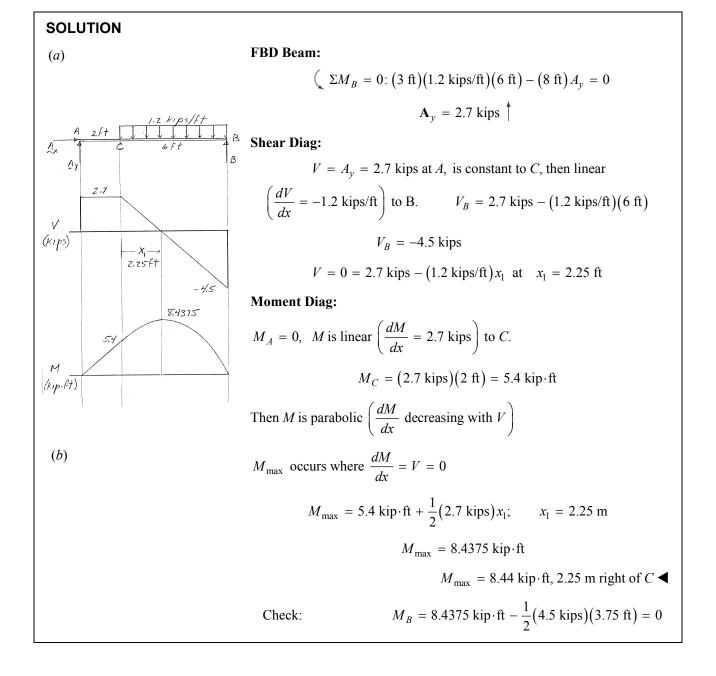
$$M_{G} = 16 \text{ kN} \cdot \text{m} - (2 \text{ kN})(3 \text{ m}) = 10 \text{ kN} \cdot \text{m}$$

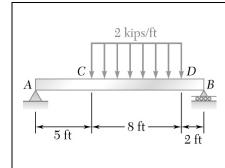
$$(b) \qquad |V|_{\text{max}} = 7.00 \text{ kN} \blacktriangleleft$$

$$|M|_{\text{max}} = 30.0 \text{ kN} \blacktriangleleft$$



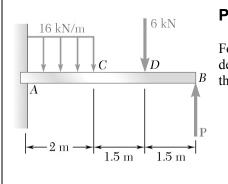
For the beam and loading shown, (a) draw the shear and bending-moment diagrams, (b) determine the magnitude and location of the maximum bending moment.



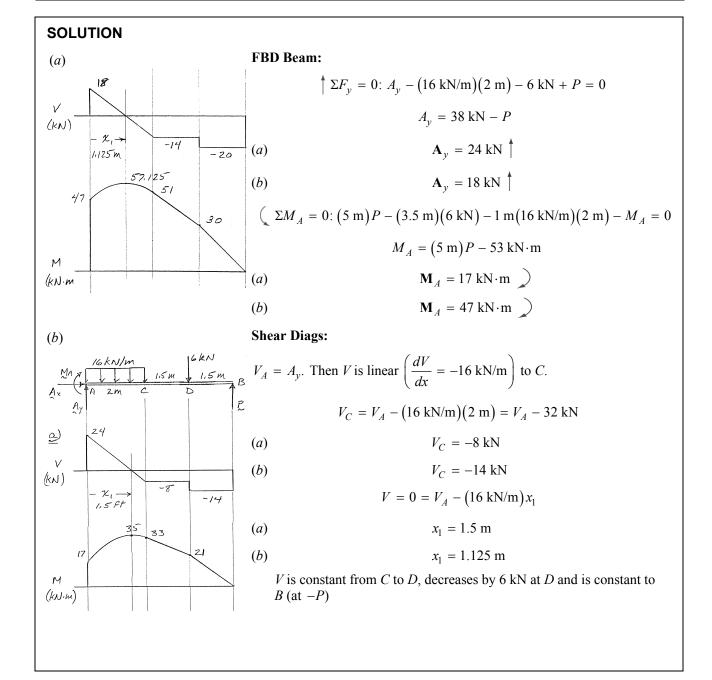


For the beam and loading shown, (a) draw the shear and bending-moment diagrams, (b) determine the magnitude and location of the maximum bending moment.

# SOLUTION **FBD Beam:** (a) $(\Sigma M_B = 0: (6 \text{ ft})(2 \text{ kips/ft})(8 \text{ ft}) - (15 \text{ ft})A_y = 0$ $A_v = 6.4$ kips A, ß **Shear Diag:** $V = A_v = 6.4$ kips at A, and is constant to C, then linear $\left(\frac{dV}{dx} = -2 \text{ kips/ft}\right)$ to D, ν (kips) - *K*,→ 3.2.Ft $V_D = 6.4 \text{ kips} - (2 \text{ kips/ft})(8 \text{ ft}) = -9.6 \text{ kips}$ -9.6 V = 0 = 6.4 kips $-(2 \text{ kips/ft})x_1$ at $x_1 = 3.2$ ft 42.24 32 **Moment Diag:** 19.2 $M_A = 0$ , then *M* is linear $\left(\frac{dM}{dx} = 6.4 \text{ kips}\right)$ to $M_C = (6.4 \text{ kips})(5 \text{ ft})$ . М (KIp. Ft) $M_C = 32 \text{ kip} \cdot \text{ft.} M \text{ is then parabolic } \left(\frac{dM}{dx} \text{ decreasing with } V\right).$ $M_{\text{max}}$ occurs where $\frac{dM}{dr} = V = 0$ . *(b)* $M_{\text{max}} = 32 \text{ kip} \cdot \text{ft} + \frac{1}{2} (6.4 \text{ kips}) x_1; \qquad x_1 = 3.2 \text{ ft}$ $M_{\rm max} = 42.24 \ {\rm kip} \cdot {\rm ft}$ $M_{\text{max}} = 42.2 \text{ kip} \cdot \text{ft}, 3.2 \text{ ft right of } C \blacktriangleleft$ $M_D = 42.24 \text{ kip} \cdot \text{ft} - \frac{1}{2} (9.6 \text{ kips}) (4.8 \text{ ft}) = 19.2 \text{ kip} \cdot \text{ft}$ *M* is linear from *D* to zero at *B*.



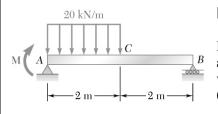
For the beam shown, draw the shear and bending-moment diagrams and determine the maximum absolute value of the bending moment knowing that (a) P = 14 kN, (b) P = 20 kN.



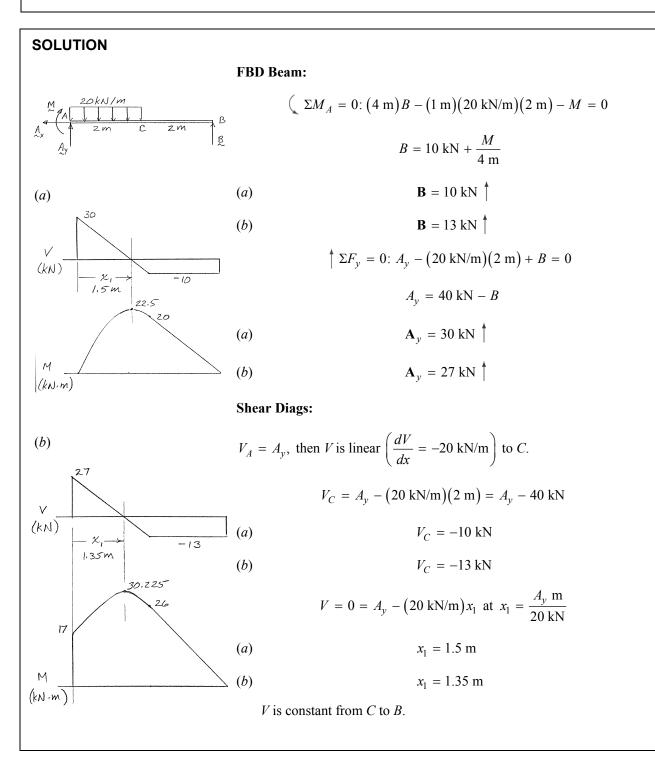
# **PROBLEM 7.74 CONTINUED**

# **Moment Diags:**

filment Diago.
$M_A = M_A$ reaction. Then <i>M</i> is parabolic $\left(\frac{dM}{dx}\right)$ decreasing with <i>V</i> .
The maximum occurs where $V = 0$ . $M_{\text{max}} = M_A + \frac{1}{2}V_A x_1$ .
(a) $M_{\text{max}} = 17 \text{ kN} \cdot \text{m} + \frac{1}{2} (24 \text{ kN}) (1.5 \text{ m}) = 35.0 \text{ kN} \cdot \text{m} \blacktriangleleft$
1.5 ft from $A \blacktriangleleft$
(b) $M_{\text{max}} = 47 \text{ kN} \cdot \text{m} + \frac{1}{2} (18 \text{ kN}) (1.125 \text{ m}) = 57.125 \text{ kN} \cdot \text{m}$
$M_{\text{max}} = 57.1 \text{ kN} \cdot \text{m} \ 1.125 \text{ ft from } A \blacktriangleleft$
$M_C = M_{\max} + \frac{1}{2} V_C (2 \text{ m} - x_1)$
(a) $M_C = 35 \text{ kN} \cdot \text{m} - \frac{1}{2} (8 \text{ kN}) (0.5 \text{ m}) = 33 \text{ kN} \cdot \text{m}$
(b) $M_C = 57.125 \text{ kN} \cdot \text{m} - \frac{1}{2} (14 \text{ kN}) (0.875 \text{ m}) = 51 \text{ kN} \cdot \text{m}$
<i>M</i> is piecewise linear along <i>C</i> , <i>D</i> , <i>B</i> , with $M_B = 0$ and
$M_D = (1.5 \text{ m})P$
(a) $M_D = 21 \mathrm{kN} \cdot \mathrm{m}$
$(b)$ $M_D = 30 \text{ kN} \cdot \text{m}$



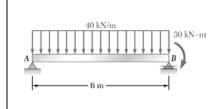
For the beam shown, draw the shear and bending-moment diagrams, and determine the magnitude and location of the maximum absolute value of the bending moment knowing that (a) M = 0, (b) M = 12 kN · m.



# PROBLEM 7.75 CONTINUED

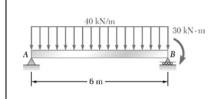
# **Moment Diags:**

$M_A$ = applied <i>M</i> . Then <i>M</i> is parabolic $\left(\frac{dM}{dx}\right)$ decreases with <i>V</i>		
<i>M</i> is max where $V = 0$ . $M_{\text{max}} = M + \frac{1}{2}A_y x_1$ .		
<i>(a)</i>	$ M _{\text{max}} = \frac{1}{2} (30 \text{ kN}) (1.5 \text{ m}) = 22.5 \text{ kN} \cdot \text{m} \blacktriangleleft$	
	1.500 m from <i>A</i> ◀	
(b)	$M_{\text{max}} = 12 \text{ kN} \cdot \text{m} + \frac{1}{2} (27 \text{ kN}) (1.35 \text{ m}) = 30.225 \text{ kN} \cdot \text{m} \blacktriangleleft$	
	$ M _{\text{max}} = 30.2 \text{ kN}  1.350 \text{ m from } A \blacktriangleleft$	
	$M_C = M_{\text{max}} - \frac{1}{2} V_C (2 \text{ m} - x_1)$	
<i>(a)</i>	$M_C = 20 \text{ kN} \cdot \text{m}$	
<i>(b)</i>	$M_C = 26 \text{ kN} \cdot \text{m}$	
Finally	$V_{C}$ , $M$ is linear $\left(\frac{dM}{dx} = V_{C}\right)$ to zero at $B$ .	

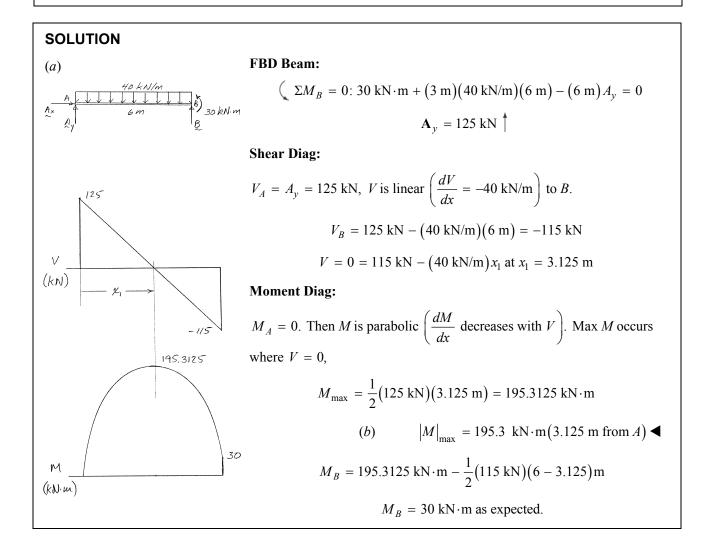


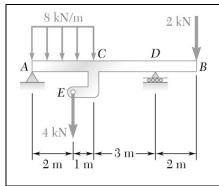
For the beam and loading shown, (a) draw the shear and bending-moment diagrams, (b) determine the magnitude and location of the maximum absolute value of the bending moment.

# SOLUTION **FBD Beam:** *(a)* $(\Sigma M_B = 0: (3 \text{ m})(40 \text{ kN/m})(6 \text{ m}) - (30 \text{ kN} \cdot \text{m}) - (6 \text{ m})A_y = 0$ $\mathbf{A}_{v} = 115 \text{ kN}^{\dagger}$ 30 k.N.m A, **Shear Diag:** $V_A = A_y = 115$ kN, then V is linear $\left(\frac{dM}{dx} = -40$ kN/m $\right)$ to B. 115 $V_B = 115 \text{ kN} - (40 \text{ kN/m})(6 \text{ m}) = -125 \text{ kN}.$ $\mathbf{v}$ $V = 0 = 115 \text{ kN} - (40 \text{ kN/m})x_1 \text{ at } x_1 = 2.875 \text{ m}$ (KN) ×, 2.875 W **Moment Diag:** $M_A = 0$ . Then *M* is parabolic $\left(\frac{dM}{dr}\right)$ decreasing with *V*. Max *M* occurs 165.3125 where V = 0, $M_{\text{max}} = \frac{1}{2} (115 \text{ kN/m}) (2.875 \text{ m}) = 165.3125 \text{ kN} \cdot \text{m}$ M (KN.m) $M_B = M_{\text{max}} - \frac{1}{2} (125 \text{ kN}) (6 \text{ m} - x_1)$ $= 165.3125 \text{ kN} \cdot \text{m} - \frac{1}{2} (125 \text{ kN}) (6 - 2.875) \text{m}$ = $-30 \text{ kN} \cdot \text{m}$ as expected. $|M|_{\text{max}} = 165.3 \text{ kN} \cdot \text{m} (2.88 \text{ m from } A) \blacktriangleleft$ *(b)*



Solve Prob. 7.76 assuming that the 30 kN  $\cdot$  m couple applied at *B* is counterclockwise



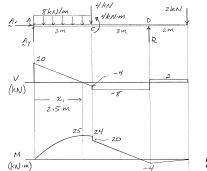


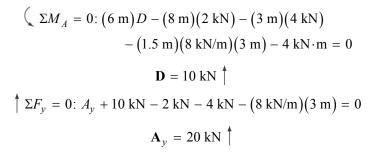
For beam AB, (a) draw the shear and bending-moment diagrams, (b) determine the magnitude and location of the maximum absolute value of the bending moment.

#### SOLUTION

*(a)* 

Replacing the load at *E* with equivalent force-couple at *C*:





Shear Diag:

$$V_A = A_y = 20 \text{ kN}$$
, then V is linear  $\left(\frac{dV}{dx} = -8 \text{ kN/m}\right)$  to C  
 $V_C = 20 \text{ kN} - (8 \text{ kN/m})(3 \text{ m}) = -4 \text{ kN}$   
 $V = 0 = 20 \text{ kN} - (8 \text{ kN/m})x_1 \text{ at } x_1 = 2.5 \text{ m}$ 

At C, V decreases by 4 kN to -8 kN.

At D, V increases by 10 kN to 2 kN.

#### **Moment Diag:**

 $M_A = 0$ , then *M* is parabolic  $\left(\frac{dM}{dx}\right)$  decreasing with *V*. Max *M* occurs where V = 0.

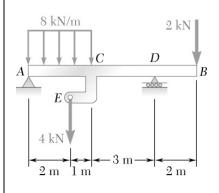
$$M_{\text{max}} = \frac{1}{2} (20 \text{ kN}) (2.5 \text{ m}) = 25 \text{ kN} \cdot \text{m}$$
  
(b)  $M_{\text{max}} = 25.0 \text{ kN} \cdot \text{m}, 2.50 \text{ m} \text{ from } A \blacktriangleleft$ 

# **PROBLEM 7.78 CONTINUED**

$$M_C = 25 \text{ kN} \cdot \text{m} - \frac{1}{2} (4 \text{ kN}) (0.5 \text{ m}) = 24 \text{ kN} \cdot \text{m}.$$

At C, M decreases by 4 kN·m to 20 kN·m. From C to B, M is piecewise

linear with 
$$\frac{dM}{dx} = -8$$
 kN to *D*, then  $\frac{dM}{dx} = +2$  kN to *B*.  
 $M_D = 20$  kN·m -  $(8$  kN) $(3$  m) = -4 kN·m.  $M_B = 0$ 



Solve Prob. 7.78 assuming that the 4-kN force applied at E is directed upward.

# SOLUTION

Ax A Ay

(*a*) Replacing the load at *E* with equivalent force-couple at *C*.

$$\frac{\delta k N/m}{\delta m} = \frac{4 k N}{C} \frac{1}{A} \frac{1}{3 m} \frac{1}{b^2} \frac{1}{c^2} \frac{1}{b^2} \frac{1}{b^3} \frac{1}{b^3} \frac{1}{b^3} \sum_{k=1}^{2 m} \frac{1}{b^3} \frac{1}{b^3} \sum_{k=1}^{2 m} \frac{1}{b^3} \sum_{k=1$$

 Shear Diag:

$$V_A = A_y = \frac{44}{3} \text{ kN, then } V \text{ is linear} \left(\frac{dV}{dx} = -8 \text{ kN/m}\right) \text{ to } C$$

$$V_C = \frac{44}{3} \text{ kN} - (8 \text{ kN/m})(3 \text{ m}) = -\frac{28}{3} \text{ kN}$$

$$V = 0 = \frac{44}{3} \text{ kN} - (8 \text{ kN/m})x_1 \text{ at } x_1 = \frac{11}{6} \text{ m.}$$
At C, V increases 4 kN to  $-\frac{16}{3} \text{ kN.}$ 
At D, V increases  $\frac{22}{3} \text{ kN}$  to 2 kN.

# **PROBLEM 7.79 CONTINUED**

# Moment Diag:

 $M_A = 0$ . Then *M* is parabolic  $\left(\frac{dM}{dx}\right)$  decreasing with *V*. Max *M* occurs where V = 0.

$$M_{\text{max}} = \frac{1}{2} \left( \frac{44}{3} \text{ kN} \right) \left( \frac{11}{6} \text{ m} \right) = \frac{121}{9} \text{ kN} \cdot \text{m}$$

(b) 
$$M_{\text{max}} = 13.44 \text{ kN} \cdot \text{m at } 1.833 \text{ m from } A \blacktriangleleft$$

$$M_C = \frac{121}{9} \text{ kN} \cdot \text{m} - \frac{1}{2} \left(\frac{28}{3} \text{ kN}\right) \left(\frac{7}{6} \text{ m}\right) = 8 \text{ kN} \cdot \text{m}.$$

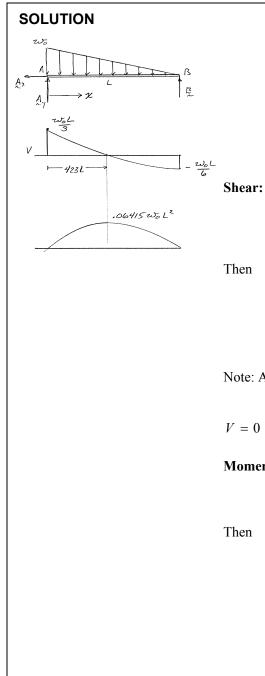
At C, M increases by  $4 \text{ kN} \cdot \text{m}$  to  $12 \text{ kN} \cdot \text{m}$ . Then M is linear

$$\left(\frac{dM}{dx} = -\frac{16}{3} \text{ kN}\right) \text{ to } D.$$

$$M_D = 12 \text{ kN} \cdot \text{m} - \left(\frac{16}{3} \text{ kN}\right)(3 \text{ m}) = -4 \text{ kN} \cdot \text{m}. \text{ M is again linear}$$

$$\left(\frac{dM}{dx} = 2 \text{ kN}\right) \text{ to zero at } B.$$

For the beam and loading shown, (a) derive the equations of the shear and bending-moment curves, (b) draw the shear and bending-moment diagrams, (c) determine the magnitude and location of the maximum bending moment.



w $w_0$ 

A

Distributed load 
$$w = w_0 \left(1 - \frac{x}{L}\right)$$
  $\left(\text{total} = \frac{1}{2}w_0L\right)$   
 $\left(\sum M_A = 0: \frac{L}{3}\left(\frac{1}{2}w_0L\right) - LB = 0$   $\mathbf{B} = \frac{w_0L}{6}$   
 $\uparrow \Sigma F_y = 0: A_y - \frac{1}{2}w_0L + \frac{w_0L}{6} = 0$   $\mathbf{A}_y = \frac{w_0L}{3}$ 

$$V_A = A_y = \frac{w_0 L}{3},$$

Then

$$\frac{dV}{dx} = -w \to V = V_A - \int_0^x w_0 \left(1 - \frac{x}{L}\right) dx$$
$$V = \left(\frac{w_0 L}{3}\right) - w_0 x + \frac{1}{2} \frac{w_0}{L} x^2 = w_0 L \left[\frac{1}{3} - \frac{x}{L} + \frac{1}{2} \left(\frac{x}{L}\right)^2\right]$$

Note: At x = L,  $V = -\frac{w_0 L}{6}$ ;

$$V = 0$$
 at  $\left(\frac{x}{L}\right)^2 - 2\left(\frac{x}{L}\right) + \frac{2}{3} = 0 \rightarrow \frac{x}{L} = 1 - \sqrt{\frac{1}{3}}$ 

Moment:

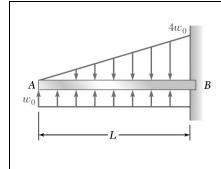
$$\left(\frac{dM}{dx}\right) = V \rightarrow M = \int_0^x V dx = L \int_0^{x/L} V\left(\frac{x}{L}\right) d\left(\frac{x}{L}\right)$$
$$M = w_0 L^2 \int_0^{x/L} \left[\frac{1}{3} - \frac{x}{L} + \frac{1}{2}\left(\frac{x}{L}\right)^2\right] d\left(\frac{x}{L}\right)$$
$$M = w_0 L^2 \left[\frac{1}{3}\left(\frac{x}{L}\right) - \frac{1}{2}\left(\frac{x}{L}\right)^2 + \frac{1}{6}\left(\frac{x}{L}\right)^3\right]$$

 $M_A = 0,$ 

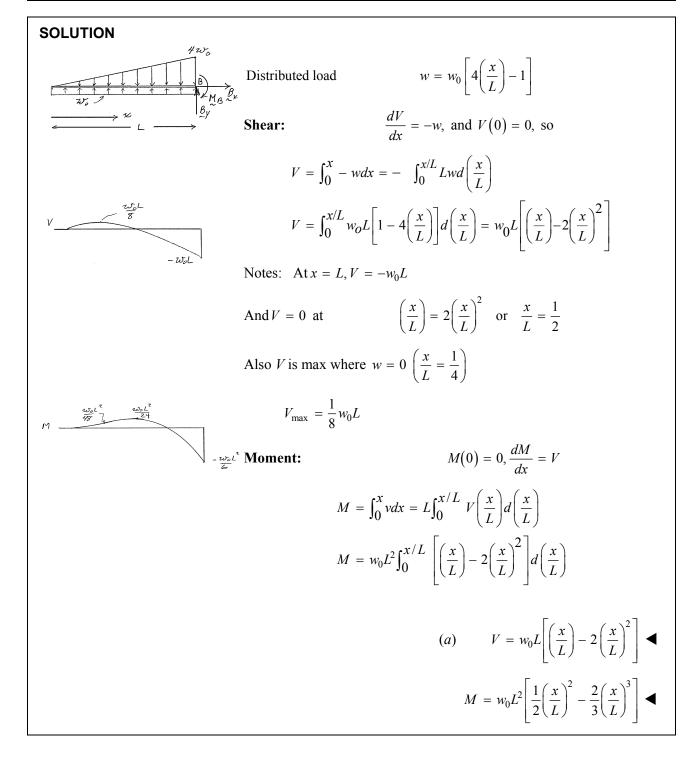
# PROBLEM 7.80 CONTINUED

$$M_{\max}\left(at \ \frac{x}{L} = 1 - \sqrt{\frac{1}{3}}\right) = 0.06415w_0L^2$$
(a)  $V = w_0L\left[\frac{1}{3} - \frac{x}{L} + \frac{1}{2}\left(\frac{x}{L}\right)^2\right] \blacktriangleleft$ 

$$M = w_0L^2\left[\frac{1}{3}\left(\frac{x}{L}\right) - \frac{1}{2}\left(\frac{x}{L}\right)^2 + \frac{1}{6}\left(\frac{x}{L}\right)^3\right] \bigstar$$
(c)  $M_{\max} = 0.0642 \ w_0L^2 \bigstar$ 
at  $x = 0.423L \bigstar$ 



For the beam and loading shown, (a) derive the equations of the shear and bending-moment curves, (b) draw the shear and bending-moment diagrams, (c) determine the magnitude and location of the maximum bending moment.



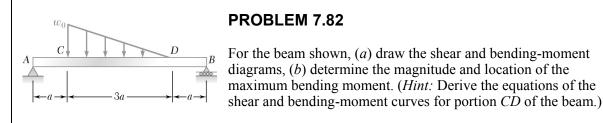
#### **PROBLEM 7.81 CONTINUED**

$$M_{\text{max}} = \frac{1}{24} w_0 L^2 \text{ at } x = \frac{L}{2}$$

$$M_{\text{min}} = -\frac{1}{6} w_0 L^2 \text{ at } x = L$$

$$M_{\text{max}} = \frac{w_0 L^2}{24} \text{ at } x = \frac{L}{2}$$

$$(c) \qquad |M|_{\text{max}} = -M_{\text{min}} = \frac{w_0 L^2}{6} \text{ at } B \blacktriangleleft$$



#### SOLUTION

*(a)* 

#### **FBD Beam:**

$$\Sigma M_{B} = 0: \quad (3a) \left[ \frac{1}{2} w_{0} (3a) \right] - 5aA_{y} = 0 \qquad \mathbf{A}_{y} = 0.9 w_{0} a^{\dagger}$$
$$\uparrow \Sigma F_{y} = 0: \quad 0.9 w_{0} a - \frac{1}{2} w_{0} (3a) + B = 0$$
$$\mathbf{B} = 0.6 w_{0} a^{\dagger}$$

#### **Shear Diag:**

 $V = A_y = 0.9w_0 a \text{ from } A \text{ to } C \text{ and } V = B = -0.6w_0 a \text{ from } B \text{ to } D.$ Then from D to C,  $w = w_0 \frac{x_1}{3a}$ . If  $x_1$  is measured right to left,  $\frac{dV}{dx_1} = +w$  and  $\frac{dM}{dx_1} = -V$ . So, from D,  $V = -0.6w_0 a + \int_0^{x_1} \frac{w_0}{3a} x_1 dx_1$ ,  $V = w_0 a \left[ -0.6 + \frac{1}{6} \left( \frac{x_1}{a} \right)^2 \right]$ Note: V = 0 at  $\left( \frac{x_1}{a} \right)^2 = 3.6$ ,  $x_1 = \sqrt{3.6}a$ 

#### **Moment Diag:**

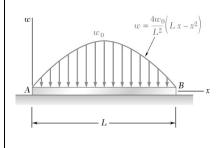
 $M = 0 \text{ at } A, \text{ increasing linearly} \left(\frac{dM}{dx_1} = 0.9w_0a\right) \text{to } M_C = 0.9w_0a^2.$ Similarly M = 0 at B increasing linearly  $\left(\frac{dM}{dx} = 0.6w_0a\right)$  to  $M_D = 0.6w_0a^2.$  Between C and D $M = 0.6w_0a^2 + w_0a \int_0^{x_1} \left[0.6 - \frac{1}{2}\left(\frac{x_1}{2}\right)^2\right] dx_1,$ 

$$M = 0.6w_0 a^2 + w_0 a \int_0^1 \left[ 0.6 - \frac{1}{6} \left( \frac{x_1}{a} \right) \right] dx$$
$$M = w_0 a^2 \left[ 0.6 + 0.6 \left( \frac{x_1}{a} \right) - \frac{1}{18} \left( \frac{x_1}{a} \right)^3 \right]$$

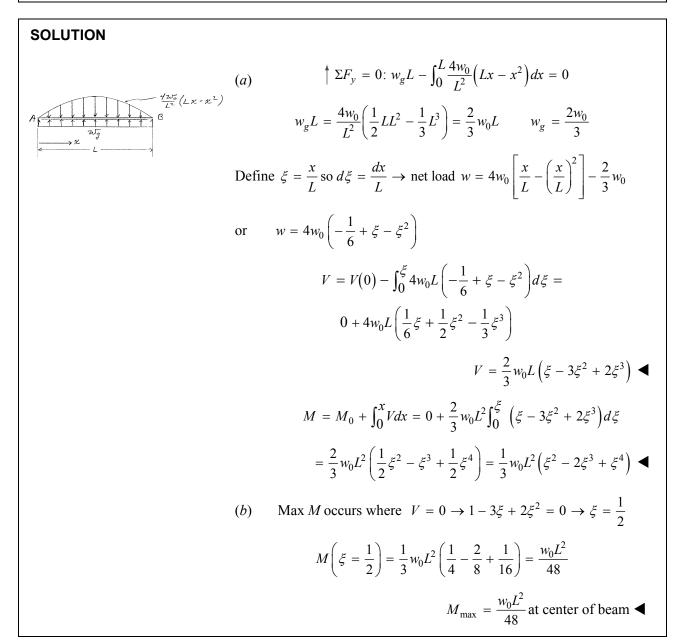
A a  $x_{0}$   $x_{0}$   $x_{1}$   $x_{1}$   $x_{1}$   $x_{2}$   $x_{1}$   $x_{2}$   $x_{3}$   $x_{1}$   $x_{1}$   $x_{2}$   $x_{3}$   $x_{2}$   $x_{3}$   $x_{2}$   $x_{3}$   $x_{3}$ 

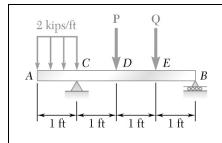
#### **PROBLEM 7.82 CONTINUED**

- (b) At  $\frac{x_1}{a} = \sqrt{3.6}, M = M_{\text{max}} = 1.359 w_0 a^2 \blacktriangleleft$ 
  - $x_1 = 1.897a$  left of *D*

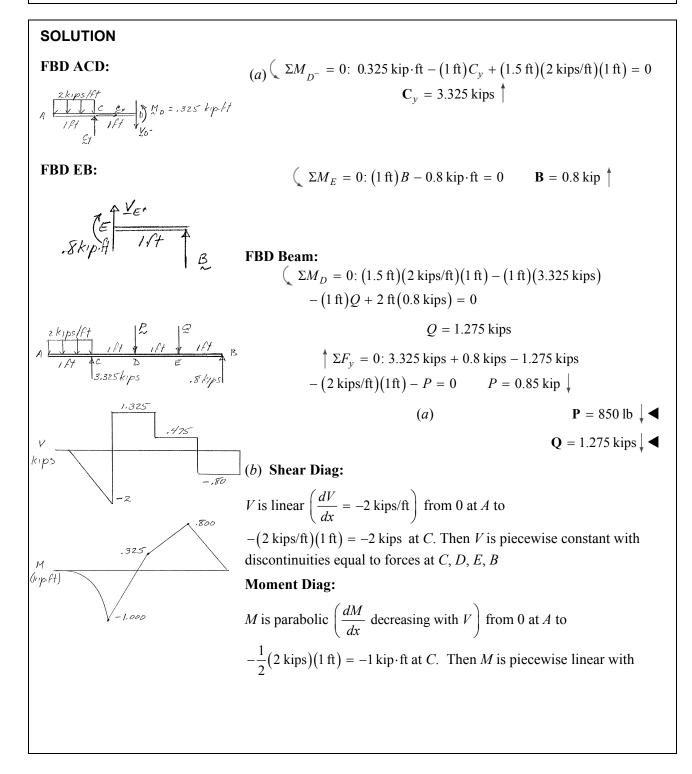


Beam AB, which lies on the ground, supports the parabolic load shown. Assuming the upward reaction of the ground to be uniformly distributed, (*a*) write the equations of the shear and bending-moment curves, (*b*) determine the maximum bending moment.



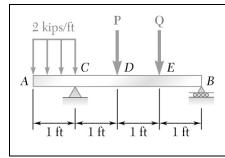


The beam *AB* is subjected to the uniformly distributed load shown and to two unknown forces **P** and **Q**. Knowing that it has been experimentally determined that the bending moment is +325 lb ft at *D* and +800 lb ft at *E*, (*a*) determine **P** and **Q**, (*b*) draw the shear and bending-moment diagrams for the beam.

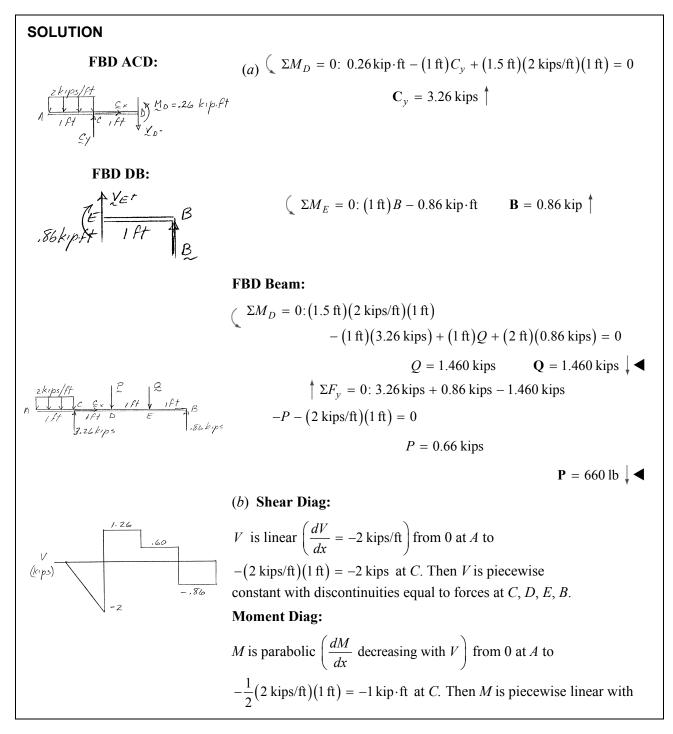


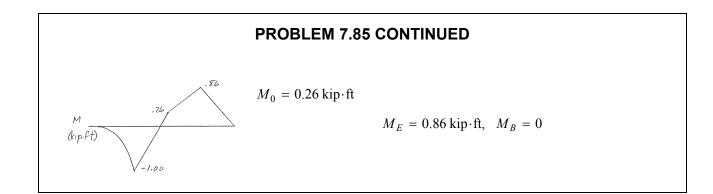
#### **PROBLEM 7.84 CONTINUED**

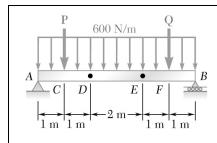
$$M_D = -1 \operatorname{kip} \cdot \operatorname{ft} + (1.325 \operatorname{kips})(1 \operatorname{ft}) = 0.325 \operatorname{kip} \cdot \operatorname{ft}$$
$$M_E = 0.325 \operatorname{kip} \cdot \operatorname{ft} + (0.475 \operatorname{kips})(1 \operatorname{ft}) = 0.800 \operatorname{kip} \cdot \operatorname{ft}$$
$$M_B = 0.8 \operatorname{kip} \cdot \operatorname{ft} - (0.8 \operatorname{kip})(1 \operatorname{ft}) = 0$$



Solve Prob. 7.84 assuming that the bending moment was found to be +260 lb ft at *D* and +860 lb ft at *E*.



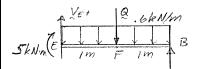


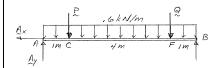


The beam *AB* is subjected to the uniformly distributed load shown and to two unknown forces **P** and **Q**. Knowing that it has been experimentally determined that the bending moment is  $+7 \text{ kN} \cdot \text{m}$ at *D* and  $+5 \text{ kN} \cdot \text{m}$  at *E*, (*a*) determine **P** and **Q**, (*b*) draw the shear and bending-moment diagrams for the beam.

## SOLUTION FBD AD: (a) $A = \frac{A}{M} = \frac{1}{M} = \frac{1}{M}$

FBD EB:





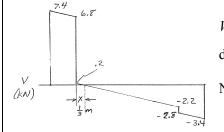
$(\Sigma M_D = 0: 7 \text{ kN} \cdot \text{m} + (1 \text{ m})(0.6 \text{ kN/m})(2 \text{ m})$
$-(2 \mathrm{m})A_y = 0$
$2A_y - P = 8.2 \text{ kN}$ (1)
$(\Sigma M_E = 0: (2 \text{ m})B - (1 \text{ m})Q - (1 \text{ m})(0.6 \text{ kN/m})(2 \text{ m})$
$-5 \text{ kN} \cdot \text{m} = 0$
$2B - Q = 6.2 \mathrm{kN}$ (2)
$(\Sigma M_A = 0: (6 \text{ m})B - (1 \text{ m})P - (5 \text{ m})Q$
-(3 m)(0.6 kN/m)(6 m) = 0
$6B - P - 5Q = 10.8 \mathrm{kN}$ (3)
$(\Sigma M_B = 0: (1 \text{ m})Q + (5 \text{ m})P + (3 \text{ m})(0.6 \text{ kN/m})(6 \text{ m})$
$-(6 \mathrm{m})A = 0$
6A - Q - 5P = 10.8  kN (4)
$\mathbf{P}_{\mathbf{A}}(1) (4)$

Solving (1)–(4):

 $\mathbf{P} = 6.60 \text{ kN } \downarrow, \ \mathbf{Q} = 600 \text{ N} \downarrow \blacktriangleleft$ 

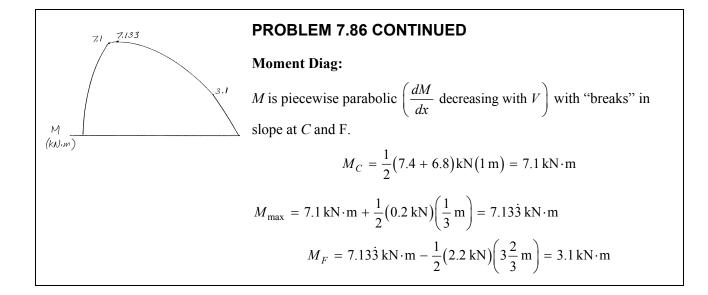
$$\mathbf{A}_y = 7.4 \text{ kN} \uparrow, \quad \mathbf{B} = 3.4 \text{ kN} \uparrow$$

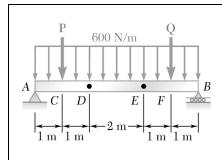
#### (b) Shear Diag:



*V* is piecewise linear with  $\frac{dV}{dx} = -0.6$  kN/m throughout, and discontinuities equal to forces at *A*, *C*, *F*, *B*.

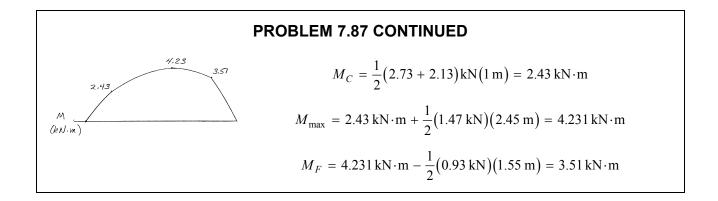
Note 
$$V = 0 = 0.2 \text{ kN} - (0.6 \text{ kN/m})x$$
 at  $x = \frac{1}{3} \text{ m}$ 

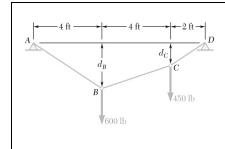




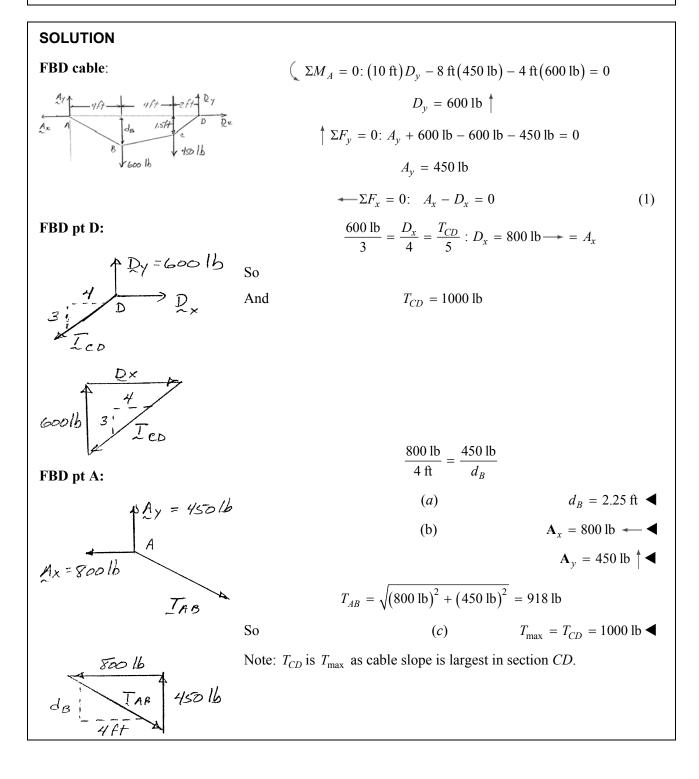
Solve Prob. 7.86 assuming that the bending moment was found to be +3.6 kN  $\cdot$  m at *D* and +4.14 kN  $\cdot$  m at *E*.

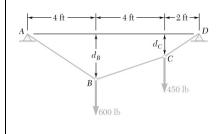
SOLUTION  $(\Sigma M_D = 0: 3.6 \text{ kN} \cdot \text{m} + (1 \text{ m})P + (1 \text{ m})(0.6 \text{ kN/m})(2 \text{ m})$ FBD AD: *(a)*  $-(2 \mathrm{m})A_{v}=0$ 3.6 KN·M  $2A_v - P = 4.8 \text{ kN}$ (1) FBD EB:  $(\Sigma M_E = 0: (2 m)B - (1 m)Q - (1 m)(0.6 kN/m)(2 m) - 4.14 kN \cdot m = 0$  $2B - Q = 5.34 \,\mathrm{kN}$ (2) $\sum M_{A} = 0: (6 \text{ m})B - (5 \text{ m})Q - (1 \text{ m})P - (3 \text{ m})(0.6 \text{ kN/m})(6 \text{ m}) = 0$ 6B - P - 5Q = 10.8 kN (3)By symmetry:  $6A - Q - 5P = 10.8 \,\mathrm{kN}$  (4)  $\mathbf{P} = 660 \text{ N } \downarrow, \ \mathbf{Q} = 2.28 \text{ kN} \downarrow \blacktriangleleft$ Solving (1)–(4) (KN)  $A_v = 2.73 \text{ kN}$  , B = 3.81 kN-.93 (b) Shear Diag: -3.2 -3.8 *V* is piecewise linear with  $\left(\frac{dV}{dx} = -0.6 \text{ kN/m}\right)$  throughout, and discontinuities equal to forces at A, C, F, B. Note that V = 0 = 1.47 kN - (0.6 kN/m)x at x = 2.45 m**Moment Diag:** *M* is piecewise parabolic  $\left(\frac{dM}{dx}\right)$  decreasing with *V*, with "breaks" in slope at C and F.





Two loads are suspended as shown from cable *ABCD*. Knowing that  $d_C = 1.5$  ft, determine (*a*) the distance  $d_B$ , (*b*) the components of the reaction at *A*, (*c*) the maximum tension in the cable.





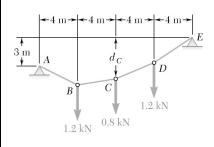
SOLUTION

Godi

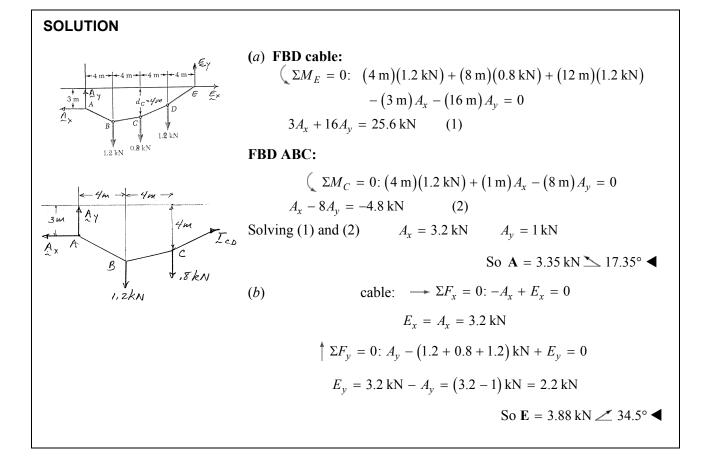
#### **PROBLEM 7.89**

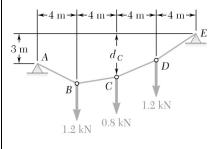
Two loads are suspended as shown from cable ABCD. Knowing that the maximum tension in the cable is 720 lb, determine (a) the distance  $d_B$ , (*b*) the distance  $d_C$ .

### $(\Sigma M_A = 0: (10 \text{ ft})D_y - (8 \text{ ft})(450 \text{ lb}) - (4 \text{ ft})(600 \text{ lb}) = 0$ FBD cable: $\mathbf{A}_{v} = 450 \, \text{lb}$ $-2F_x = 0: A_x - B_x = 0$ Since $A_x = B_x$ ; And $D_y > A_y$ , Tension $T_{CD} > T_{AB}$ So $T_{CD} = T_{max} = 720 \text{ lb}$ $D_x = \sqrt{(720 \text{ lb})^2 - (600 \text{ lb})^2} = 398$ FBD pt D: $\longleftarrow \Sigma F_x = 0: A_x - B_x = 0$ $D_x = \sqrt{(720 \text{ lb})^2 - (600 \text{ lb})^2} = 398 \text{ lb} = A_x$ $\frac{d_C}{600 \text{ lb}} = \frac{2 \text{ ft}}{398 \text{ lb}}$ $d_C = 3.015 \text{ ft}$ 7*20* || (a) $d_B = 4.52 \text{ ft} \blacktriangleleft$ $\frac{d_B}{450\,\mathrm{lb}} = \frac{4\,\mathrm{ft}}{398\,\mathrm{lb}}$ FBD pt. A: (b) $d_C = 3.02 \text{ ft} \blacktriangleleft$ 3981b TAB 45016 TAR

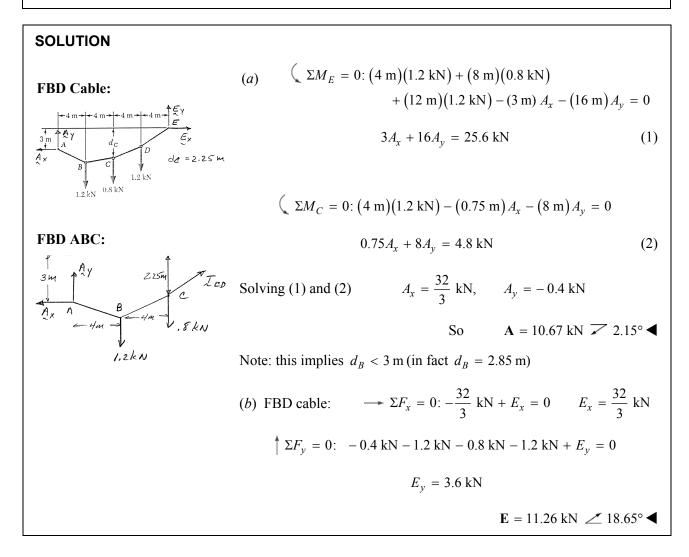


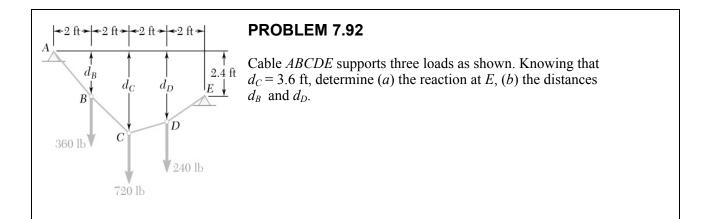
Knowing that  $d_C = 4$  m, determine (*a*) the reaction at *A*, (*b*) the reaction at *E*.

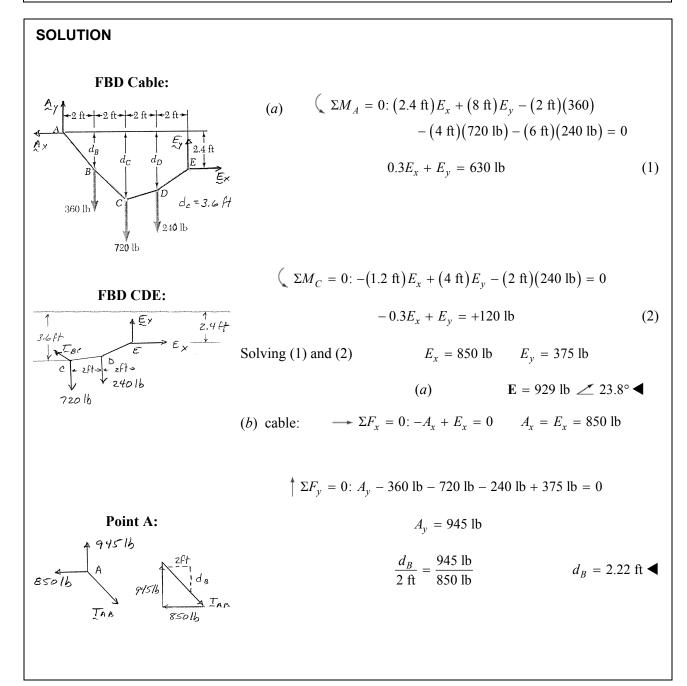


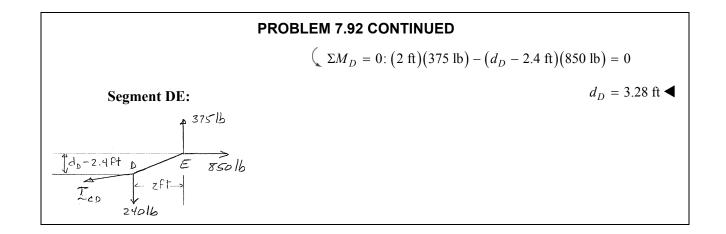


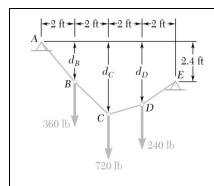
Knowing that  $d_C = 2.25$  m, determine (a) the reaction at A, (b) the reaction at E.



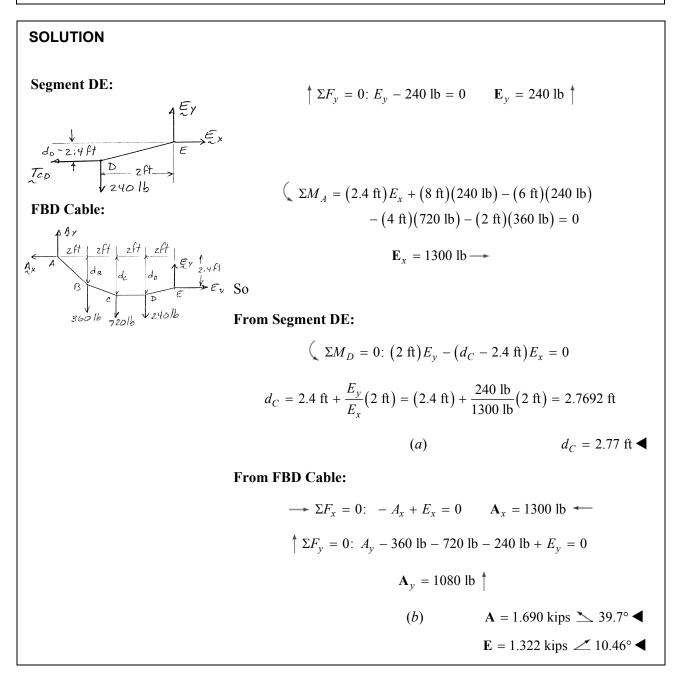


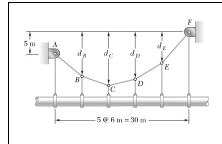






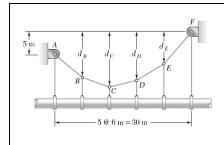
Cable *ABCDE* supports three loads as shown. Determine (*a*) the distance  $d_C$  for which portion *CD* of the cable is horizontal, (*b*) the corresponding reactions at the supports.





An oil pipeline is supported at 6-m intervals by vertical hangers attached to the cable shown. Due to the combined weight of the pipe and its contents, the tension in each hanger is 4 kN. Knowing that  $d_c = 12$  m, determine (*a*) the maximum tension in the cable, (*b*) the distance  $d_D$ .

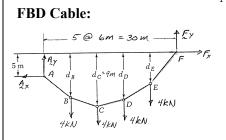
SOLUTION Note:  $\mathbf{A}_{v}$  and  $\mathbf{F}_{v}$  shown are forces on cable, assuming the 4 kN loads **FBD Cable:** at A and F act on supports.  $\sum M_F = 0: (6 \text{ m}) [1(4 \text{ kN}) + 2(4 \text{ kN}) + 3(4 \text{ kN}) + 4(4 \text{ kN})] - (30 \text{ m}) A_y - (5 \text{ m}) A_x = 0$  $A_{\rm r} + 6A_{\rm v} = 48 \, \rm kN$ (1) **FBD ABC:**  $(\Sigma M_C = 0: (6 \text{ m})(4 \text{ kN}) + (7 \text{ m})A_x - (12 \text{ m})A_y = 0$  $7A_x - 12A_y = -24 \text{ kN}$ (2)Solving (1) and (2)  $A_x = 8 \text{ kN} \longrightarrow A_y = \frac{20}{3} \text{ kN}$ From FBD Cable:  $\longrightarrow \Sigma F_x = 0$ :  $-A_x + F_x = 0$   $F_x = A_x = 8 \text{ kN}$  $\sum F_v = 0: A_v - 4(4 \text{ kN}) + F_v = 0$  $F_y = 16 \text{ kN} - A_y = \left(16 - \frac{20}{3}\right) \text{kN} = \frac{28}{3} \text{ kN} > A_y$ So  $T_{EF} > T_{AB}$   $T_{max} = T_{EF} = \sqrt{F_x^2 + F_y^2}$ **FBD DEF:** do  $d_D = 11.00 \text{ m}$ *(b)* 



Solve Prob. 7.94 assuming that  $d_C = 9$  m.

#### SOLUTION

**FBD CDEF:** 

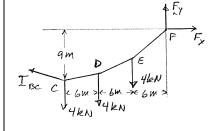


Note: 4 kN loads at A and F act directly on supports, not on cable.

$$\sum M_{A} = 0: (30 \text{ m})F_{y} - (5 \text{ m})F_{x}$$
$$- (6 \text{ m})[1(4 \text{ kN}) + 2(4 \text{ kN}) + 3(4 \text{ kN}) + 4(4 \text{ kN})] = 0$$
$$F_{x} - 6F_{y} = -48 \text{ kN}$$
(1)

$$\Sigma M_C = 0: (18)F_y - (9 \text{ m})F_x - (12 \text{ m})(4 \text{ kN}) - (6 \text{ m})(4 \text{ kN}) = 0$$

$$E - 2F_y = -8 \text{ kN}$$



*(a)* 

Since slope EF > slope AB this is  $T_{\text{max}}$ 

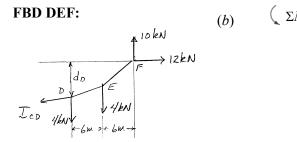
$$T_{\rm max} = 15.62 \text{ kN} \blacktriangleleft$$

Also could note from FBD cable

$$\sum F_y = 0: A_y + F_y - 4(4 \text{ kN}) = 0$$

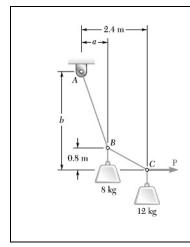
$$A_y = 16 \text{ kN} - 12 \text{ kN} = 4 \text{ kN}$$
Thus  $A_y < F_y$  and  $T_{AB} < T_{EF}$ 

$$M_D = 0: (12 \text{ m})(10 \text{ kN}) - d_D(12 \text{ kN}) - (6 \text{ m})(4 \text{ kN})$$

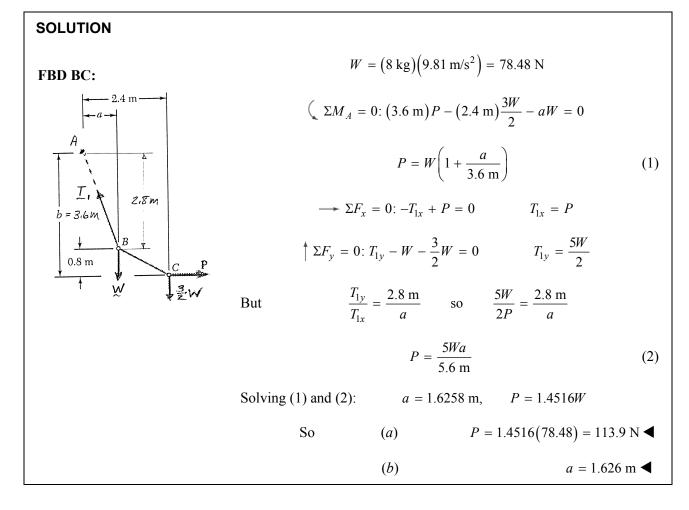


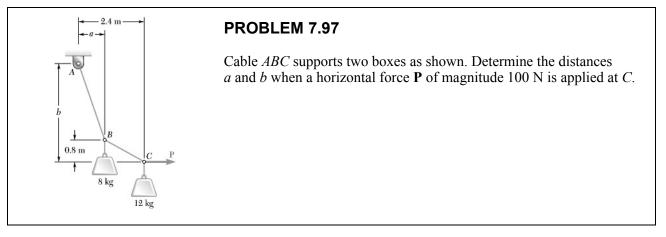
 $d_D = 8.00 \text{ m} \blacktriangleleft$ 

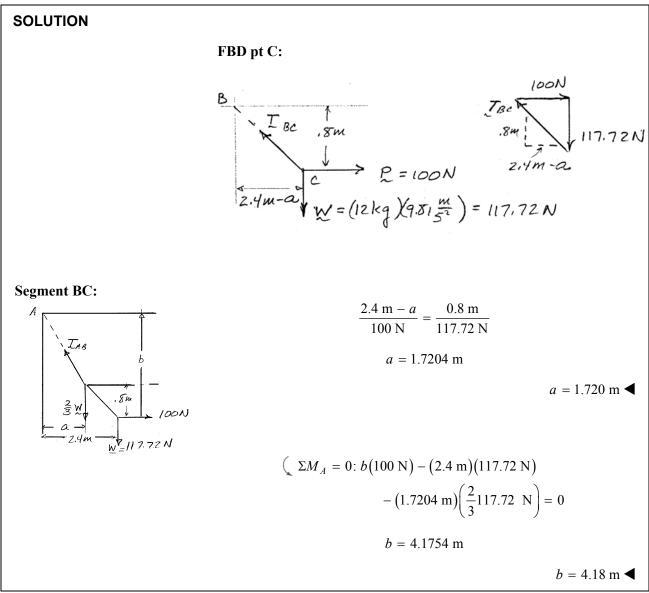
= 0

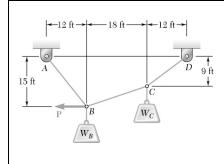


Cable *ABC* supports two boxes as shown. Knowing that b = 3.6 m, determine (*a*) the required magnitude of the horizontal force **P**, (*b*) the corresponding distance *a*.

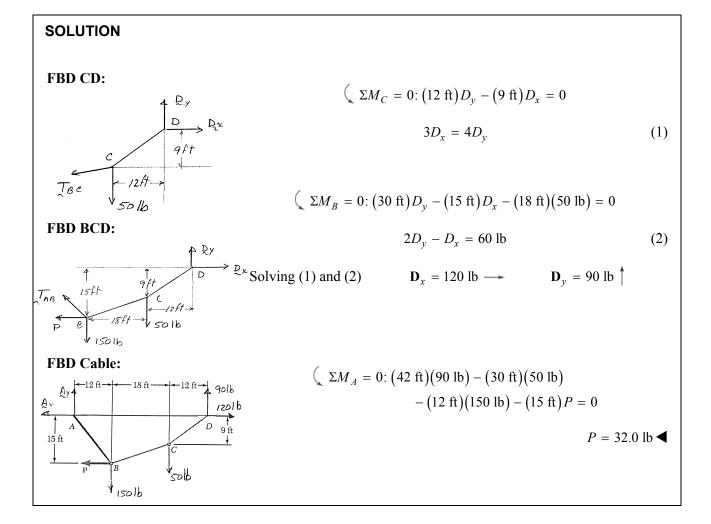


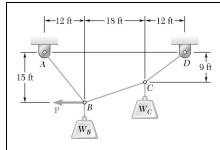




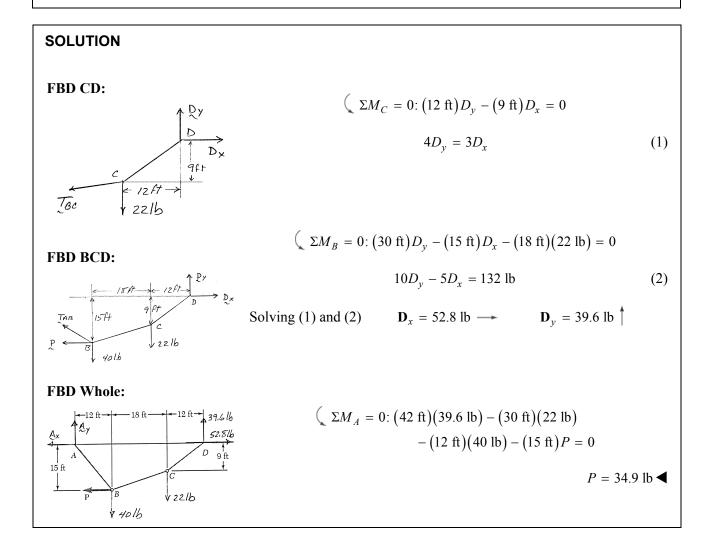


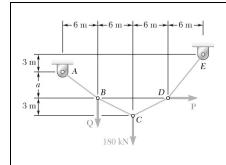
Knowing that  $W_B = 150$  lb and  $W_C = 50$  lb, determine the magnitude of the force **P** required to maintain equilibrium.





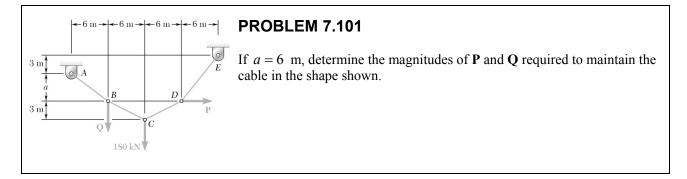
Knowing that  $W_B = 40$  lb and  $W_C = 22$  lb, determine the magnitude of the force **P** required to maintain equilibrium.

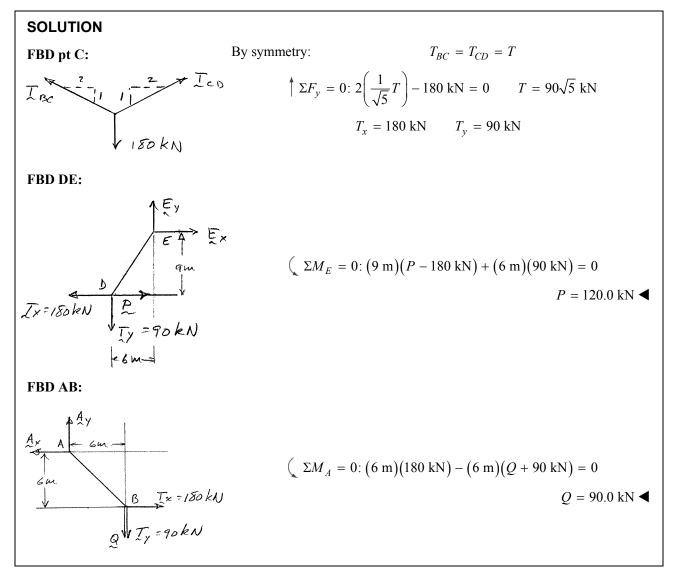




If a = 4.5 m, determine the magnitudes of **P** and **Q** required to maintain the cable in the shape shown.

SOLUTION  $T_{BC} = T_{CD} = T$ By symmetry: FBD pt C:  $\uparrow$  ΣF<sub>y</sub> = 0: 2 $\left(\frac{1}{\sqrt{5}}T\right)$  - 180 kN = 0  $T = 90\sqrt{5}$  kN TBE  $T_x = 180 \text{ kN} \qquad T_y = 90 \text{ kN}$ 180 KN Segment DE:  $\sum M_E = 0: (7.5 \text{ m})(P - 180 \text{ kN}) + (6 \text{ m})(90 \text{ kN}) = 0$ Seg DE - 6m -7,5m P = 108.0 kN→₽ Tx=180KN D Ty=90 KN Segment AB:  $(\Sigma M_A = 0: (4.5 \text{ m})(180 \text{ kN}) - (6 \text{ m})(Q + 90 \text{ kN}) = 0$ Q = 45.0 kN4.5m > Tx=180 kN Q VIJy=90KN





A transmission cable having a mass per unit length of 1 kg/m is strung between two insulators at the same elevation that are 60 m apart. Knowing that the sag of the cable is 1.2 m, determine (*a*) the maximum tension in the cable, (*b*) the length of the cable.

#### SOLUTION

(a) Since  $h = 1.2 \text{ m} \ll L = 30 \text{ m}$  we can approximate the load as evenly distributed in the horizontal direction.

$$w = 1 \text{ kg/m} (9.81 \text{ m/s}^2) = 9.81 \text{ N/m}.$$
  

$$w = (60 \text{ m}) (9.81 \text{ N/m})$$
  

$$w = 588.6 \text{ N}$$

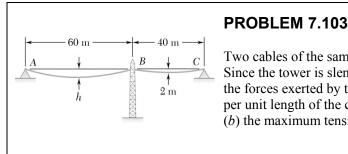
Also we can assume that the weight of half the cable acts at the  $\frac{1}{4}$  chord point.

FBD half-cable:

$$T_{max} = 3.69 \text{ kN} \blacktriangleleft$$

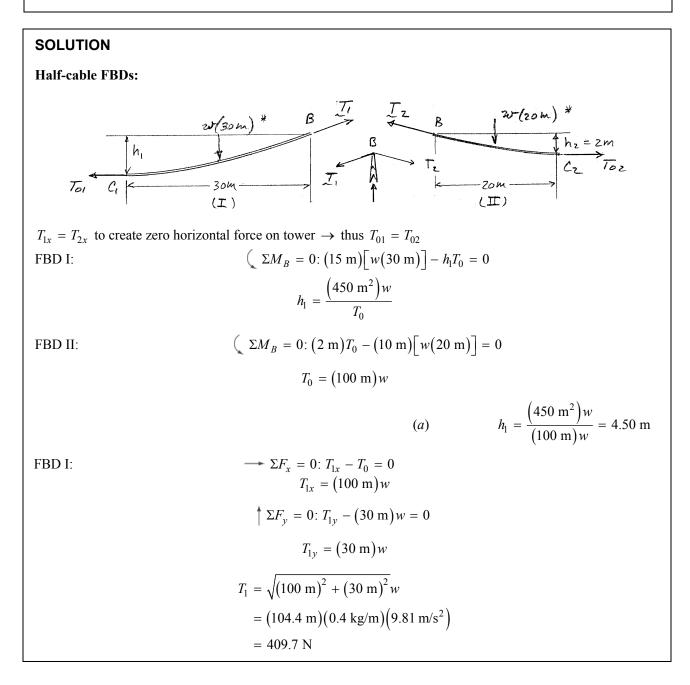
$$(b) \qquad s_B = x_B \left[ 1 + \frac{2}{3} \left( \frac{y_B}{30} \right)^2 - \frac{2}{5} \left( \frac{1.2}{30} \right)^4 + \cdots \right] = 30.048 \text{ m} \text{ so } s = 2s_B = 60.096 \text{ m} \\ s = 60.1 \text{ m} \checkmark$$

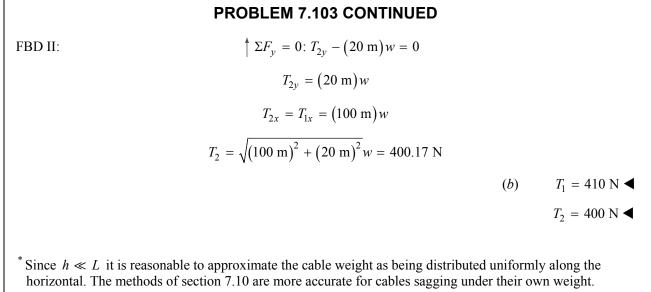
Note: The more accurate methods of section 7.10, which assume the load is evenly distributed along the length instead of horizontally, yield  $T_{\text{max}} = 3690.5 \text{ N}$  and s = 60.06 m. Answers agree to 3 digits at least.



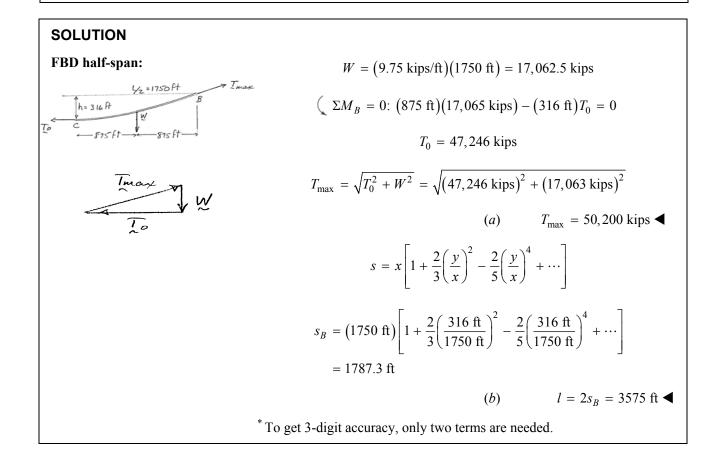
# Two cables of the same gauge are attached to a transmission tower at *B*.

Since the tower is slender, the horizontal component of the resultant of the forces exerted by the cables at B is to be zero. Knowing that the mass per unit length of the cables is 0.4 kg/m, determine (a) the required sag h, (b) the maximum tension in each cable.

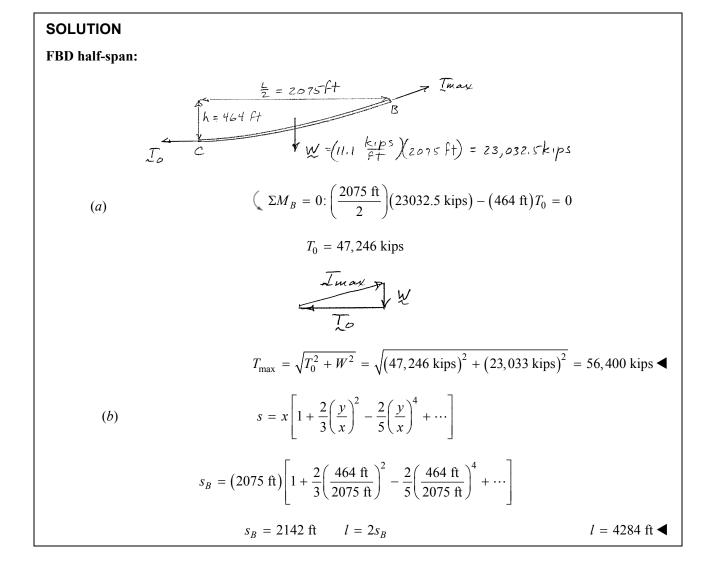


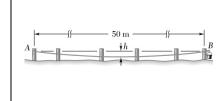


The center span of the George Washington Bridge, as originally constructed, consisted of a uniform roadway suspended from four cables. The uniform load supported by each cable was w = 9.75 kips/ft along the horizontal. Knowing that the span *L* is 3500 ft and that the sag *h* is 316 ft, determine for the original configuration (*a*) the maximum tension in each cable, (*b*) the length of each cable.



Each cable of the Golden Gate Bridge supports a load w = 11.1 kips/ft along the horizontal. Knowing that the span *L* is 4150 ft and that the sag *h* is 464 ft, determine (*a*) the maximum tension in each cable, (*b*) the length of each cable.





To mark the positions of the rails on the posts of a fence, a homeowner ties a cord to the post at A, passes the cord over a short piece of pipe attached to the post at B, and ties the free end of the cord to a bucket filled with bricks having a total mass of 20 kg. Knowing that the mass per unit length of the rope is 0.02 kg/m and assuming that A and B are at the same elevation, determine (a) the sag h, (b) the slope of the cable at B. Neglect the effect of friction.

#### SOLUTION

FBD pulley:

$$T_{max} = (zokg)(9.81 \frac{M}{3^2}) = 196.2 N$$

$$(\Sigma M_P = 0: (T_{max} - W_B)r = 0$$

$$T_{max} = W_B = 196.2 N$$

FBD half-span:\*

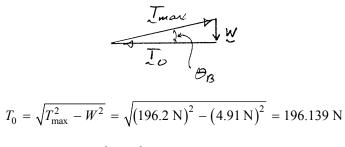
$$\frac{1}{2} = 25m$$

$$\frac{1}{2} = 25m$$

$$\frac{1}{2} = 25m$$

$$\frac{1}{2} = 196.2N$$

$$\frac{1}{2} = \frac{1}{2} = \frac{1}{2}$$



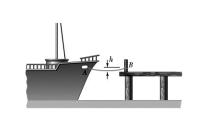
$$\left(\Sigma M_B = 0: \left(\frac{25 \text{ m}}{2}\right) (4.905 \text{ N}) - h(196.139 \text{ N}) = 0$$

*(a)* 

h = 0.3126 m = 313 mm

(b) 
$$\theta_B = \sin^{-1} \frac{W}{T_{\text{max}}} = \sin^{-1} \left( \frac{4.905 \text{ N}}{196.2 \text{ N}} \right) = 1.433^{\circ} \blacktriangleleft$$

\*See note Prob. 7.103



A small ship is tied to a pier with a 5-m length of rope as shown. Knowing that the current exerts on the hull of the ship a 300-N force directed from the bow to the stern and that the mass per unit length of the rope is 2.2 kg/m, determine (*a*) the maximum tension in the rope, (*b*) the sag *h*. [*Hint:* Use only the first two terms of Eq. (7.10).]

## SOLUTION (a) **FBD ship:** To It It $\longrightarrow \Sigma F_x = 0: T_0 - 300 \text{ N} = 0$ $T_0 = 300 \text{ N}$ FBD half-span:\* $\begin{array}{c|c} & \downarrow & \downarrow \\ A & & \downarrow \\ A & & \downarrow \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ &$ $c = \frac{1}{2} \frac{kq}{m} \left( \frac{q}{51} \frac{M}{5^2} \right) \left( 2.5 \text{ m} \right) = 53.955 \text{ N}$ $T_{\text{max}} = \sqrt{T_0^2 + W^2} = \sqrt{(300 \text{ N})^2 = (54 \text{ N})^2} = 305 \text{ N} \blacktriangleleft$ $\sum M_A = 0$ : $hT_x - \frac{L}{4}W = 0$ $h = \frac{LW}{4T_x}$ *(b)* W To = To $s = x \left[ 1 + \frac{2}{3} \left( \frac{4}{x} \right)^2 + \cdots \right]$ but $y_A = h = \frac{LW}{4T_x}$ so $\frac{y_A}{x_A} = \frac{W}{2T_x}$ $(2.5 \text{ m}) = \frac{L}{2} \left[ 1 + \frac{2}{3} \left( \frac{53.955 \text{ N}}{600 \text{ N}} \right)^2 - \dots \right] \rightarrow L = 4.9732 \text{ m}$ So $h = \frac{LW}{4T} = 0.2236 \text{ m}$ *h* = 224 mm ◀ \*See note Prob. 7.103

The center span of the Verrazano-Narrows Bridge consists of two uniform roadways suspended from four cables. The design of the bridge allowed for the effect of extreme temperature changes which cause the sag of the center span to vary from  $h_w = 386$  ft in winter to  $h_s = 394$  ft in summer. Knowing that the span is L = 4260 ft, determine the change in length of the cables due to extreme temperature changes.

#### SOLUTION

$$s = x \left[ 1 + \frac{2}{3} \left( \frac{y}{x} \right)^2 - \frac{2}{5} \left( \frac{y}{x} \right)^4 + \cdots \right]$$
$$l = 2s_{\text{TOT}} = L \left[ 1 + \frac{2}{3} \left( \frac{h}{L/2} \right)^2 - \frac{2}{5} \left( \frac{h}{L/2} \right)^2 + \cdots \right]$$

Winter:

Knowing

$$l_w = (4260 \text{ ft}) \left[ 1 + \frac{2}{3} \left( \frac{386 \text{ ft}}{2130 \text{ ft}} \right)^2 - \frac{2}{5} \left( \frac{386 \text{ ft}}{2130 \text{ ft}} \right)^4 + \cdots \right] = 4351.43 \text{ ft}$$

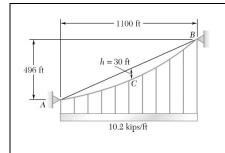
Summer:

$$l_s = (4260 \text{ ft}) \left[ 1 + \frac{2}{3} \left( \frac{394 \text{ ft}}{2130 \text{ ft}} \right)^2 - \frac{2}{5} \left( \frac{394 \text{ ft}}{2130 \text{ ft}} \right)^4 + \cdots \right] = 4355.18 \text{ ft}$$

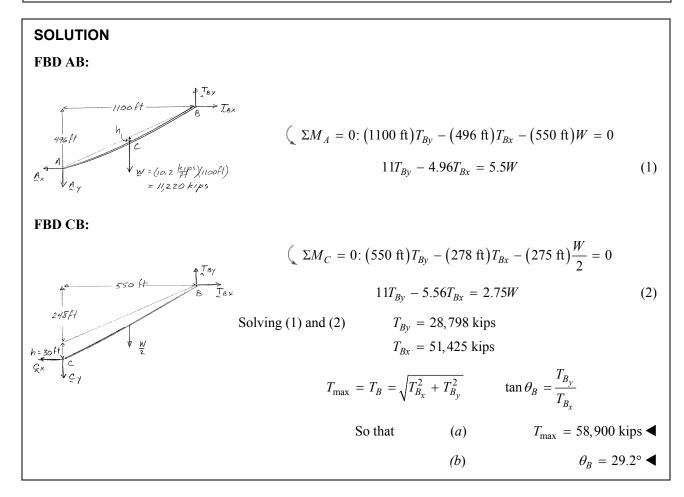
 $\Delta l = l_s - l_w = 3.75 \text{ ft} \blacktriangleleft$ 

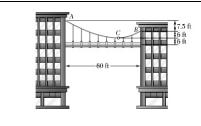
A cable of length  $L + \Delta$  is suspended between two points which are at the same elevation and a distance L apart. (a) Assuming that  $\Delta$  is small compared to L and that the cable is parabolic, determine the approximate sag in terms of L and  $\Delta$ . (b) If L = 30 m and  $\Delta = 1.2$  m, determine the approximate sag. [*Hint:* Use only the first two terms of Eq. (7.10).]

SOLUTION	
( <i>a</i> )	$s = x \left[ 1 + \frac{2}{3} \left( \frac{y}{x} \right)^2 - \cdots \right]$
	$L + \Delta = 2s_{\text{TOT}} = L \left[ 1 + \frac{2}{3} \left( \frac{h}{L/2} \right)^2 - \cdots \right]$
	$\frac{\Delta}{L} = \frac{2}{3} \left(\frac{2h}{L}\right)^2 = \frac{8}{3} \left(\frac{h}{L}\right)^2 \to h = \sqrt{\frac{3}{8}L\Delta} \blacktriangleleft$
(b)	For $L = 30 \text{ m}$ , $\Delta = 1.2 \text{ m}$ $h = 3.67 \text{ m}$

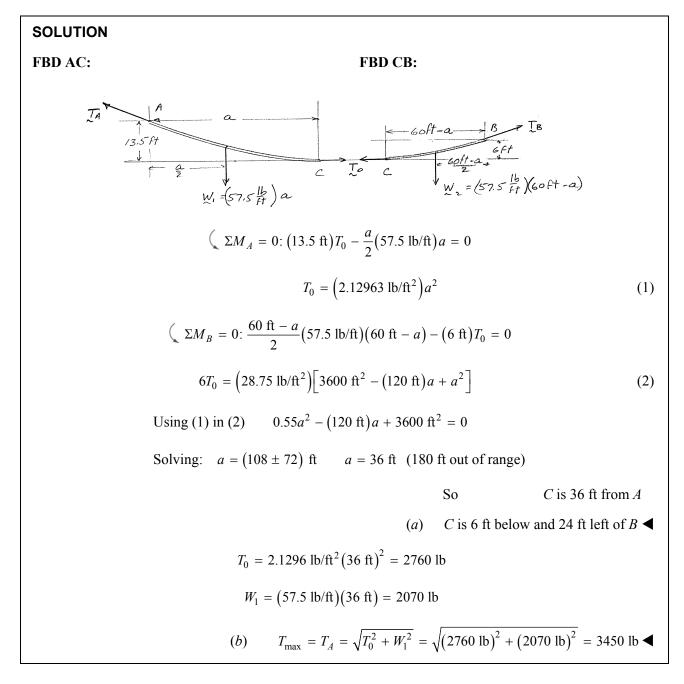


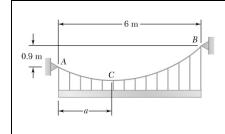
Each cable of the side spans of the Golden Gate Bridge supports a load w = 10.2 kips/ft along the horizontal. Knowing that for the side spans the maximum vertical distance *h* from each cable to the chord *AB* is 30 ft and occurs at midspan, determine (*a*) the maximum tension in each cable, (*b*) the slope at *B*.





A steam pipe weighting 50 lb/ft that passes between two buildings 60 ft apart is supported by a system of cables as shown. Assuming that the weight of the cable is equivalent to a uniformly distributed loading of 7.5 lb/ft, determine (*a*) the location of the lowest point *C* of the cable, (*b*) the maximum tension in the cable.





Chain *AB* supports a horizontal, uniform steel beam having a mass per unit length of 85 kg/m. If the maximum tension in the cable is not to exceed 8 kN, determine (*a*) the horizontal distance *a* from *A* to the lowest point *C* of the chain, (*b*) the approximate length of the chain.

SOLUTION			
$ \begin{array}{c} T_{A} \\ \downarrow A \\ \downarrow $			
$\sum M_A = 0: y_A T_0 - \frac{a}{2} wa = 0$ $\sum M_B = 0: -y_B T_0 + \frac{b}{2} wb = 0$			
$y_A = \frac{wa^2}{2T_0} \qquad \qquad$			
$d = (y_B - y_B) = \frac{w}{2T_0} (b^2 - a^2)$			
But $T_0 = \sqrt{T_B^2 - (wb)^2} = \sqrt{T_{\text{max}}^2 - (wb)^2}$			
$\therefore (2d)^{2} \left[ T_{\max}^{2} - (wb)^{2} \right] = w^{2} \left( b^{2} - a^{2} \right)^{2} = L^{2} w^{2} \left( 4b^{2} - 4Lb + L^{2} \right)$			
or $4(L^2 + d^2)b^2 - 4L^3b + \left(L^4 - 4d^2\frac{T_{\max}^2}{w^2}\right) = 0$			
Using $L = 6 \text{ m},  d = 0.9 \text{ m},  T_{\text{max}} = 8 \text{ kN},  w = (85 \text{ kg/m})(9.81 \text{ m/s}^2) = 833.85 \text{ N/m}$			
yields $b = (2.934 \pm 1.353)$ m $b = 4.287$ m (since $b > 3$ m)			
(a) $a = 6 \text{ m} - b = 1.713 \text{ m} \blacktriangleleft$			

# PROBLEM 7.112 CONTINUED

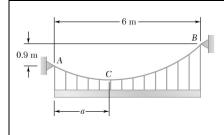
$$T_{0} = \sqrt{T_{\text{max}}^{2} - (wb)^{2}} = 7156.9 \text{ N}$$

$$\frac{y_{A}}{x_{A}} = \frac{wa}{2T_{0}} = 0.09979 \qquad \frac{y_{B}}{x_{B}} = \frac{wb}{2T_{0}} = 0.24974$$

$$l = s_{A} + s_{B} = a \left[ 1 + \frac{2}{3} \left( \frac{y_{A}}{x_{A}} \right)^{2} + \cdots \right] + b \left[ 1 + \frac{2}{3} \left( \frac{y_{B}}{x_{B}} \right)^{2} + \cdots \right]$$

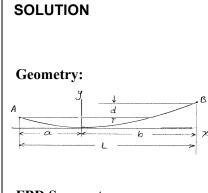
$$= (1.713 \text{ m}) \left[ 1 + \frac{2}{3} (0.09979)^{2} \right] + (4.287 \text{ m}) \left[ 1 + \frac{2}{3} (0.24974)^{2} \right] = 6.19 \text{ m}$$

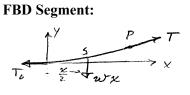
$$(b) \qquad l = 6.19 \text{ m} \blacktriangleleft$$



Chain AB of length 6.4 m supports a horizontal, uniform steel beam having a mass per unit length of 85 kg/m. Determine (a) the horizontal distance a from A to the lowest point C of the chain, (b) the maximum tension in the chain.

r





$$\left(\sum M_{P} = 0: \frac{x}{2}wx - yT_{0} = 0\right)$$

$$y = \frac{wx^{2}}{2T_{0}} \qquad \text{so} \qquad \frac{y}{x} = \frac{wx}{2T_{0}}$$
and  $d = y_{B} - y_{A} = \frac{w}{2T_{0}}\left(b^{2} - a^{2}\right)$ 

$$l = s_{A} + s_{B} = a\left[1 + \frac{2}{3}\left(\frac{y_{A}}{a}\right)^{2}\right] + b\left[1 + \frac{2}{3}\left(\frac{y_{B}}{b}\right)^{2}\right]$$

$$l - L = \frac{2}{3}\left[\left(\frac{y_{A}}{a}\right)^{2} + \left(\frac{y_{B}}{b}\right)^{2}\right] = \frac{w^{2}}{6T_{0}^{2}}\left(a^{3} + b^{3}\right)$$

$$= \frac{1}{6}\frac{4d^{2}}{\left(b^{2} - a^{2}\right)^{2}}\left(a^{3} + b^{3}\right) = \frac{2}{3}\frac{d^{2}\left(a^{3} + b^{3}\right)}{\left(b^{2} - a^{2}\right)^{2}}$$

Using l = 6.4 m, L = 6 m, d = 0.9 m, b = 6 m - a, and solving for a, knowing that a < 3 ft

$$a = 2.2196 \text{ m}$$
 (a)  $a = 2.22 \text{ m}$ 

 $T_0 = \frac{w}{2d} \left( b^2 - a^2 \right)$ 

Then

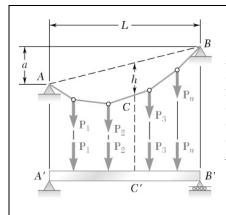
Also

And with 
$$w = (85 \text{ kg/m})(9.81 \text{ m/s}^2) = 833.85 \text{ N/m}$$

And b = 6 m - a = 3.7804 m  $T_0 = 4338 \text{ N}$ 

wb

$$T_{\text{max}} = T_B = \sqrt{T_0^2 + (wb)^2}$$
  
=  $\sqrt{(4338 \text{ N})^2 + (833.85 \text{ N/m})^2 (3.7804 \text{ m})^2}$   
 $T_{\text{max}} = 5362 \text{ N}$  (b)  $T_{\text{max}} = 5.36 \text{ kN}$ 



A cable AB of span L and a simple beam A'B' of the same span are subjected to identical vertical loadings as shown. Show that the magnitude of the bending moment at a point C' in the beam is equal to the product,  $T_0h$  where  $T_0$  is the magnitude of the horizontal component of the tension force in the cable and h is the vertical distance between point C and the chord joining the points of support A and B.

# SOLUTION

FBD AC:

To A

ABX

Acy

Ρ,

P

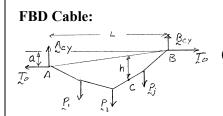
Ρ,

X

 $V_{P_2}$ 

VPN

**FBD Beam:** 



ß

B,

Mc

P1

$$\Sigma M_B = 0: LA_{Cy} + aT_0 - \Sigma M_B \text{ loads} = 0$$
(1)

 $\mathcal{T}_{\mathcal{F}}$  (Where  $\Sigma M_{B \text{ loads}}$  includes all applied loads)

$$\left(\Sigma M_C = 0: xA_{Cy} - \left(h - a\frac{x}{L}\right)T_0 - \Sigma M_{C \text{ left}} = 0$$
(2)

(Where  $\Sigma M_{C \text{ left}}$  includes all loads left of *C*)

$$\frac{x}{L}(1) - (2): \quad hT_0 - \frac{x}{L} \Sigma M_{B \text{ loads}}^2 + \Sigma M_{C \text{ left}}^2 = 0$$
(3)

 $\left( \sum M_B = 0 : LA_{By} - \sum M_B^{\circ}_{loads} = 0 \right)$  (4)

$$\sum M_C = 0 \colon xA_{By} - \Sigma M_C = 0$$
(5)

FBD AC:

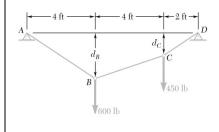
ABX

ABY

ABY

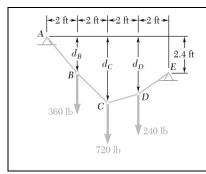
$$\frac{x}{L}(4) - (5): -\frac{x}{L} \Sigma M_{B \text{ loads}}^{2} + \Sigma M_{C \text{ left}}^{2} + M_{C} = 0$$
(6)

Comparing (3) and (6) 
$$M_C = hT_0$$
 Q.E.D.

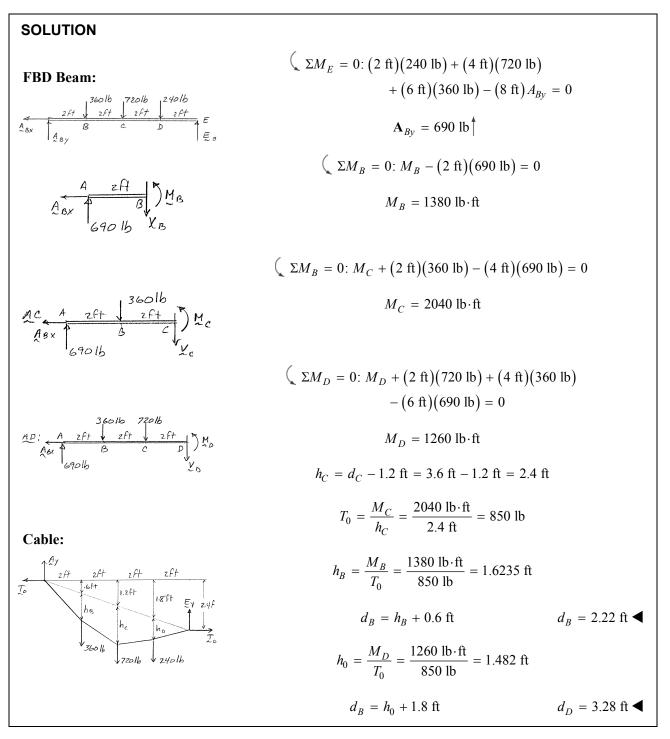


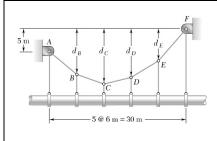
Making use of the property established in Prob. 7.114, solve the problem indicated by first solving the corresponding beam problem. Prob. 7.89*a*.

SOLUTION  $(\Sigma M_D = 0: (2 \text{ ft})(450 \text{ lb}) + (6 \text{ ft})(600 \text{ lb}) - (10 \text{ ft})\mathbf{A}_{Bv} = 0$ **FBD Beam:**  $A_{Bv} = 450 \text{ lb}$ 4Ft 2Ft D 4 FI  $\sum M_B = 0: M_B - (4 \text{ ft})(450 \text{ lb}) = 0$ 600 lb Section AB:  $M_B = 1800 \text{ lb} \cdot \text{ft}$ ) MB 4Ft ABX  $\sum M_A = 0: (10 \text{ ft}) D_{Cy} - (8 \text{ ft}) (450 \text{ lb}) - (4 \text{ ft}) (600 \text{ lb}) = 0$ 4501 Cable:  $D_{Cv} = 600 \text{ lb}$ To A  $d_B = \frac{M_B}{T_0} = \frac{1800 \text{ lb} \cdot \text{ft}}{398 \text{ lb}} = 4.523 \text{ ft}$  $d_{R} = 4.52 \text{ ft} \blacktriangleleft$ 



Making use of the property established in Prob. 7.114, solve the problem indicated by first solving the corresponding beam problem. Prob. 7.92*b*.

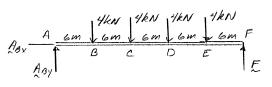




Making use of the property established in Prob. 7.114, solve the problem indicated by first solving the corresponding beam problem. Prob. 7.94*b*.

# SOLUTION

#### **FBD Beam:**



By symmetry:  $\mathbf{A}_{By} = \mathbf{F} = 8 \, kN$ 

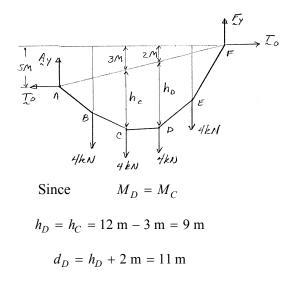
$$M_B = M_E; \qquad M_C = M_D$$

$$(\Sigma M_C = 0: M_C + (6 \text{ m})(4 \text{ kN}) - (12 \text{ m})(8 \text{ kN}) = 0$$

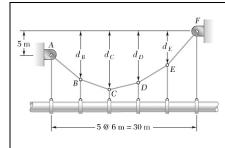
$$M_C = 72 \text{ kN} \cdot \text{m}$$
 so  $M_D = 72 \text{ kN} \cdot \text{m}$ 

Cable:

AC:



 $d_D = 11.00 \text{ m} \blacktriangleleft$ 



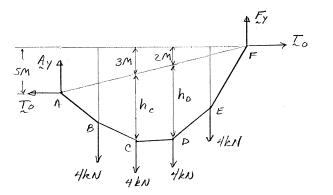
Making use of the property established in Prob. 7.114, solve the problem indicated by first solving the corresponding beam problem. Prob. 7.95*b*.

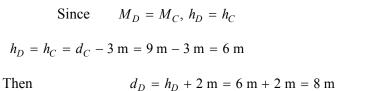
# SOLUTION

FBD Beam:

By symmetry:  $M_B = M_E$  and  $M_C = M_D$ 

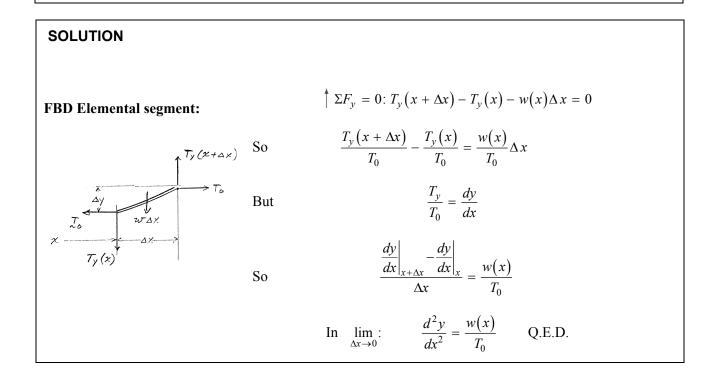
Cable:



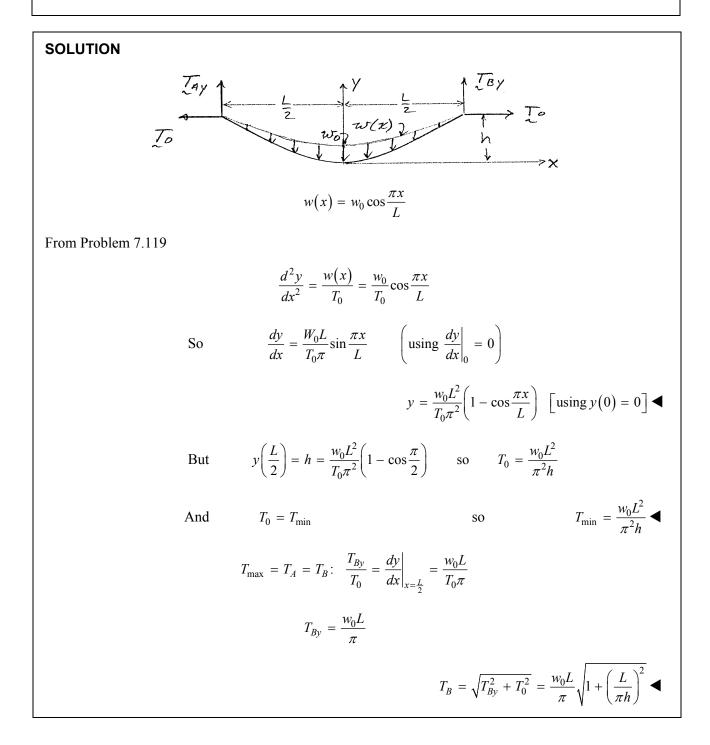


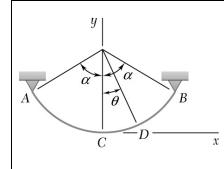
 $d_D = 8.00 \text{ m} \blacktriangleleft$ 

Show that the curve assumed by a cable that carries a distributed load w(x) is defined by the differential equation  $d^2y/dx^2 = w(x)/T_0$ , where  $T_0$  is the tension at the lowest point.

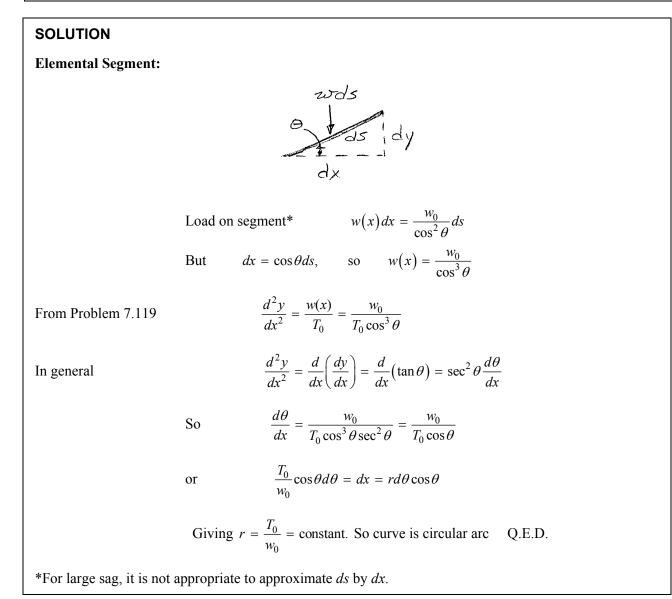


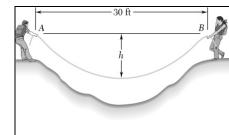
Using the property indicated in Prob. 7.119, determine the curve assumed by a cable of span *L* and sag *h* carrying a distributed load  $w = w_0 \cos(\pi x/L)$ , where *x* is measured from mid-span. Also determine the maximum and minimum values of the tension in the cable.





If the weight per unit length of the cable *AB* is  $w_0 / \cos^2 \theta$ , prove that the curve formed by the cable is a circular arc. (*Hint:* Use the property indicated in Prob. 7.119.)



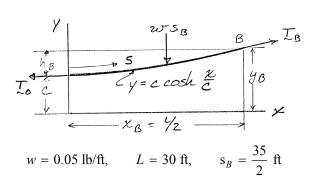


# SOLUTION

Half-span:

# <sup>B</sup> PROBLEM 7.122

Two hikers are standing 30-ft apart and are holding the ends of a 35-ft length of rope as shown. Knowing that the weight per unit length of the rope is 0.05 lb/ft, determine (*a*) the sag h, (*b*) the magnitude of the force exerted on the hand of a hiker.



$$s_B = c \ \sinh \frac{y_B}{x_B}$$

$$17.5 \text{ ft} = c \sinh\left(\frac{15 \text{ ft}}{c}\right)$$

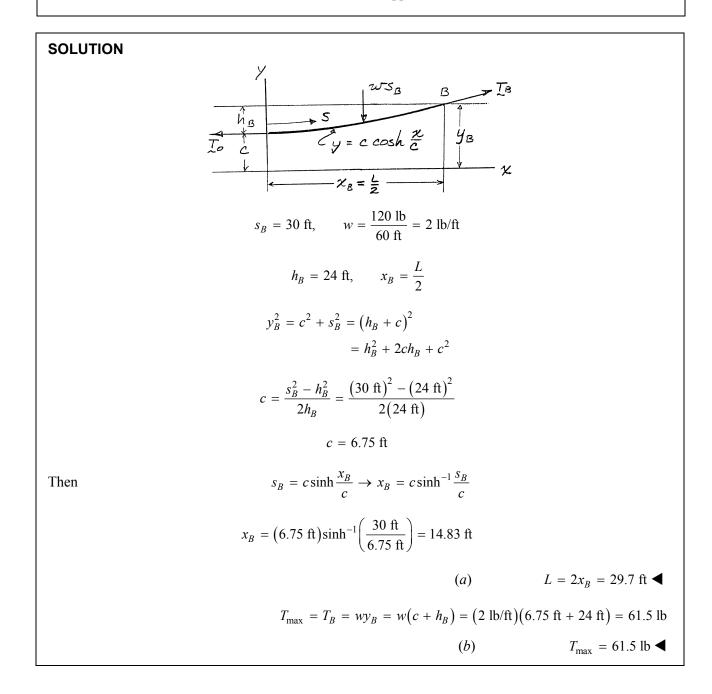
Solving numerically,

$$c = 15.36 \text{ ft}$$

Then

$$y_B = c \cosh \frac{x_B}{c} = (15.36 \text{ ft}) \cosh \frac{15 \text{ ft}}{15.36 \text{ ft}} = 23.28 \text{ ft}$$
(a)  $h_B = y_B - c = 23.28 \text{ ft} - 15.36 \text{ ft} = 7.92 \text{ ft} \blacktriangleleft$ 
(b)  $T_B = wy_B = (0.05 \text{ lb/ft})(23.28 \text{ ft}) = 1.164 \text{ lb} \blacktriangleleft$ 

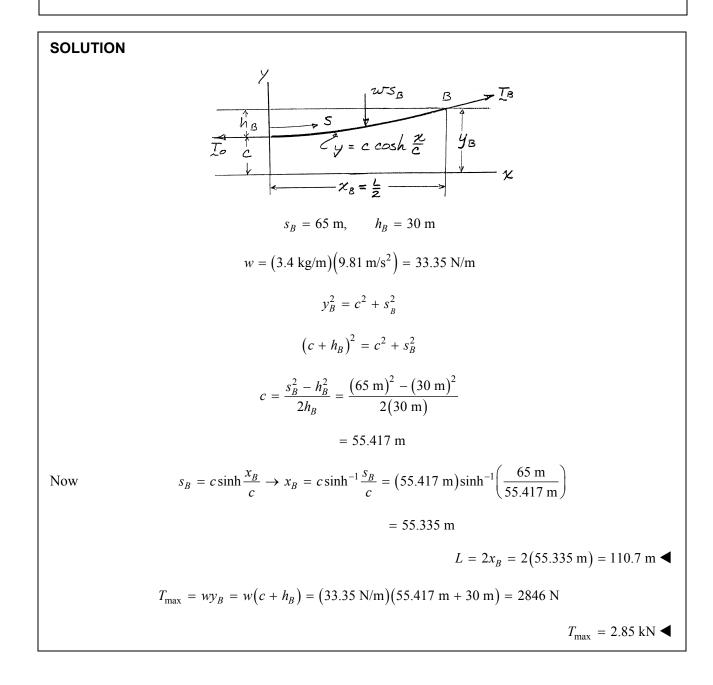
A 60-ft chain weighing 120 lb is suspended between two points at the same elevation. Knowing that the sag is 24 ft, determine (a) the distance between the supports, (b) the maximum tension in the chain.

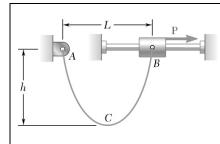


A 200-ft steel surveying tape weighs 4 lb. If the tape is stretched between two points at the same elevation and pulled until the tension at each end is 16 lb, determine the horizontal distance between the ends of the tape. Neglect the elongation of the tape due to the tension.

# SOLUTION To $s_B = 100 \text{ ft}, \qquad w = \frac{4 \text{ lb}}{200 \text{ ft}} = 0.02 \text{ lb/ft}$ $T_{\rm max} = 16 \ \rm lb$ $T_{\text{max}} = T_B = w y_B$ $y_B = \frac{T_B}{w} = \frac{16 \text{ lb}}{0.02 \text{ lb/ft}} = 800 \text{ ft}$ $c^2 = y_B^2 - s_B^2$ $c = \sqrt{(800 \text{ ft})^2 - (100 \text{ ft})^2} = 793.73 \text{ ft}$ $y_B = x_B \cosh \frac{x_B}{c} \rightarrow x_B = c \cosh^{-1} \frac{y_B}{c}$ But $= (793.73 \text{ ft}) \cosh^{-1}\left(\frac{800 \text{ ft}}{793.73 \text{ ft}}\right) = 99.74 \text{ ft}$ $L = 2x_B = 2(99.74 \text{ ft}) = 199.5 \text{ ft} \blacktriangleleft$

An electric transmission cable of length 130 m and mass per unit length of 3.4 kg/m is suspended between two points at the same elevation. Knowing that the sag is 30 m, determine the horizontal distance between the supports and the maximum tension.

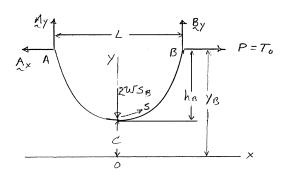




A 30-m length of wire having a mass per unit length of 0.3 kg/m is attached to a fixed support at *A* and to a collar at *B*. Neglecting the effect of friction, determine (*a*) the force **P** for which h = 12 m, (*b*) the corresponding span *L*.



FBD Cable:



$$s = 30 \text{ m}$$
 (so  $s_B = \frac{30 \text{ m}}{2} = 15 \text{ m}$ )

$$w = (0.3 \text{ kg/m})(9.81 \text{ m/s}^2) = 2.943 \text{ N/m}$$

 $h_B = 12 \text{ m}$ 

 $y_B^2 = (c + h_B)^2 = c^2 + s_B^2$ 

So

$$c = \frac{s_B^2 - h_B^2}{2h_B}$$
$$c = \frac{(15 \text{ m})^2 - (12 \text{ m})^2}{2(12 \text{ m})} = 3.375 \text{ m}$$

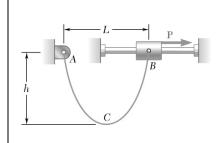
Now

$$s_B = c \sinh \frac{x_B}{c} \to x_B = c \sinh^{-1} \frac{s_B}{c} = (3.375 \text{ m}) \sinh^{-1} \left(\frac{15 \text{ m}}{3.375 \text{ m}}\right)$$

$$x_B = 7.4156 \text{ m}$$

$$P = T_0 = wc = (2.943 \text{ N/m})(3.375 \text{ m}) \qquad (a) \qquad \mathbf{P} = L = 2x_B = 2(7.4156 \text{ m}) \qquad (b) \qquad L$$

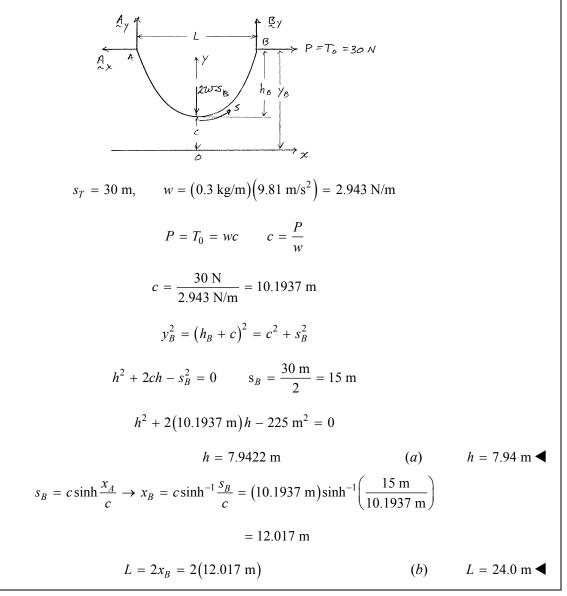
$$\mathbf{P} = 9.93 \text{ N} \longrightarrow \blacktriangleleft$$
$$L = 14.83 \text{ m} \blacktriangleleft$$

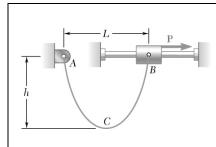


A 30-m length of wire having a mass per unit length of 0.3 kg/m is attached to a fixed support at *A* and to a collar at *B*. Knowing that the magnitude of the horizontal force applied to the collar is P = 30 N, determine (*a*) the sag *h*, (*b*) the corresponding span *L*.

# SOLUTION

#### **FBD Cable:**





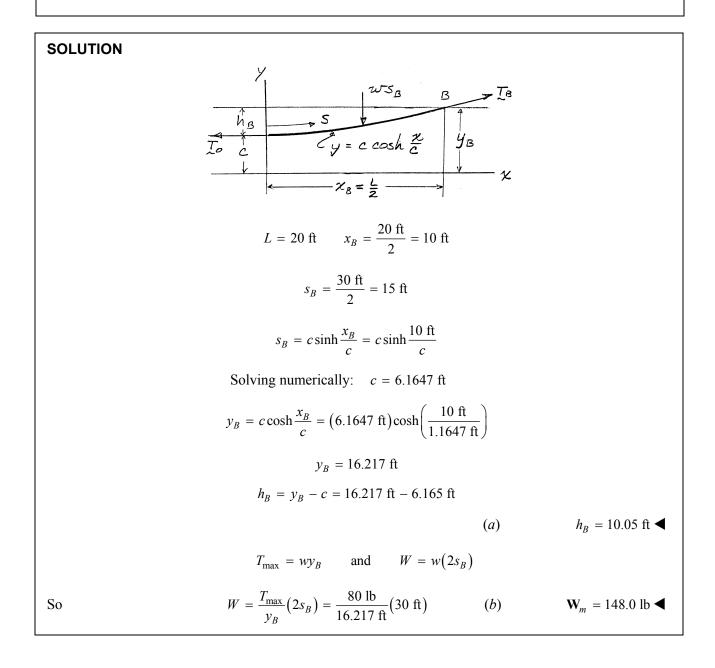
A 30-m length of wire having a mass per unit length of 0.3 kg/m is attached to a fixed support at A and to a collar at B. Neglecting the effect of friction, determine (a) the sag h for which L = 22.5 m, (b) the corresponding force **P**.

# SOLUTION

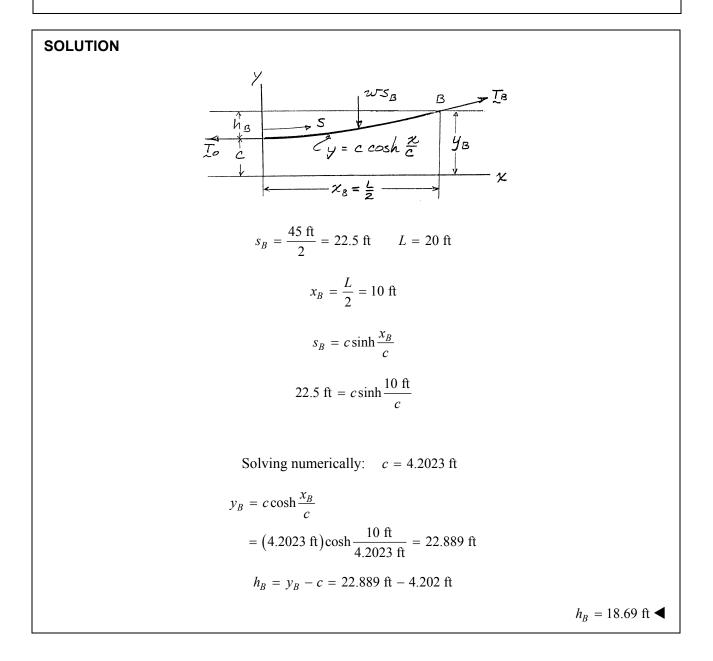
FBD Cable:

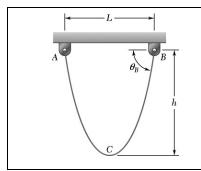
DD Cable:		
$A_{\gamma}$ $A_{\gamma$	6	
Δ		
$w = (0.3 \text{ kg/m})(9.81 \text{ m/s}^2) = 2.943 \text{ N/m}$	1	
L = 22.5  m		
$s_B = c \sinh \frac{x_B}{c} = c \sinh \frac{L/2}{c}$		
$15 \text{ m} = c \sinh \frac{11.25 \text{ m}}{c}$		
Solving numerically: $c = 8.328$ m		
$y_B^2 = c^2 + s_B^2 = (8.328 \text{ m})^2 + (15 \text{ m})^2 = 294.36 \text{ m}^2$	$y_B = 17.157 \text{ r}$	n
$h_B = y_B - c = 17.157 \text{ m} - 8.328 \text{ m}$		
	<i>(a)</i>	$h_B = 8.83 \text{ m} \blacktriangleleft$
P = wc = (2.943  N/m)(8.328  m)	(b)	$\mathbf{P} = 24.5 \text{ N} \longrightarrow \blacktriangleleft$

A 30-ft wire is suspended from two points at the same elevation that are 20 ft apart. Knowing that the maximum tension is 80 lb, determine (a) the sag of the wire, (b) the total weight of the wire.

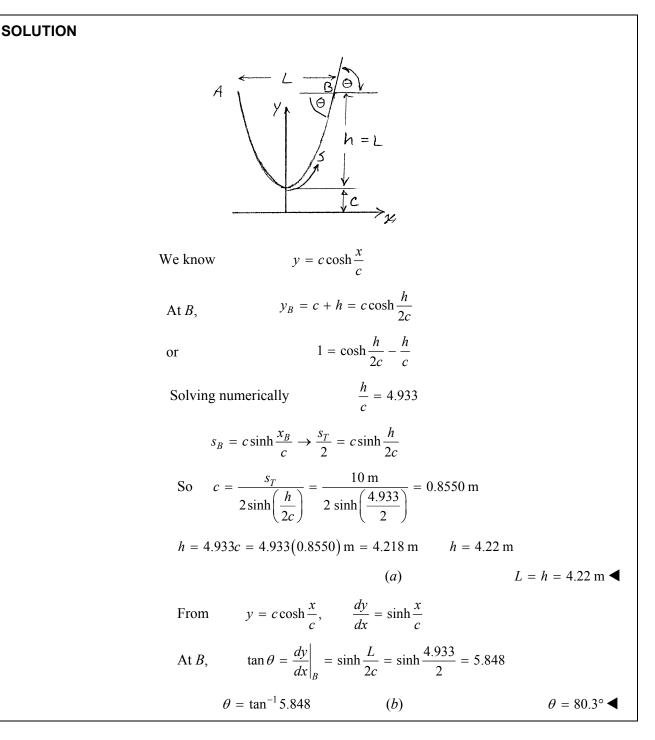


Determine the sag of a 45-ft chain which is attached to two points at the same elevation that are 20 ft apart.



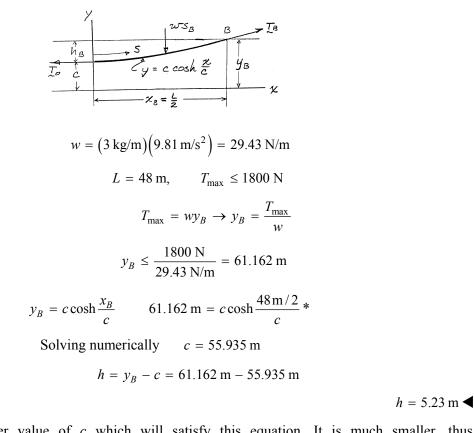


A 10-m rope is attached to two supports *A* and *B* as shown. Determine (*a*) the span of the rope for which the span is equal to the sag, (*b*) the corresponding angle  $\theta_{B}$ .

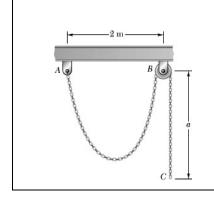


A cable having a mass per unit length of 3 kg/m is suspended between two points at the same elevation that are 48 m apart. Determine the smallest allowable sag of the cable if the maximum tension is not to exceed 1800 N.

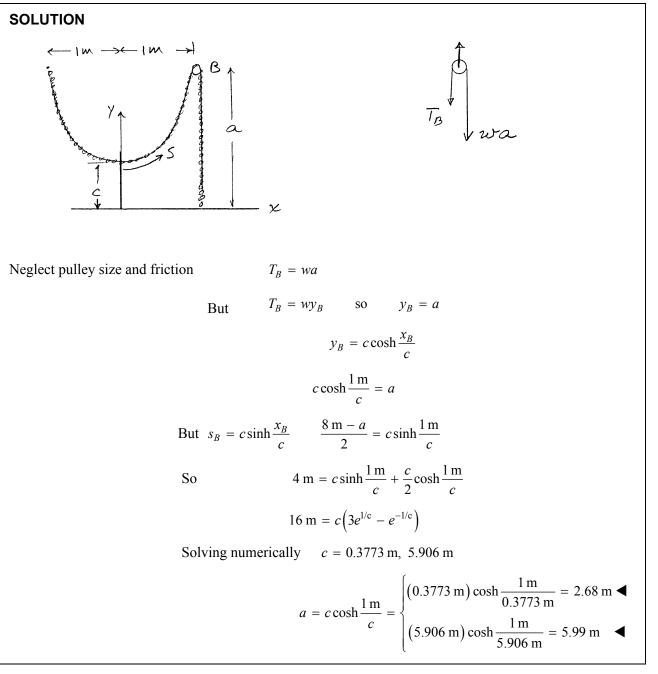
#### SOLUTION

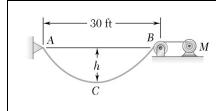


\*Note: There is another value of c which will satisfy this equation. It is much smaller, thus corresponding to a much larger h.



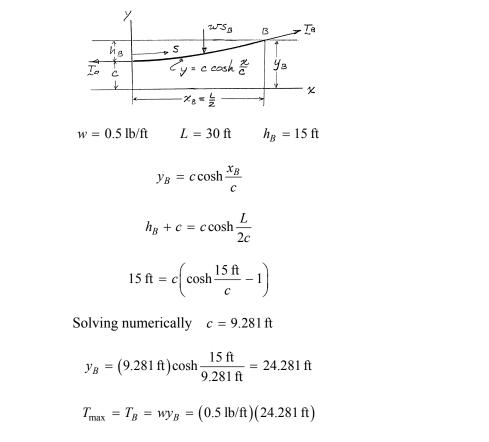
An 8-m length of chain having a mass per unit length of 3.72 kg/m is attached to a beam at A and passes over a small pulley at B as shown. Neglecting the effect of friction, determine the values of distance a for which the chain is in equilibrium.



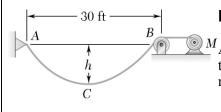


A motor *M* is used to slowly reel in the cable shown. Knowing that the weight per unit length of the cable is 0.5 lb/ft, determine the maximum tension in the cable when h = 15 ft.

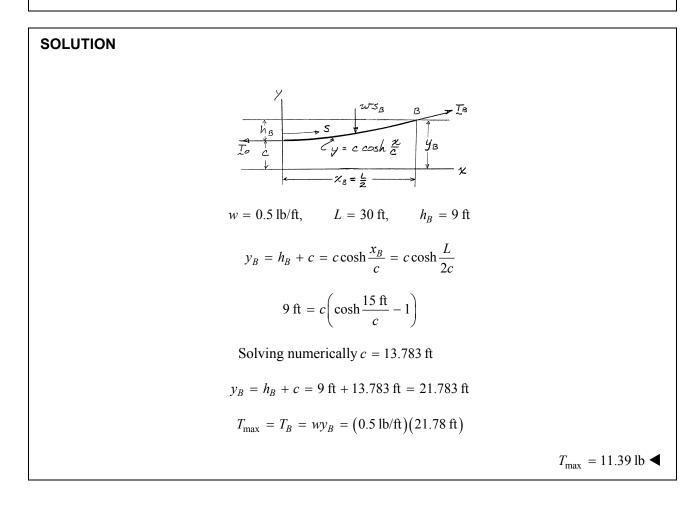
# SOLUTION

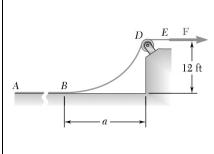


 $T_{\text{max}} = 12.14 \text{ lb} \blacktriangleleft$ 

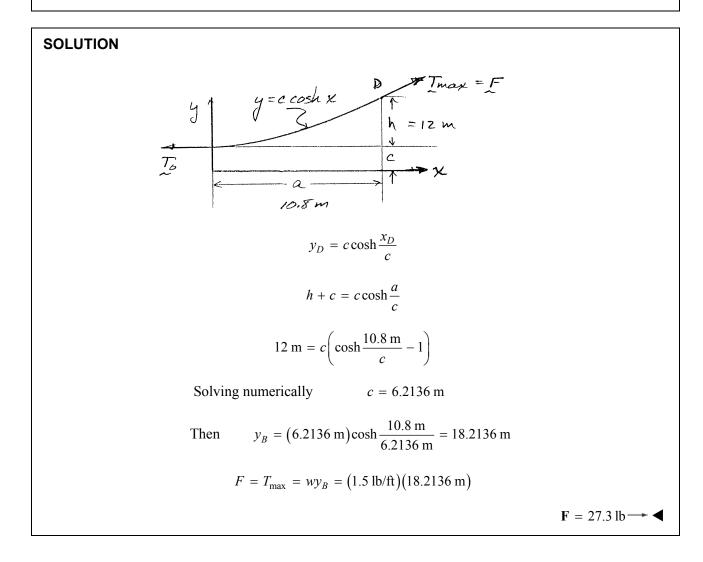


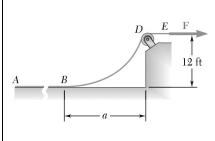
A motor *M* is used to slowly reel in the cable shown. Knowing that the weight per unit length of the cable is 0.5 lb/ft, determine the maximum tension in the cable when h = 9 ft.



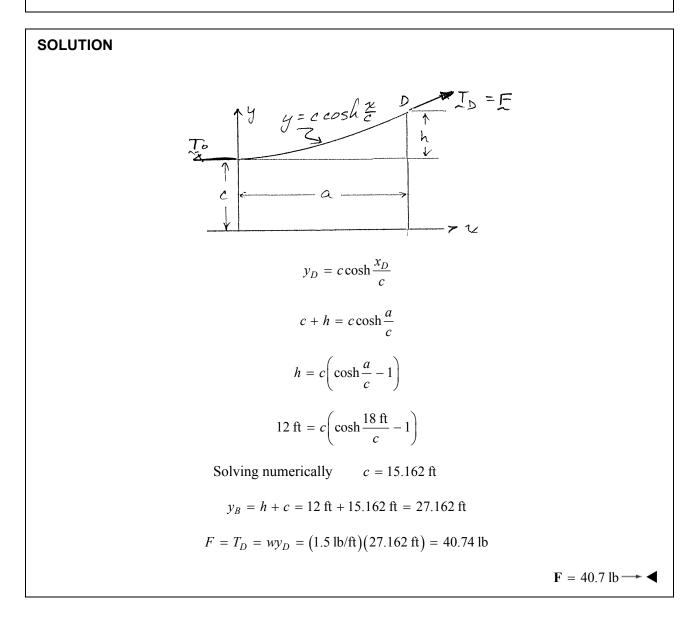


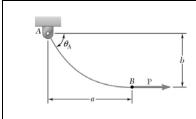
To the left of point *B* the long cable *ABDE* rests on the rough horizontal surface shown. Knowing that the weight per unit length of the cable is 1.5 lb/ft, determine the force **F** when a = 10.8 ft.





To the left of point *B* the long cable *ABDE* rests on the rough horizontal surface shown. Knowing that the weight per unit length of the cable is 1.5 lb/ft, determine the force **F** when a = 18 ft.

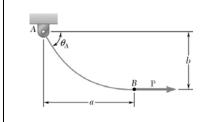




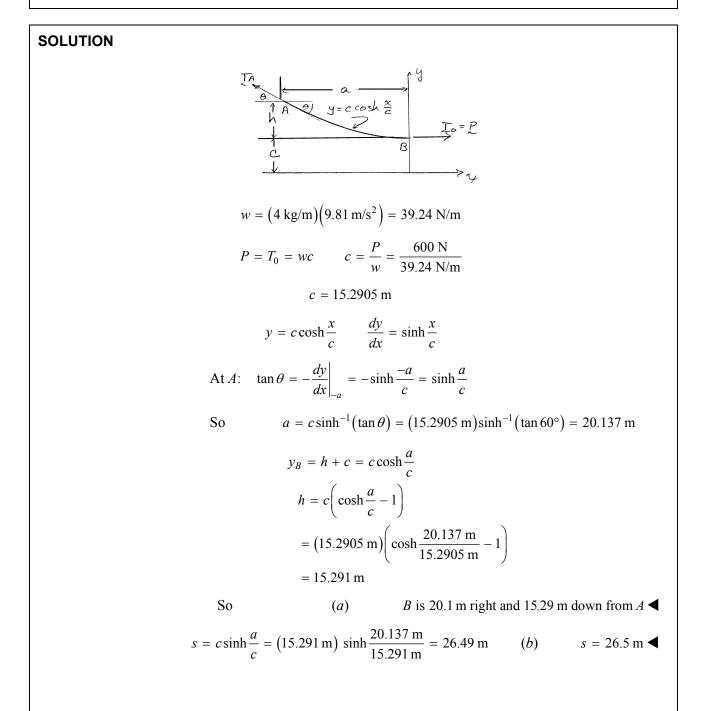
A uniform cable has a mass per unit length of 4 kg/m and is held in the position shown by a horizontal force **P** applied at *B*. Knowing that P = 800 N and  $\theta_A = 60^\circ$ , determine (*a*) the location of point *B*, (*b*) the length of the cable.

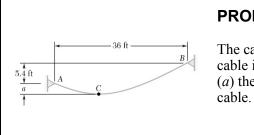
SOLUTION

 $\overline{\mathbb{Y}}$   $y = c \cosh \frac{x}{2}$  $\xrightarrow{B} T_{o} = P$ TO TO TO ĺΧ  $w = 4 \text{ kg/m}(9.81 \text{ m/s}^2) = 39.24 \text{ N/m}$  $P = T_0 = wc$   $c = \frac{P}{w} = \frac{800 \text{ N}}{39.24 \text{ N/m}}$  $c = 20.387 \,\mathrm{m}$  $y = c \cosh \frac{x}{c}$  $\frac{dy}{dx} = \sinh \frac{x}{c}$  $\tan \theta = -\frac{dy}{dx} = -\sinh \frac{-a}{c} = \sinh \frac{a}{c}$  $a = c \sinh^{-1}(\tan \theta) = (20.387 \text{ m}) \sinh^{-1}(\tan 60^{\circ})$ a = 26.849 m $y_A = c \cosh \frac{a}{c} = (20.387 \text{ m}) \cosh \frac{26.849 \text{ m}}{20.387 \text{ m}} = 40.774 \text{ m}$  $b = y_A - c = 40.774 \text{ m} - 20.387 \text{ m} = 20.387 \text{ m}$ So (a)*B* is 26.8 m right and 20.4 m down from  $A \blacktriangleleft$  $s = c \sinh \frac{a}{c} = (20.387 \text{ m}) \sinh \frac{26.849 \text{ m}}{20.387 \text{ m}} = 35.31 \text{ m}$ *(b) s* = 35.3 m ◀

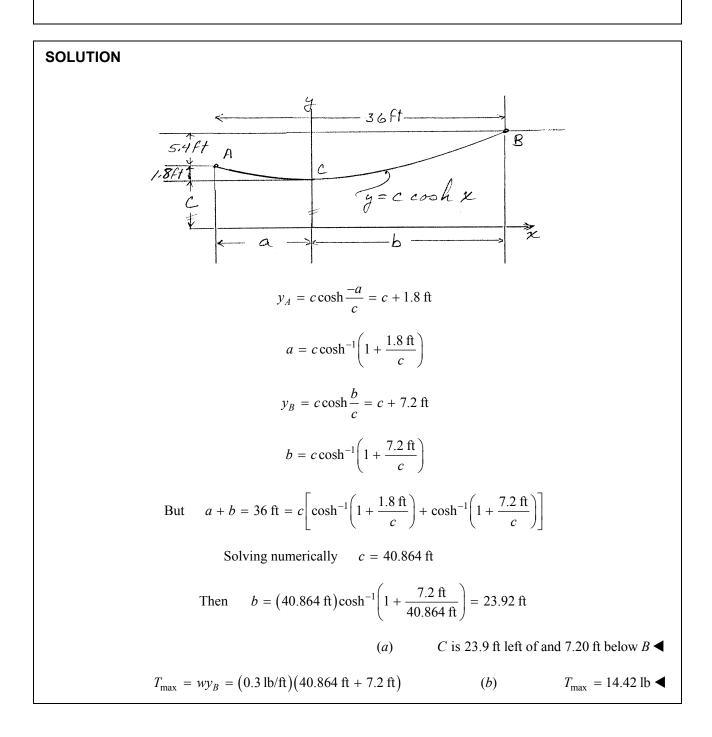


A uniform cable having a mass per unit length of 4 kg/m is held in the position shown by a horizontal force **P** applied at *B*. Knowing that P = 600 N and  $\theta_A = 60^\circ$ , determine (*a*) the location of point *B*, (*b*) the length of the cable.

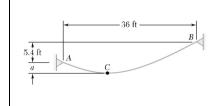




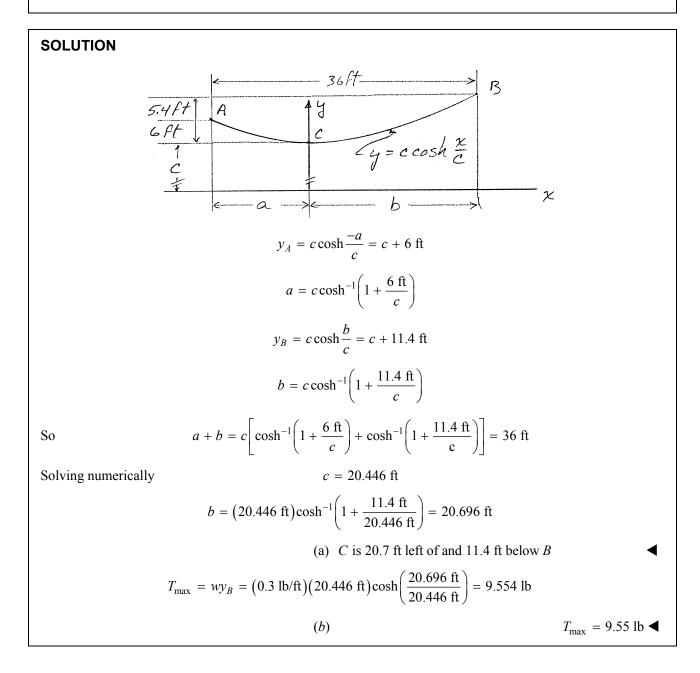
The cable *ACB* weighs 0.3 lb/ft. Knowing that the lowest point of the cable is located at a distance a = 1.8 ft below the support *A*, determine (*a*) the location of the lowest point *C*, (*b*) the maximum tension in the cable.



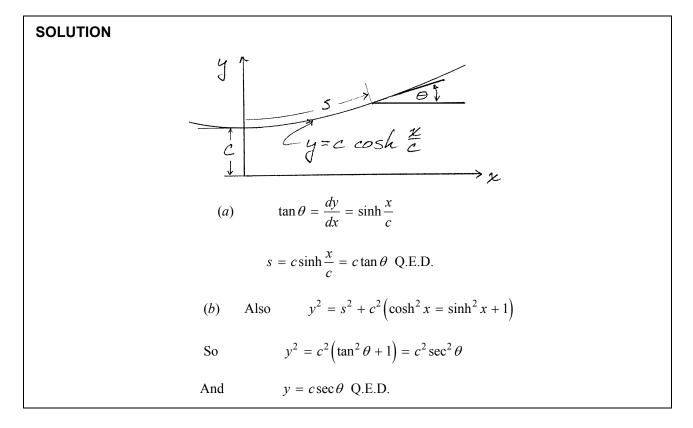
#### PROBLEM 7.140



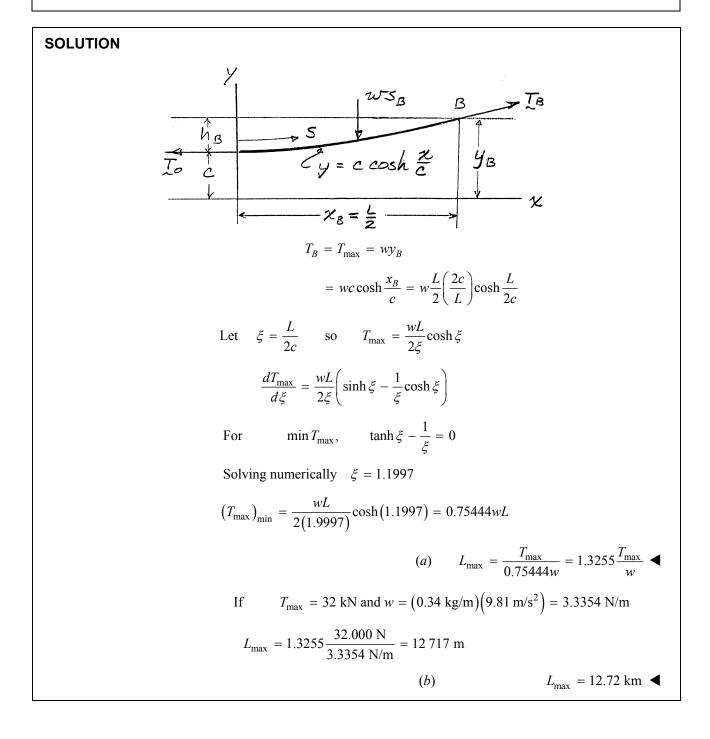
The cable ACB weighs 0.3 lb/ft. Knowing that the lowest point of the cable is located at a distance a = 6 ft below the support A, determine (a) the location of the lowest point C, (b) the maximum tension in the cable.

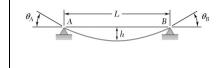


Denoting by  $\theta$  the angle formed by a uniform cable and the horizontal, show that at any point (a)  $s = c \tan \theta$ , (b)  $y = c \sec \theta$ .

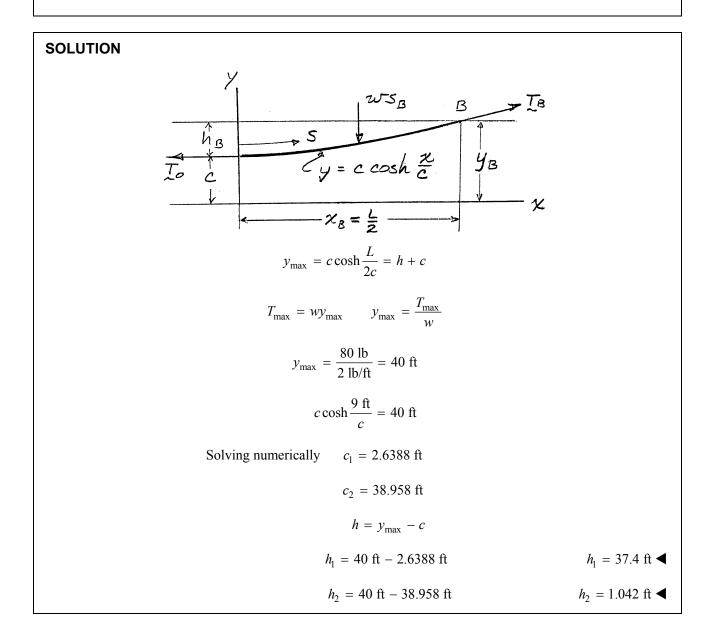


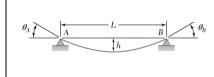
(a) Determine the maximum allowable horizontal span for a uniform cable of mass per unit length m' if the tension in the cable is not to exceed a given value  $T_m$ . (b) Using the result of part a, determine the maximum span of a steel wire for which m' = 0.34 kg/m and  $T_m = 32$  kN.



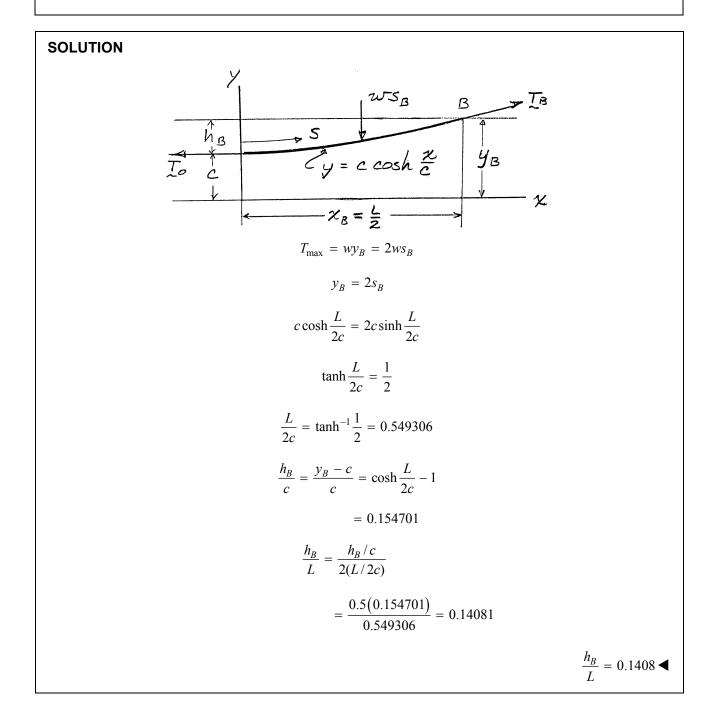


A cable has a weight per unit length of 2 lb/ft and is supported as shown. Knowing that the span L is 18 ft, determine the two values of the sag h for which the maximum tension is 80 lb.



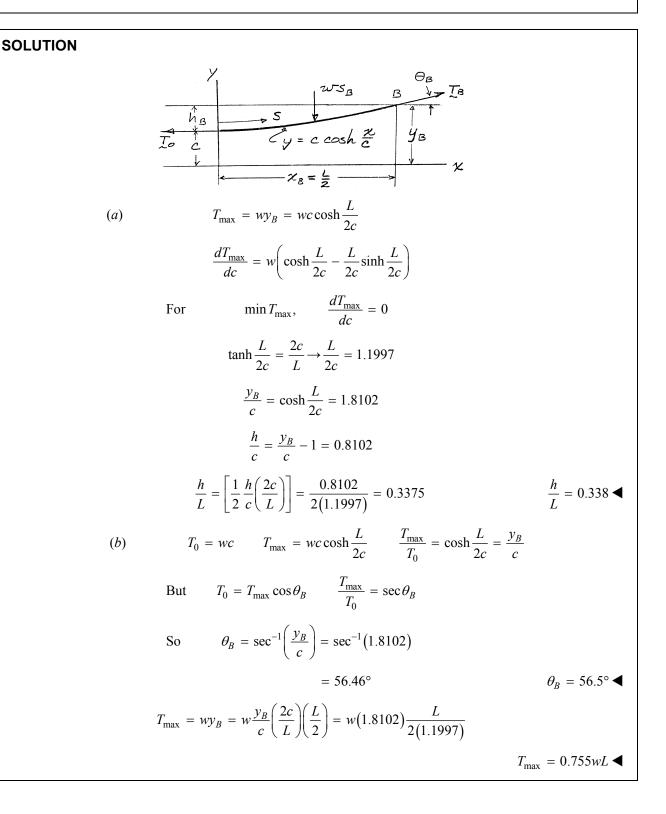


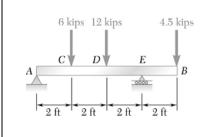
Determine the sag-to-span ratio for which the maximum tension in the cable is equal to the total weight of the entire cable *AB*.



$$\theta_{\Lambda}$$

A cable of weight w per unit length is suspended between two points at the same elevation that are a distance L apart. Determine (a) the sagto-span ratio for which the maximum tension is as small as possible, (b) the corresponding values of  $\theta_B$  and  $T_m$ .

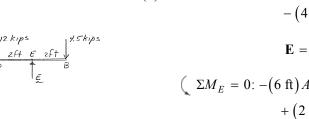


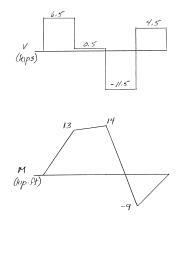


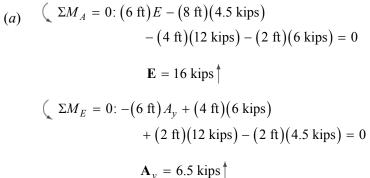
For the beam and loading shown, (a) draw the shear and bending moment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

### SOLUTION

#### **FBD Beam:**



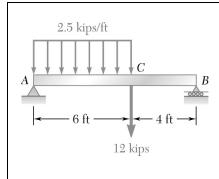




Shear Diag: V is piece wise constant with discontinuities equal to the forces at A, C, D, E, B

Moment Diag: *M* is piecewise linear with slope changes at *C*, *D*, *E* 

 $M_{A} = 0$  $M_C = (6.5 \text{ kips})(2 \text{ ft}) = 13 \text{ kip} \cdot \text{ft}$  $M_C = 13 \operatorname{kip} \cdot \operatorname{ft} + (0.5 \operatorname{kips})(2 \operatorname{ft}) = 14 \operatorname{kip} \cdot \operatorname{ft}$  $M_D = 14 \operatorname{kip} \cdot \operatorname{ft} - (11.5 \operatorname{kips})(2 \operatorname{ft}) = -9 \operatorname{kip} \cdot \operatorname{ft}$  $M_B = -9 \, \text{kip} \cdot \text{ft} + (4.5 \, \text{kips})(2 \, \text{ft}) = 0$  $|V|_{\text{max}} = 11.50$  kips on  $DE \blacktriangleleft$ *(b)*  $|M|_{\text{max}} = 14.00 \text{ kip} \cdot \text{ft} \text{ at } D \blacktriangleleft$ 



For the beam and loading shown, (a) draw the shear and bending moment diagrams, (b) determine the maximum absolute values of the shear and bending moment.

# SOLUTION FBD Beam:

GFt

3

- 11.7

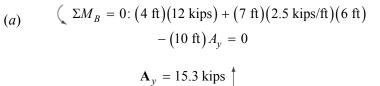
46.8

15.3

Ax

V\_ (kips)

M (kip.ft)



**Shear Diag:**  $V_A = A_y = 15.3$  kips, then V is linear

$$\left(\frac{dV}{dx} = -2.5 \text{ kips/ft}\right) \text{to } C.$$
$$V_C = 15.3 \text{ kips} - (2.5 \text{ kips/ft})(6 \text{ ft}) = 0.3 \text{ kips}$$

At C, V decreases by 12 kips to -11.7 kips and is constant to B.

**Moment Diag:**  $M_A = 0$  and M is parabolic

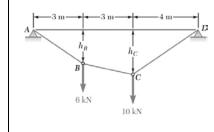
$$\left(\frac{dM}{dx} \text{ decreasing with } V\right) \text{ to } C$$

$$M_C = \frac{1}{2} (15.3 \text{ kips} + 0.3 \text{ kip}) (6 \text{ ft}) = 46.8 \text{ kip} \cdot \text{ft}$$

$$M_B = 46.8 \text{ kip} \cdot \text{ft} - (11.7 \text{ kips}) (4 \text{ ft}) = 0$$

$$(b) \qquad |V|_{\text{max}} = 15.3 \text{ kips} \blacktriangleleft$$

$$|M|_{\text{max}} = 46.8 \text{ kip} \cdot \text{ft} \blacktriangleleft$$



Two loads are suspended as shown from the cable *ABCD*. Knowing that  $h_B = 1.8$  m, determine (*a*) the distance  $h_C$ , (*b*) the components of the reaction at *D*, (*c*) the maximum tension in the cable.

SOLUTION  
FBD Cable:  

$$\rightarrow \Sigma F_x = 0: -A_x + D_x = 0 \qquad A_x = D_x$$

$$(\Sigma M_A = 0: (10 m) D_y - (6 m)(10 kN) - (3 m)(6 kN) = 0$$

$$D_y = 7.8 kN \uparrow$$

$$(\Sigma M_A = 0: (10 m) D_y - (6 m)(10 kN) - (3 m)(6 kN) = 0$$

$$D_y = 7.8 kN \uparrow$$

$$(\Sigma M_B = 0: (1.8 m) A_x - (3 m)(8.2 kN) = 0$$

$$A_x = \frac{41}{3} kN + -$$
FBD AB:  

$$(\Sigma M_B = 1.8 m, From above \qquad D_x = A_x = \frac{41}{3} kN$$
FBD CD:  

$$(\Sigma M_C = 0: (4 m)(7.8 kN) - h_C(\frac{41}{3} kN) = 0$$

$$A_c = 2.28 m$$

$$(b) \qquad D_x = 13.67 kN \rightarrow 4$$

$$D_y = 7.80 kN \uparrow$$

$$C = 0; (4 m)(7.8 kN) - h_C(\frac{41}{3} kN) = 0$$

$$D_y = 7.80 kN \uparrow 4$$

$$C = 0; (4 m)(7.8 kN) - h_C(\frac{41}{3} kN) = 0$$

$$D_y = 7.80 kN \uparrow 4$$

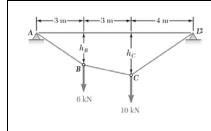
$$C = 0; (4 m)(7.8 kN) - h_C(\frac{41}{3} kN) = 0$$

$$D_y = 7.80 kN \uparrow 4$$

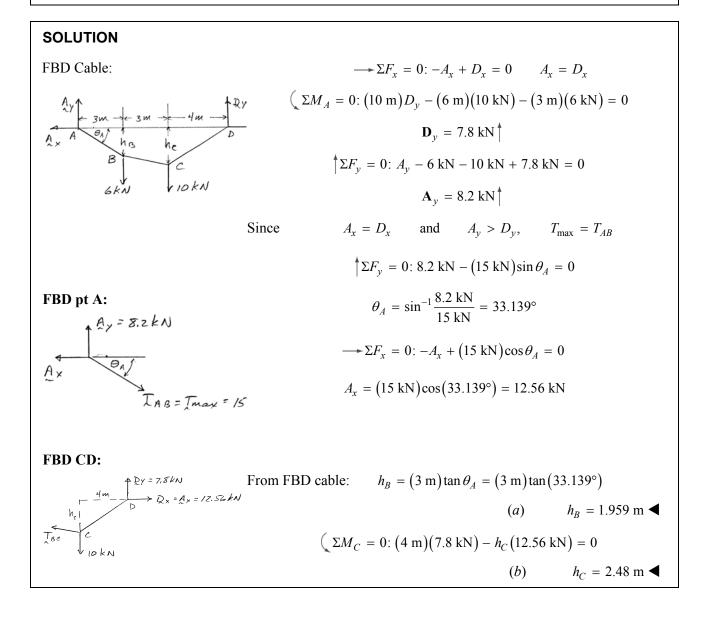
$$C = 0; (4 m)(7.8 kN) - h_C(\frac{41}{3} kN) = 0$$

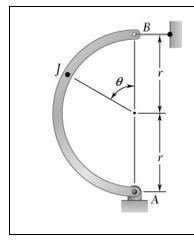
$$D_y = 7.80 kN \uparrow 4$$

$$D_y = 7.80 kN \uparrow 4$$



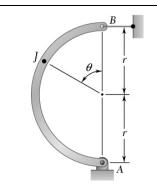
Knowing that the maximum tension in cable *ABCD* is 15 kN, determine (*a*) the distance  $h_B$ , (*b*) the distance  $h_C$ .



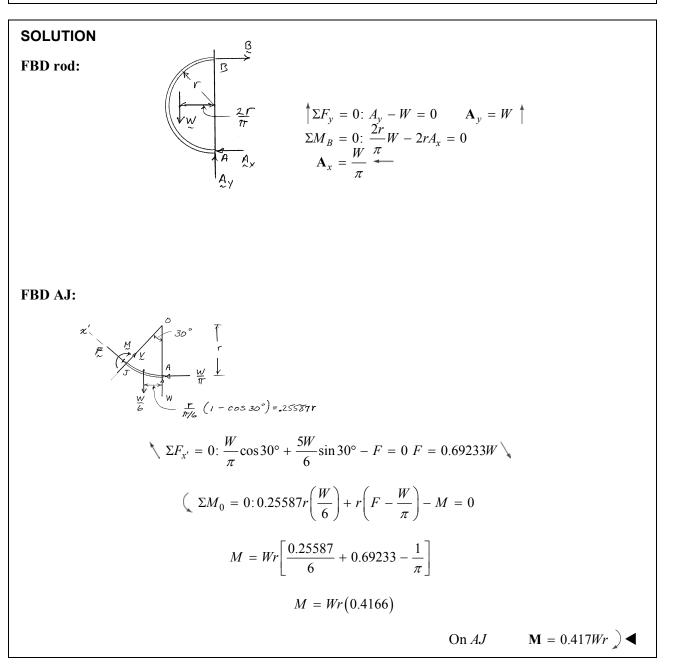


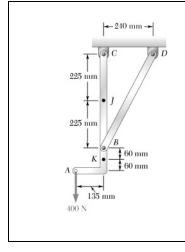
A semicircular rod of weight W and uniform cross section is supported as shown. Determine the bending moment at point Jwhen  $\theta = 60^{\circ}$ .

# SOLUTION **FBD Rod:** $\left(\Sigma M_A = 0: \frac{2r}{\pi}W - 2rB = 0\right)$ в r ₽ $\mathbf{B} = \frac{W}{\pi} \longrightarrow$ $\int \Sigma F_{y'} = 0$ : $F + \frac{W}{3} \sin 60^\circ - \frac{W}{\pi} \cos 60^\circ = 0$ Ŵ F = -0.12952WFBD BJ: W/IT $\left(\Sigma M_0 = 0: r\left(F - \frac{W}{\pi}\right) + \frac{3r}{2\pi}\left(\frac{W}{3}\right) + M = 0$ 3r 211 ↓<u>₩</u> $M = Wr\left(0.12952 + \frac{1}{\pi} - \frac{1}{2\pi}\right) = 0.28868Wr$ On BJ $\mathbf{M}_J = 0.289Wr$ $\mathbf{M}_J$



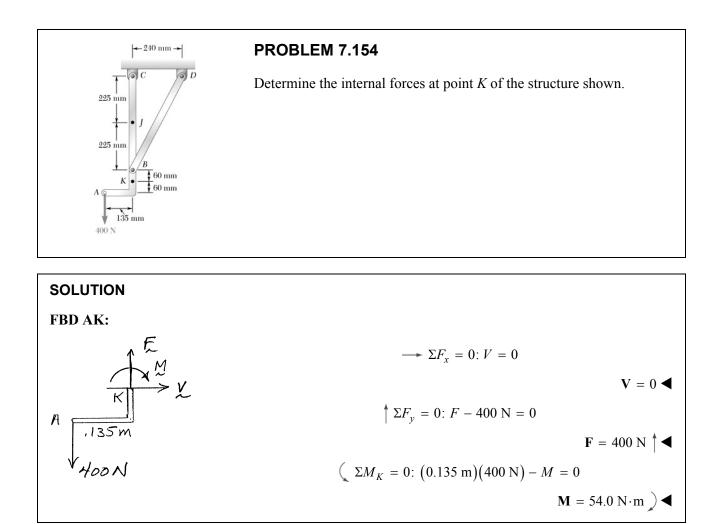
A semicircular rod of weight W and uniform cross section is supported as shown. Determine the bending moment at point Jwhen  $\theta = 150^{\circ}$ .

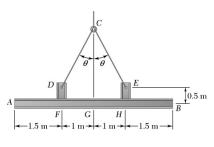




Determine the internal forces at point J of the structure shown.

### SOLUTION **FBD ABC:** Cy .24M D $(\Sigma M_D = 0: (0.375 \text{ m})(400 \text{ N}) - (0.24 \text{ m})C_y = 0$ Ĉ, $C_y = 625 \text{ N}^{\dagger}$ ,45m $(\Sigma M_B = 0: -(0.45 \text{ m})C_x + (0.135 \text{ m})(400 \text{ N}) = 0$ ß ,12m $C_x = 120 \text{ N} \longrightarrow$ A .135m 400 N FBD CJ: 625N C $\sum F_y = 0:625 \text{ N} - F = 0$ 120N $\mathbf{F} = 625 \text{ N} \downarrow \blacktriangleleft$ ,225m $\longrightarrow \Sigma F_x = 0:120 \text{ N} - V = 0$ V = 120.0 N ← ◀ Ň $(\Sigma M_J = 0: M - (0.225 \text{ m})(120 \text{ N}) = 0$ Μ $\mathbf{M} = 27.0 \text{ N} \cdot \text{m}$

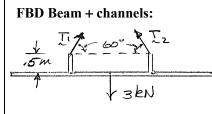




Two small channel sections *DF* and *EH* have been welded to the uniform beam *AB* of weight W = 3 kN to form the rigid structural member shown. This member is being lifted by two cables attached at *D* and *E*. Knowing the  $\theta = 30^{\circ}$  and neglecting the weight of the channel sections, (*a*) draw the shear and bending-moment diagrams for beam *AB*, (*b*) determine the maximum absolute values of the shear and bending moment in the beam.

### SOLUTION

*(a)* 



# By symmetry: $T_1 = T_2 = T$ $\uparrow \Sigma F_y = 0: 2T \sin 60^\circ - 3 \text{ kN} = 0$ $T = \frac{3}{\sqrt{3}} \text{ kN}$ $T_{1x} = \frac{3}{2\sqrt{3}}$ $T_{1y} = \frac{3}{2} \text{ kN}$ $M = (0.5 \text{ m}) \frac{3}{2\sqrt{3}} \text{ kN} = 0.433 \text{ kN} \cdot \text{m}$

FBD Beam:

With cable force replaced by equivalent force-couple system at *F* and *G* 

.6

- 9

.058

675

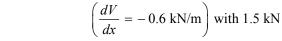
V (KN)

M

(KN·m

×IM×IM×ISM>

-.6



discontinuities at F and H.

$$V_{F^-} = -(0.6 \text{ kN/m})(1.5 \text{ m}) = 0.9 \text{ kN}$$

V increases by 1.5 kN to + 0.6 kN at  $F^+$ 

Shear Diagram: V is piecewise linear

$$V_G = 0.6 \text{ kN} - (0.6 \text{ kN/m})(1 \text{ m}) = 0$$

Finish by invoking symmetry

Moment Diagram: M is piecewise parabolic

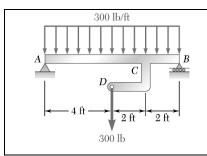
$$\left(\frac{dM}{dx} \text{ decreasing with } V\right) \text{ with discontinuities of .433 kN at } F \text{ and } H.$$
$$M_{F^{-}} = -\frac{1}{2} (0.9 \text{ kN}) (1.5 \text{ m}) = -0.675 \text{ kN} \cdot \text{m}$$

M increases by 0.433 kN·m to -0.242 kN·m at  $F^+$ 

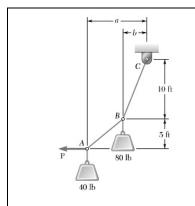
$$M_G = -0.242 \text{ kN} \cdot \text{m} + \frac{1}{2} (0.6 \text{ kN}) (1 \text{ m}) = 0.058 \text{ kN} \cdot \text{m}$$

Finish by invoking symmetry

(b) 
$$|V|_{\max} = 900 \text{ N} \blacktriangleleft$$
  
at  $F^-$  and  $G^+$   
 $|M|_{\max} = 675 \text{ N} \cdot \text{m} \blacktriangleleft$   
at  $F$  and  $G$ 

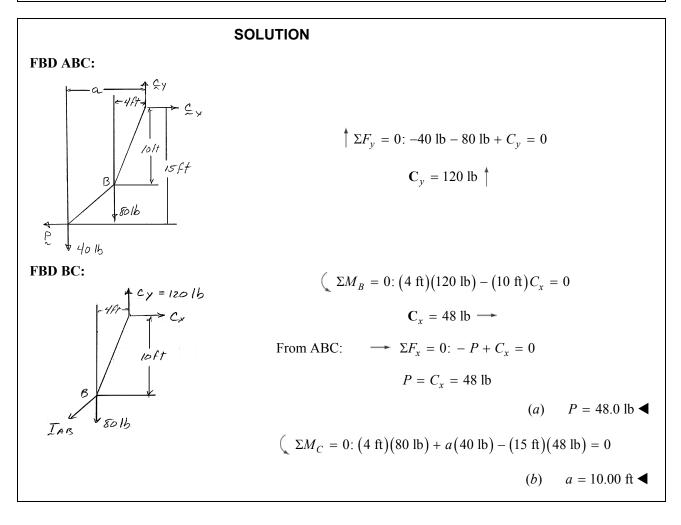


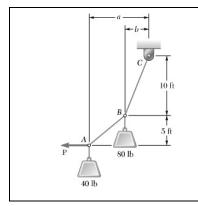
(*a*) Draw the shear and bending moment diagrams for beam *AB*,(*b*) determine the magnitude and location of the maximum absolute value of the bending moment.



### PROBLEM 7.157

Cable *ABC* supports two loads as shown. Knowing that b = 4 ft, determine (*a*) the required magnitude of the horizontal force **P**, (*b*) the corresponding distance *a*.





Cable *ABC* supports two loads as shown. Determine the distances a and b when a horizontal force **P** of magnitude 60 lb is applied at A.

## SOLUTION FBD ABC: < b $\longrightarrow \Sigma F_x = 0: C_x - P = 0 \qquad C_x = 60 \text{ lb} \longrightarrow$ $\uparrow \Sigma F_y = 0: C_y - 40 \text{ lb} - 80 \text{ lb} = 0$ 10Ft 15 Ft B $C_y = 120 \text{ lb}$ 18016 ŕ A + 4016 FBD BC: 1201b > 60 lb $(\Sigma M_B = 0: b(120 \text{ lb}) - (10 \text{ ft})(60 \text{ lb}) = 0$ 10Ft $b = 5.00 \text{ ft} \blacktriangleleft$ V 8016 TAB FBD AB: $\Sigma M_B = 0: (a - b)(40 \text{ lb}) - (5 \text{ ft})60 \text{ lb} = 0$ a-b-/B-solb a - b = 7.5 ft P= 6016 a = b + 7.5 ft = 5 ft + 7.5 ft4016 a = 12.50 ft